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Carlos Falquez

born in Guayaquil, Ecuador

INVESTIGATION OF THERMAL
GROUND-STATE EFFECTS IN
 $SU(2)$ YANG-MILLS THERMODYNAMICS

This diploma thesis has been carried out by
Carlos Falquez
at the
Laboratorium für Applikationen der Synchrotronstrahlung (LAS)
under the supervision of
Priv.-Doz. Dr. Ralf Hofmann

Abstract

We investigate experimental consequences of the postulate that fundamentally photon propagation is governed by an $SU(2)$ rather than a $U(1)$ gauge principle. In the context of thermodynamics the $SU(2)$ Yang-Mills theory is assumed to be in its deconfining phase. In addition to the results already available, we compute the dispersion law for the longitudinal mode, which does not thermalize with matter, at one-loop accuracy. We analyze radiometric and bolometric methods to detect a gap in the black-body radiation spectra for low frequencies and at low temperatures. We simulate the expected experimental results for total-power and Dicke-switch radiometry. These simulations indicate that the predicted $SU(2)$ signature is measurable with presently available detector technology appealing to both radiometric methods. We also investigate non-homogeneous thermodynamics (thermomagnetic effect) in the adiabatic approximation.

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Chapter 1

Introduction

The discovery of the Cosmic Microwave Background (CMB) by Penzias and Wilson [52] is easily one of the pivotal moments in the history of cosmology and the development of the Hot Big-Bang model. COBE further confirmed that the CMB power spectrum follows to a high accuracy $\sim 10^{-2}$ a Planck distribution in the frequency region of $\nu=60-600$ GHz, [48, 49, 68].

Recently, however, measurements of CMB line temperatures T performed by the ARCADE 2 instrument [61] at very low-frequencies ($\nu = 3 \text{ GHz} \dots 90 \text{ GHz}$) show a statistically significant (5σ) unexplained power excess. Combining the ARCADE 2 data with data from the relevant literature in the frequency region from 22 MHz to 10 GHz results in a background power law spectrum of the form [14]

$$T(\nu) = T_0 + T_R \left(\frac{\nu}{\nu_0} \right)^\beta, \quad (1.1)$$

with $T_0 = 2.725 \text{ K}$, $\nu_0 = 1 \text{ GHz}$, $T_R = 1.19 \pm 0.14 \text{ K}$, and a spectral index of $\beta = -2.62 \pm 0.04$. It is further argued in [14] that this deviation from the perfect black-body relation $T(\nu) = \text{const}$ is neither an artifact of galactic foreground subtraction, nor can it be attributed to distant point sources.

Remarkably, a thermodynamical field theory developed in [25, 28] could be able to explain the power excess in (1.1). Namely, it is argued that the gauge group $U(1)_Y$ of the photon field in the Standard Model (SM) is not fundamental but merely emerges from a $SU(2)$ Yang-Mills theory in a specific thermodynamical phase: The *deconfining phase*. This is called the $SU(2)_{\text{CMB}}$ hypothesis. The theory is determined by a single parameter, and can be fixed by specifying the *critical temperature* T_c below which the thermal $SU(2)$ gas undergoes a *phase transition* to the *preconfining phase*.

Assuming the $SU(2)_{\text{CMB}}$ hypothesis, the excess power at low frequencies measured by the ARCADE2 radiometers can be explained as a result of evanescent photon fields thermalized near the critical temperature $T_c \stackrel{!}{=} T_{\text{CMB}}$ of the deconfining phase [30].

That such an explanation for the excess power of the CMB is possible based solely on gauge symmetry considerations and finite temperature effects motivates the search for further experimental evidence in favor of the $SU(2)_{\text{CMB}}$ hypothesis. The ARCADE2 observation serves to fix T_c , which we use to predict further observable consequences that can then be tested by experiment.

The purpose of this thesis is the investigation of possible realizations of such an experimental test. We discuss the characteristics of the thermal radiation spectrum at low

temperature and frequency under the $SU(2)_{\text{CMB}}$ hypothesis. It will turn out that $SU(2)$ gauge dynamics manifests itself through the appearance of a temperature-dependent *frequency cutoff* $\nu^*(T)$ below which photon propagation is forbidden. The cutoff frequency ν^* thus defines a *screening region*. At low frequencies and temperatures comparable to that of T_c , this effect results in a *black-body anomaly*: The vanishing of the power output of a black-body cavity within the screening region. This will turn out to be the key experimental effect to search for when probing for $SU(2)$ physics.

This thesis is organized as follows. Chapter 2 reviews elementary properties of gauge theory and corresponding symmetry groups. A short review of Maxwell electrodynamics introduces the required mathematical formalism which is then generalized to nonabelian gauge symmetries. Basic concepts of topological configurations in $SU(2)$ Yang-Mills theory are introduced. In the final section, thermal field theory is shortly summarized. Chapter 3 serves as an introduction to our main subject: The thermodynamics of $SU(2)$ Yang-Mills theory, in the context of the nonperturbative approach developed in [25, 28]. After a review of the relevant theory, we proceed to calculate the dispersion law of the transverse and longitudinal polarization modes of the $SU(2)$ photon. We also investigate the thermodynamical consistency of one-loop resummed energy density and pressure. In chapter 4 we investigate the possibility of generalizing an important assumption made in chapter 3 while deriving the thermal ground state, namely thermodynamical homogeneity (and isotropy). It will turn out that, within the restrictions imposed by an adiabatic approximation, certain deviations from homogeneity are indeed allowed. Chapter 5 is the most important section of this work. After a quick introduction to the basics of radiation transfer, antenna theory and radiometry, we investigate the implications of the $SU(2)_{\text{CMB}}$ hypothesis on the radiometric measurement of thermal photon radiation. We show how the existence of a screening region can be established through purely radiometric means. In the final section, we comment on the possibility of a bolometric experimental setup. The appendices contain the details of certain derivations. Essential for chapter 4 is the result derived in appendix A, where a particular solution to the $SU(2)$ Yang-Mills equations in Minkowskian signature is derived. We have attached a CD with the Mathematica source code used in this work.

Unless stated otherwise, we always work in natural units $\hbar = c = k_B = 1$.

Chapter 2

Gauge Fields and Symmetries

In this chapter, we give a very summarized survey of gauge theory and related concepts, in order to provide the reader with the minimal background needed for chapter 3. We first review the basics of gauge theory and symmetry groups, then we briefly show how Yang-Mills theory emerges by extending the U(1) symmetry to the nonabelian gauge group SU(N). Next, we discuss topological field configurations in the context of Euclidean Yang-Mills theory. Finally, a brief summary of thermal field theory is given for completeness.

2.1 Gauge theories and symmetry groups

2.1.1 Maxwell electrodynamics

In the Lagrangian formalism, the dynamics of the photon field A^μ in the presence of an external charged field of current density j^μ are described by the *Maxwell Lagrangian density* \mathcal{L}_M

$$\mathcal{L}_M \equiv -\frac{1}{4}F^{\mu\nu}F_{\mu\nu} - ej^\mu A_\mu. \quad (2.1)$$

where the *coupling constant* e characterizes the strength of the electromagnetic interaction. It is identified with the *electric charge* of the current j^μ inducing external field.

The *field strength tensor* $F_{\mu\nu}$ can be defined by the action of the commutator $[D_\mu, D_\nu]$ on an arbitrary Lorentz scalar Φ

$$F_{\mu\nu}\Phi \equiv \frac{i}{e}[D_\mu, D_\nu]\Phi, \quad (2.2)$$

where the *covariant derivative* D_μ is defined in terms of the *gauge potential* A_μ

$$D_\mu \equiv \partial_\mu - ieA_\mu. \quad (2.3)$$

The familiar electromagnetic vector fields \mathbf{E} and \mathbf{B} are recovered from the field strength tensor by the identities

$$E^i \equiv -F^{0i}, \quad (2.4)$$

$$B^i \equiv -\frac{1}{2}\epsilon^{ijk}F_{jk}. \quad (2.5)$$

It can be shown (Bohm-Aharonov effect) that the gauge potential A_μ , not the field strength tensor $F_{\mu\nu}$, is the fundamental physical field of the theory [57].

The Maxwell field strength tensor can in turn be written in terms of the gauge potential A_μ by inserting equation (2.3) in (2.2)

$$F_{\mu\nu} = \partial_\mu A_\nu - \partial_\nu A_\mu. \quad (2.6)$$

Note that the electromagnetic coupling e does not appear in the expression (2.6), since the single gauge field commutes with itself and terms such as $e^2[A_\mu, A_\nu]$ vanish. The photon cannot *interact with itself*, and does not carry charge. We will later generalize Maxwell electrodynamics to allow for a selfinteracting (also charged) gauge potential multiplet.

The *inhomogeneous* Maxwell equations are given by the Euler-Lagrange equations of motion derived from (2.1) by the principle of least action

$$\partial_\mu F^{\mu\nu} = j^\nu. \quad (2.7)$$

The *homogeneous* Maxwell equations follow from the *Bianchi identity* [3, 15, 57]

$$\partial_\mu \tilde{F}^{\mu\nu} = 0, \quad (2.8)$$

where the *dual field strength tensor* $\tilde{F}^{\mu\nu}$ is defined by

$$\tilde{F}^{\mu\nu} \equiv \frac{1}{2} \epsilon^{\mu\nu\sigma\rho} F_{\sigma\rho}. \quad (2.9)$$

Here $\epsilon^{\mu\nu\sigma\rho}$ is the totally antisymmetric Levi-Civita tensor with $\epsilon^{0123} = 1$.

The dynamics of the system described by equation. (2.7) and (2.8) are *invariant* under local field shifts

$$A_\mu \rightarrow A'_\mu = A_\mu + \frac{1}{e} \partial_\mu \xi, \quad (2.10)$$

with $\xi = \xi(x)$ an arbitrary Lorentz scalar function. Transformations of the form (2.10) are called *gauge transformations*. They leave the field strength tensor (2.6), and thus the equations of motion (2.7) and integrability conditions (2.8), unmodified

$$F^{\mu\nu} \rightarrow F'^{\mu\nu} = F^{\mu\nu}. \quad (2.11)$$

This *gauge invariance* is a manifestation of redundancy in the degrees of freedom of the theory: The photon is a massless spin-1 particle with only two transverse polarizations, yet in (2.1) the dynamics are given by a 4-component gauge potential A_μ . The excess polarization modes are nevertheless necessary for a covariant formalism. Local gauge freedom also implies that the gauge potential transforms under Lorentz rotations as a 4-vector only up to gauge transformations. A Lorentz transformation between two frames is always associated with a gauge transformation [50].

In the framework of differential geometry, the field A_μ with transformation law (2.10) can be interpreted as the *connection* on a *principal* $U(1)$ -*bundle* over the space-time manifold \mathbb{R}^4 with Minkowskian signature $(+, -, -, -)$, $U(1)$ being the group of 1×1 unitary matrices [3, 15]. The Maxwell gauge potential A_μ is therefore also called the $U(1)$ *gauge field*. Its emergence can be understood as the result of demanding *invariance* under *local*

phase transformations of the quantum state vector $|\psi\rangle$ characterizing the physical system [57]

$$|\psi\rangle \rightarrow |\psi'\rangle = \Omega(x)|\psi\rangle, \quad \langle\psi'|\psi'\rangle \stackrel{!}{=} \langle\psi|\psi\rangle. \quad (2.12)$$

Here, $\Omega(x) = e^{i\xi(x)}$ is a space-time function taking values in $U(1)$, which we write for simplicity as $\Omega(x) \in U(1)$. Theories which exhibit invariance under a continuous group of *local symmetry transformations* are called *gauge theories*. The group $U(1)$ is the *gauge group* of the Maxwell theory. After a $U(1)$ phase transformation, the Maxwell gauge field A_μ transforms as in (2.10), which may be rewritten as

$$A_\mu \rightarrow A'_\mu = \Omega A_\mu \Omega^\dagger + \frac{i}{e} \Omega \partial_\mu \Omega^\dagger, \quad (2.13)$$

for any $\Omega(x) \in U(1)$.

The geometric formalism just described can be generalized to larger groups G , while respecting Lorentz symmetries and covariance [3]. From (2.12) it is clear that G must be either unitary or anti-unitary. Following Yang and Mills [71], we replace phase transformations with non-abelian *isotopic spin* rotations of $SU(2)$ valued fields. The theory of $SU(N)$ groups is reviewed in the next section.

2.1.2 Lie groups and Lie algebras

The $U(1)$ group underlying Maxwell electromagnetism is the *abelian* group of phase rotations (two arbitrary phase rotations commute), and a generic element of $U(1)$ may be written as $e^{i\xi}$ with real parameter ξ . In general, a *continuous group* G of order n may be parametrized by a set of n real parameters. A *Lie group* G of order n is a continuous group where the set of parameters live in a differentiable manifold M^n . The operations of group multiplication and inversion are *smooth maps* in M^n . A *compact Lie group* is a Lie group with compact manifold.

In the neighbourhood near the identity element $\mathbf{1}$, M^n looks locally like \mathbb{R}^n with flat Euclidean metric. This region can always be given a coordinate basis. The n coordinate unit vectors t^a , $a = 1..n$ are called the *generators* of the group G . Every element g of G near the identity can thus be written as

$$g = \mathbf{1} + i\omega^a t^a, \quad (2.14)$$

with ω_a infinitesimal parameters. Note that for unitary groups $U(N)$, t^a is hermitian, and for special unitary groups $SU(N)$, t^a is also traceless. Elements further away from the identity are generated by the *exponential map* $e^{i\omega^a t^a}$. In the case of a matrix group, the exponential map is given by the usual series

$$e^{i\omega^a t^a} = \sum_{n=0}^{\infty} \frac{i^n}{n!} (\omega^a t^a)^n. \quad (2.15)$$

Let g_1 and g_2 be two elements close to the identity, from (2.14) we write them as $g_1 = \mathbf{1} + i\omega_1^a t^a$ and $g_2 = \mathbf{1} + i\omega_2^a t^a$. Their product is given, up to first order, by the expression $g_1 g_2 = \mathbf{1} + i(\omega_1^a + \omega_2^a) t^a + O(\omega^2)$, so up to first order they both commute,

$[g_1, g_2] = O(\omega^2)$. Up to second order, however, the expression $g_1 g_2 g_1^{-1} g_2^{-1}$ is not the identity, but

$$g_1 g_2 g_1^{-1} g_2^{-1} = \mathbf{1} - \omega_1^a \omega_2^b [t^a, t^b]. \quad (2.16)$$

Nevertheless, (2.16) is still close enough to the identity such that it can be written as in (2.14). This means that the commutator $[t^a, t^b]$ must be a linear combination of the generators t^c

$$[t^a, t^b] = i f^{abc} t^c. \quad (2.17)$$

The factors $f^{abc} \in \mathbb{R}$ are called *structure constants*, and can always be chosen to be completely antisymmetric. The generators t^c together with the commutator relations (2.17) define the *Lie algebra* of the group G , which we denote as \mathfrak{g} . The *rank* of the Lie algebra is defined as the number of mutually commuting and linear independent generators. These generators form the *Cartan sub-algebra* of the group. A Lie group G containing no invariant subgroup other than the identity and G itself is called *simple*. A Lie group G is called *semi-simple* if it does not contain any abelian invariant subgroup other than the identity.

Finally, we review some concepts from the theory of representations [19]. A linear representation R of a group G is a map which associates every element g of G with a linear transformation $R(g)$ acting on a vector space V of dimension m . For a given basis of V , the transformations $R(g)$ can be written as matrices, also of dimension m . The elements of a matrix group, for example, build a representation themselves, called the *fundamental representation* of the group. For a Lie group with n generators, the structure constants also define a matrix representation, the *adjoint representation*, made up of $n \times n$ matrices

$$(R_c)_{ab} = -i f^{abc}. \quad (2.18)$$

Further discussion of Lie groups, Lie algebras, and their representations can be found in [19]. In the following, we specialize for the group $SU(2)$.

2.2 $SU(2)$ Yang-Mills Theory

Following Yang and Mills [71], we extend the gauge symmetry of the vacuum ($j^\mu \equiv 0$) Maxwell equations to the non-abelian compact Lie group $SU(2)$. The group $SU(2)$ is defined as the group of 2×2 unitary matrices with unit determinant. It is a continuous Lie group of rank 1, and its Lie algebra is defined by three traceless hermitian generators which we may choose as $t^a = \frac{1}{2} \sigma^a$, $a = 1..3$, where σ^a are the Pauli matrices. Then $\text{tr } t^a t^b = \frac{1}{2} \delta^{ab}$, and the structure constant is the totally antisymmetric tensor $f^{abc} = \epsilon^{abc}$. The matrices t^a define the 2-dimensional fundamental representation, while the 3-dimensional adjoint representation is given by the structure constant as in (2.18).

Define now the Yang-Mills Lie-algebra valued connection A_μ

$$A_\mu(x) = A_\mu^a(x) t^a, \quad (2.19)$$

where the $A_\mu^a(x)$ are (Minkowski) space-time-dependent real functions. The gauge potentials A_μ^a now carry space-time index μ and internal symmetry index a . They are the basic dynamical variables of $SU(2)$ Yang-Mills theory.

Generalizing (2.13), we demand that under SU(2) gauge transformations, the Lie-algebra valued potential transform as

$$A_\mu \rightarrow A'_\mu = \Omega A_\mu \Omega^\dagger + \frac{i}{g} \Omega \partial_\mu \Omega^\dagger, \quad (2.20)$$

where the local transformation $\Omega(x) = e^{i\omega^a t^a}$ is now an element of SU(2), $\Omega(x) \in \text{SU}(2)$, and g is the Yang-Mills *gauge coupling*. Note that this implies that the individual gauge potentials $A_\mu^a = 2\text{tr } A_\mu t^a$ transform in the adjoint representation, up to an inhomogeneous term. A field ϕ^a transforming homogeneously $\phi^a \rightarrow \phi'^a = \Omega_{\text{adj}}^{ab} \phi^b$ under the adjoint representation $\Omega_{\text{adj}}^{ab} \equiv 2\text{tr } t^a \Omega t^b \Omega^\dagger$ is also called an *adjoint field*.

As in Maxwell electrodynamics, we introduce the SU(2) gauge covariant derivative D_μ . The operator D_μ is constructed so that a field and its covariant derivative transform in the same way. Acting on a field ϕ that transforms bi-homogeneously under the fundamental representation, $\phi \rightarrow \Omega \phi \Omega^\dagger$, D_μ acts as a SU(2) matrix

$$D_\mu = \mathbf{1}_{2 \times 2} \partial_\mu - ig A_\mu. \quad (2.21)$$

This results in a bi-homogeneous transformation law for $D_\mu \phi$

$$D_\mu \phi \rightarrow \Omega D_\mu \phi \Omega^\dagger. \quad (2.22)$$

Similarly, on an adjoint field ϕ^a , D_μ acts as

$$(D_\mu \phi)^a = [D_\mu, \phi]^a = \partial_\mu \phi^a + g f^{abc} A_\mu^b \phi^c, \quad (2.23)$$

so that the transformation for the adjoint field $(D_\mu \phi)^a$ reads

$$(D_\mu \phi)^a \rightarrow \Omega_{\text{adj}}^{ab} (D_\mu \phi)^b. \quad (2.24)$$

A Lie-valued Yang-Mills field strength tensor $F_{\mu\nu}$ can be defined as in (2.2) by its action on a field ϕ living in the fundamental representation

$$F_{\mu\nu} \phi = \frac{i}{g} [D_\mu, D_\nu] \phi. \quad (2.25)$$

Calculating the commutator in (2.25) gives

$$F_{\mu\nu} = \partial_\mu A_\nu - \partial_\nu A_\mu - ig [A_\mu, A_\nu], \quad (2.26)$$

written in components

$$F_{\mu\nu}^a = \partial_\mu A_\nu^a - \partial_\nu A_\mu^a + g f^{abc} A_\mu^b A_\nu^c. \quad (2.27)$$

Observe that, compared with the strength tensor (2.6) of the U(1) theory, expression (2.27) has an extra term which is antisymmetric and bilinear in the gauge fields A_μ^a , and proportional to g . It describes gauge field self-interactions, and is what makes *non-abelian* gauge theories fundamentally different from their abelian Maxwell counterpart.

By construction, the Yang-Mills field strength tensor $F_{\mu\nu}$ transforms in the fundamental representation

$$F_{\mu\nu} \rightarrow \Omega F_{\mu\nu} \Omega^\dagger. \quad (2.28)$$

This allows us to define a gauge invariant pure Yang-Mills SU(2) Lagrangian \mathcal{L}_{YM}

$$\begin{aligned}\mathcal{L}_{YM} &\equiv -\frac{1}{4}F^{a\mu\nu}F_{\mu\nu}^a \\ &= -\frac{1}{2}\text{tr } F^{\mu\nu}F_{\mu\nu}.\end{aligned}\tag{2.29}$$

The term *pure* refers to the absence in (2.29) of any field other than the SU(2) gauge field. From the behaviour of the field strength tensor under gauge transformations (2.28) it is easily seen that the Lagrangian defined in (2.29) is SU(2) gauge invariant. Further, Lagrangian (2.29) respects Lorentz invariance, renormalizability and CP-Invariance. A term proportional to $F_{\mu\nu}^a\tilde{F}^{a\mu\nu}$, where the SU(2) dual field strength tensor is defined as in (2.9), $\tilde{F}^{a\mu\nu} \equiv \frac{1}{2}\varepsilon^{\mu\nu\rho\sigma}F_{\rho\sigma}^a$, may be added to the SU(2) Lagrangian (2.29) if the demand for CP-Invariance is relaxed, but this will not concern us in this work.

The SU(2) Yang-Mills action \mathcal{S}_{YM} is defined as

$$\begin{aligned}\mathcal{S}_{YM} &\equiv \int d^4x \mathcal{L}_{YM} \\ &= -\frac{1}{4} \int d^4x F^{a\mu\nu}F_{\mu\nu}^a.\end{aligned}\tag{2.30}$$

The Euler-Lagrange equations of motion can be derived from (2.30) by the principle of least action. We obtain the *SU(2) Yang-Mills equations of motion*

$$D_\mu F^{\mu\nu} = 0.\tag{2.31}$$

As in the Maxwell case, the Bianchi identity of differential geometry results in the integrability conditions [3, 44]

$$D_\mu \tilde{F}^{\mu\nu} = 0.\tag{2.32}$$

Note that (2.31) follows from (2.32) if the field strength tensor satisfies

$$F_{\mu\nu}^a = \tilde{F}_{\mu\nu}^a,\tag{2.33}$$

in which case $F_{\mu\nu}$ is called *selfdual*, or

$$F_{\mu\nu}^a = -\tilde{F}_{\mu\nu}^a.\tag{2.34}$$

in which case $F_{\mu\nu}$ is called *anti-selfdual*. Because of their importance, such field configurations are discussed in the next section.

2.2.1 Selfdual field configurations

We have seen that for *(anti) selfdual field configurations*

$$F_{\mu\nu}^a = \pm \tilde{F}_{\mu\nu}^a,\tag{2.35}$$

the SU(2) Yang-Mills equations (2.31) are *automatically satisfied*, since (2.31) then follows from the geometric identity (2.32). This is significant, since equation (2.35) is *first-order*, yet (2.35) automatically implies the *second-order* Yang-Mills equations.

There are no known solutions for the selfdual equation (2.35) in 4D Minkowski $SU(2)$ Yang-Mills theory. Consider now Euclidean 4D Yang-Mills, which is arrived at by letting the metric become $g_{\mu\nu} \rightarrow -\delta_{\mu\nu}$ and rotating the real time-like component of the 4-vectors

$$x^0 \rightarrow ix^4, \quad (2.36a)$$

$$A_0^a \rightarrow -iA_4^a. \quad (2.36b)$$

with real x^4, A_4^a . It can be shown that the Euclidean Yang-Mills action \mathcal{S}_{YM}^E in \mathbb{R}^4 (that is, the action (2.30) after rotation (2.36)) can be decomposed as

$$\mathcal{S}_{YM}^E = \frac{1}{4} \int d^4x \left[\pm F^{a\mu\nu} \tilde{F}_{\mu\nu}^a + \frac{1}{2} \left(F_{\mu\nu}^a \mp \tilde{F}_{\mu\nu}^a \right)^2 \right]. \quad (2.37)$$

This is the celebrated *Bogomol'nyi decomposition* [6]. The action (2.37) is invariant under space-time translations. The canonical *Euclidean energy-momentum tensor* $\theta_{\mu\nu}$ then follows from Noether's theorem [20] as the Noether current resulting from translation invariance, and can be calculated from the Lagrangian (2.29) after rotation (2.36) (up to a 4-divergence term). In the case of pure Yang-Mills theory it can be written as [55]

$$\theta_{\mu\nu} = \frac{1}{4} \text{tr} \left[\left(F_{\mu\lambda} - \tilde{F}_{\mu\lambda} \right) \left(F_{\nu\lambda} + \tilde{F}_{\nu\lambda} \right) + (\mu \leftrightarrow \nu) \right] \quad (2.38)$$

Note that for (anti) selfdual field configurations the energy-momentum tensor (2.38) *vanishes*. This guarantees that (anti) selfdual field configurations have zero energy-momentum, and *do not propagate*. Further, the Euclidean action (2.35) becomes

$$\mathcal{S}_{YM}^E = \pm \frac{1}{4} \int d^4x F^{a\mu\nu} \tilde{F}_{\mu\nu}^a, \quad (2.39)$$

with $+/-$ sign for selfdual/anti-selfdual field configurations.

To further interpret this result, rescale the field strength by absorbing the coupling constant in the gauge field: $gA_\mu \rightarrow A_\mu$. Then $F_{\mu\nu}^a \rightarrow \frac{1}{g} F_{\mu\nu}^a$, and the expression (2.39) goes to

$$\mathcal{S}_{YM}^E \rightarrow \pm \frac{1}{4g^2} \int d^4x F^{a\mu\nu} \tilde{F}_{\mu\nu}^a. \quad (2.40)$$

Consider now field configurations with finite action (2.40). Following [3], we assume finite action configurations define a field strength which vanishes at infinity. That is, $F_{a\mu\nu}(x) \rightarrow 0$ sufficiently fast as $|x| \rightarrow \infty$. The gauge potential $A_\mu(x)$ of finite action configurations should therefore also tend to zero. But because of *gauge freedom*, this limit is zero only up to a gauge transformation (2.20)

$$\lim_{|x| \rightarrow \infty} A_\mu(x) \sim \Omega(x) \partial_\mu \Omega^\dagger(x). \quad (2.41)$$

The gauge transformation $\Omega(x)$ need only be defined at large $|x|$, say over a sphere S^3 at the boundary of Euclidean 4-space-time. In this sense, $\Omega(x)$ defines a continuous map

$$\Omega : S^3 \rightarrow SU(2) \quad (2.42)$$

But such a map has a well defined *integer invariant*: The *Pontryagin index* (topological charge) k which counts the number of times the map Ω wraps around the $SU(2)$ manifold.

Thus, in Euclidean Yang-Mills theories, asymptotically flat potentials can be distinguished by its Pontryagin index. It is a *topological invariant* of the field configuration: Smooth deformations of the gauge field away from the Euclidean boundary S^3 cannot change the value of k . For the group $SU(2)$, the index k is given by the gauge invariant expression [3]

$$8\pi^2 k \equiv \frac{1}{4} \int d^4x F^{a\mu\nu} \tilde{F}_{\mu\nu}^a. \quad (2.43)$$

For (anti)selfdual field configurations, the topological invariant (2.43) coincides exactly with the Yang-Mills action (2.40). In general, the Euclidean Yang-Mills action (2.37) is given by the topological term (2.43) plus a sum of bilinears in the strength field. The *minimal-action* configuration within a given topological sector of topological charge k is thus given by (anti) selfdual field configurations with action $\mathcal{S} = \frac{8\pi^2}{g^2} |k|$.

2.2.2 Topological classification

Here we introduce some terminology we will make use of later while discussing $SU(2)$ Yang-Mills thermodynamics in chapter 3. Following Gross, Pisarski and Yaffe [21], classical gauge field configurations in Euclidean space-time with finite action can be classified according to topological charge, holonomy and magnetic charge.

Topological charge

As we saw in the preceding section, a well defined index k , topological in nature, can be defined as

$$8\pi^2 k \equiv \frac{1}{4} \int d^4x F^{a\mu\nu} \tilde{F}_{\mu\nu}^a. \quad (2.43)$$

This expression divides different field configurations into *topological sectors* classified by the integer k .

Let us summarize here the results of the preceding section. In each topological sector k , the configuration with minimal Euclidean action (2.37) is given by the solutions to the selfdual equations (2.35). The Yang-Mills equations of motion are automatically satisfied for selfdual fields, thus reducing second order field equations of the type (2.31), (2.32) to the first order selfdual equation (2.35). Selfdual field configurations in Euclidean space-time *cannot propagate*, since they have a vanishing energy-momentum tensor (2.38).

Holonomy

The *holonomy* of a field configuration is given by the eigenvalues of the *Polyakov loop* defined as a time-like *Wilson loop* L

$$L(\vec{x}) = \mathcal{P} \exp i \int_0^\beta d\tau A_4(\tau, \vec{x}), \quad (2.44)$$

where \mathcal{P} denotes path ordering and A_4 is the Euclidean-rotated gauge field (2.36).

Magnetic charge

The magnetic charge is defined as the coefficient m in the expression for the *magnetic flux* $\mathbf{B} = m \frac{\mathbf{r}}{|\mathbf{r}|^3}$, evaluated at spatial infinity [8].

2.3 Thermal field theory

Recall from quantum statistical mechanics that the *grand canonical partition function* $Z(\beta)$ for a quantum system, which is defined by the Hamilton operator \hat{H} and vanishing chemical potential $\mu = 0$, can be written as an integral over a complete set of eigenfunctions $|q\rangle$ of \hat{H}

$$Z(\beta) = \text{tr} e^{-\beta \hat{H}} = \int dq \langle q | e^{-\beta \hat{H}} | q \rangle, \quad (2.45)$$

where as usual $\beta \equiv 1/T$ is the inverse temperature. It can be shown [35, 42] that by rotating to *Euclidean space-time* (2.36), the partition function (2.45) for a quantum field $q(x)$ can be written as a transition amplitude by integrating over all field configurations that periodic in Euclidean time. In the case of pure SU(2) Yang-Mills theory, the role of $q(x)$ is played by the gauge field $A_\mu(x)$, rotated to Euclidean time. The *pure Yang-Mills partition function* is then given by

$$Z \equiv \int_{A_\mu(0, \vec{x})=A_\mu(\beta, \vec{x})} \mathcal{D}A_\mu e^{-S_{YM}^E}, \quad (2.46)$$

where the field configurations are Lie-Algebra valued $A_\mu \equiv A_\mu^a t_a$ with group generators t_a normalized as usual, and the Euclidean Yang-Mills action S_{YM}^E was defined in (2.37). Integration (2.46) goes over all periodic field configurations $A_\mu(\tau = 0, \vec{x}) = A_\mu(\tau = \beta, \vec{x})$. In this formalism, the Euclidean space-time \mathbb{R}^4 goes over to the Euclidean torus $\mathbb{R}^4 \rightarrow S_1 \times \mathbf{R}^3$. Selfdual solutions on $\mathbb{R}^4 \rightarrow S_1 \times \mathbf{R}^3$ are called *calorons*.

Expression (2.46) is used to derive other thermodynamical quantities such as the pressure, energy, etc. Perturbatively, the partition function $\ln Z$ can be expanded in *bubble diagrams*. Further details can be found in the literature [35, 42].

Chapter 3

SU(2) Yang-Mills Thermodynamics in the Deconfining Phase

In this chapter, we review a nonperturbative approach to the thermodynamics of the SU(2) Yang-Mills gas developed in [25, 29]. It is shown in [25] that such an approach results in three distinct thermodynamical phases: confining, preconfining and deconfining. Each phase is characterized by the emergence of a scalar field describing the thermal ground state dynamics. In this thesis we are interested in the physics of the deconfining phase, and the possibility of experimental detection of ground state effects in this regime. Experimental evidence for SU(2) dynamics hinges on the appearance of a *frequency cutoff* ν^* below which thermal propagation of the SU(2) photon is forbidden. This effect can be detected by measuring the *antenna temperature* of an antenna immersed into a thermalized photon gas. The radiometry of the SU(2) photon is discussed in chapter 5.

This chapter is structured as follows. In section 3.1 we briefly review the nonperturbative approach to the deconfining phase, outlining the basic assumptions and results. Section 3.2 introduces the resulting *effective theory* and some of its consequences, for example, the emergence of nonzero *vacuum energy*. In section 3.3 we list the basic thermal excitations of the theory and give the *Feynman rules* necessary to calculate effective radiative corrections. The purpose of this introductory review is not to give a complete description of the theoretical approach in [25, 29], but to introduce the concepts and mathematical results necessary for an understanding of the physics behind the ν^* cutoff.

In section 3.4 we review the hypothesis that thermalized photon propagation is described by the tree-level massless mode of a Yang-Mills SU(2) theory in the deconfining phase. This hypothesis fixes the critical temperature of the deconfining phase to be slightly lower than the baseline CMB temperature $T_{\text{CMB}} = 2.726\text{K}$.

Our own results are presented in the last two sections. In section 3.5 we calculate radiative corrections to the *propagation of massless modes*, both transverse and longitudinal. A formula for the temperature-dependent frequency cutoff $\nu^*(T)$ of the transverse polarization is derived, and the longitudinal polarization is shown to be nonpropagating. Finally, section 3.6 is dedicated to a discussion of thermal resummation and thermodynamical consistency.

3.1 A nonperturbative approach to Yang-Mills thermodynamics

The sector of topologically nontrivial, selfdual, nonpropagating pure Yang-Mills configurations on $S_1 \times \mathbf{R}^3$ Euclidean space-time (calorons) is in general not accessible by perturbation methods. The quantum amplitude \mathcal{A} of such configurations is non-analytic in the coupling constant g , $\mathcal{A} \sim \exp(-\frac{8\pi^2}{g^2})$, and thus missed at all orders of perturbation theory.

A thermodynamical approach to this problem was developed in [25, 29] that solves this difficulty by integrating out topologically nontrivial degrees of freedom through a spatial coarse-graining over such field configurations. This results in an effective theory containing topologically trivial excitations interacting with an effective *macroscopic scalar field* ϕ^a living in the adjoint representation of the gauge group $SU(2)$. The field ϕ^a also introduces with itself a *mass scale* Λ which is the only parameter of the theory.

The effective theory features a thermal ground state above which topologically trivial excitations fluctuate. In order to construct such an effective theory two basic constraints for infinite-volume thermodynamics should be obeyed [25]. First, in the absence of external perturbations, any nonzero field resulting from the ensemble average and spatial coarse-graining over nonpropagating field configurations must be, (modulo gauge transformations), *spatially homogeneous and isotropic*. Furthermore, such a field can only be constant over all space, and rotationally invariant. Similarly, the gauge invariant field resulting from such averaging and coarse-graining operations cannot explicitly depend on time. The basic considerations leading us to the unique definition of a macroscopic scalar field are sketched in this section.

3.1.1 Basic roadmap

The nonperturbative approach to $SU(2)$ Yang-Mills Thermodynamics developed in [25, 29] *uniquely derives* an effective field theory starting from the fundamental Euclidean Yang-Mills action considered in the thermodynamical limit of infinite volume. Here, we summarize the main line of analysis underlying the emergence of a macroscopic scalar field [47].

1. Consider the topologically nontrivial, selfdual sector of periodic Euclidean field configurations. Independently of their topological parameters, these field excitations have a vanishing (classical) energy-momentum tensor, and thus do not describe propagating degrees of freedom.
2. Let a Lorentz invariant gauge multiplet ϕ^a be defined by coarse-graining over such configurations in 1. The multiplet ϕ^a is thus by construction *nonpropagating* (recall section 2.2.1). But this means ϕ^a acts as a *static, spatially homogeneous* background.
3. Spatial isotropy would be broken by such a Lorentz tensor unless ϕ^a were a *scalar field*. Further, spatial homogeneity requires that the scalar field ϕ^a have a *constant modulus* $|\phi|$. Since ϕ^a by construction cannot propagate and emerges by coarse-graining over periodic configurations in Euclidean time, its equation of motion produces – in a given gauge – an Euclidean-time periodic phase $\hat{\phi}^a(\tau + \beta) = \hat{\phi}^a(\tau)$ with no space dependence. Also, since the *classical action* of selfdual configurations with topological charge k is *independent of temperature* β^{-1} , $S = \frac{8\pi^2|k|}{g^2}$ (see 2.2.1), *no explicit β dependence* is allowed in the definition of $\hat{\phi}^a$. Finally, if the scalar gauge

multiplet is thermalized with the sector of trivial topological charge $k = 0$, it must carry charge under the gauge group $SU(2)$ (that is, transform nontrivially under gauge rotations). Then the index a is just a $SU(2)$ valued *color* index.

4. It can be shown [23] that there exists a *unique construction* for a family of phases $\{\hat{\phi}^a\}$ living in the *adjoint* representation satisfying the conditions described in 3. This construction is necessarily nonlocal, and only admits contributions from $|k| = 1$ (Harrington-Shepard) (anti)calorons of trivial holonomy. Non-trivial holonomy calorons can be *a priori excluded* from contributing to ϕ^a since such configurations are known to be unstable under trivial-topology fluctuations [9] (The average Polyakov line is zero, $\langle \text{tr} L \rangle = 0$ [8]). Configurations of topological charge $|k| > 1$ are also excluded, by Lorentz symmetry arguments [23] so that ϕ^a emerges from spatial coarse graining over only *trivial holonomy calorons of topological charge $|k| = 1$* . It turns out that the set $\{\hat{\phi}^a\}$ defines the kernel of - and *completely determines* a - second order differential operator \mathcal{D} . The fact that the scalar field ϕ^a both has vanishing Euclidean energy density and belongs to the kernel of \mathcal{D} can be exploited to *fix the gauge invariant effective potential $V(\phi)$ uniquely* for ϕ^a . This action also introduces a mass scale as an integration constant, the *Yang-Mills scale* Λ .
5. Since no object other than the inert adjoint scalar field ϕ^a may emerge from the sector of topologically nontrivial fundamental configurations, the coupling of ϕ^a with the sector of zero topological charge must be minimal. That is, it should be realized via a covariant derivative $D_\mu = \partial_\mu + a_\mu$. Higher dimensional operators are forbidden by perturbative renormalizability [25].

Thus, we arrive at a scalar field ϕ and an effective Lagrangian \mathcal{L}_{eff} describing interactions with the sector of topologically trivial charge $k = 0$. The *effective theory* described by the scalar field ϕ and the Lagrangian \mathcal{L}_{eff} is discussed in some detail in the next sections.

3.2 $SU(2)$ thermal ground state in the deconfining phase

3.2.1 Inert adjoint scalar field

As described in 3.1.1, upon *spatial coarse graining* over the caloron sector of the *fundamental* $SU(2)$ theory a Lorentz invariant multiplet ϕ^a is generated which describes ground state physics up to a phase transition temperature given by the Yang-Mills scale of the theory. The *modulus* of ϕ^a does not depend on space or time, and is given by

$$|\phi| \equiv \sqrt{\frac{1}{2} \text{tr} \phi^2} \tag{3.1}$$

$$= \sqrt{\frac{\Lambda^3 \beta}{2\pi}}, \tag{3.2}$$

with the inverse temperature $\beta \equiv \frac{1}{T}$. The *equations of motion* ruling over the dynamics of ϕ^a are derived from an (effective) Euclidean Lagrangian of the form

$$\mathcal{L}_\phi = \text{tr} \left[(\partial_\tau \phi)^2 + V(\phi^2) \right], \tag{3.3}$$

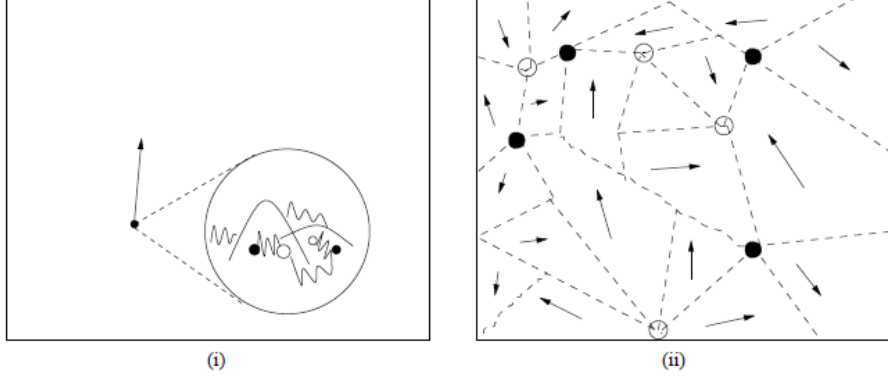


Figure 3.1: A spatially homogeneous and isotropic static field ϕ^a is generated by spatial coarse-graining over interacting calorons of trivial holonomy and topological charge $|k| = 1$, shown in (i) as fluctuations inside a spherical integration volume. The inert field ϕ^a and the pure-gauge configuration a_μ^{gs} which solves the effective Yang-Mills equations together define a *thermal ground state*. (ii) depicts domainization occurring from interactions between calorons. Domain walls intersections are identified as *magnetic monopoles*. Domainization effects can be taken into account by loop-expanding the quantity under investigation about the thermal ground state in the effective theory. Figure taken from [32].

the potential V is given by the expression

$$V(\phi) = \text{tr} \frac{\Lambda^6}{\phi^2}, \quad (3.4)$$

with the inverse of the scalar field defined as $\phi^{-1} \equiv \frac{\phi}{|\phi|^2}$. The *mass scale* Λ emerges as an integration constant and serves as the *Yang-Mills scale* of the theory, defining a phase transition temperature $T_c \equiv \lambda_c \frac{\Lambda}{2\pi}$ which bounds the deconfining phase from below. The *critical dimensionless temperature* λ_c is defined by the evolution of the gauge coupling $e(\lambda)$ in the *effective theory* (see section 3.2.2). At λ_c , the gauge coupling exhibits a logarithmic singularity so that $e(\lambda) = -4.59 \log(\lambda - \lambda_c) + 18.42$. Numerically, $\lambda_c = 13.87$ [31]. The transition temperature T_c is the *only parameter of the theory*. To make contact with experiment, this parameter must be fixed so that quantitative calculations may be performed. This will be done in section 3.4.

Up to global gauge transformations, a solution to the Euler-Lagrange equations of motion determined by (3.3) and (3.4) is given by

$$\phi = 2 \sqrt{\frac{\Lambda^3 \beta}{2\pi}} t_1 \exp(\pm \frac{4\pi i}{\beta} t_3 \tau). \quad (3.5)$$

The field ϕ represents a spatially homogeneous background for the dynamics of coarse-grained, propagating, trivial-topology gauge fields. It will also *break the gauge symmetry* $SU(2)$ down to its Abelian subgroup $U(1)$. The effect of this symmetry breaking will be to confer a temperature-dependent mass to two of the three available vector modes. This is discussed in section 3.3.1.

3.2.2 Effective action and bare thermal ground state

In section 3.1.1, it was shown how to construct a scalar field resulting from spatial coarse-graining over Harrington-Shepard calorons. The procedure integrates out the topologically nontrivial sector of the fundamental theory. The dynamics of the topologically trivial remainder is then determined by an effective theory valid up to a scale $|\phi|$, characterized by an effective Lagrangian \mathcal{L}_{eff} describing the interaction of the scalar field ϕ with the topologically trivial sector ($k = 0$). It has been shown [25] that \mathcal{L}_{eff} can be uniquely defined – up to a *maximal energy resolution* $|\phi|$ – and is given by

$$\mathcal{L}_{\text{eff}}[a_\mu] = \text{tr} \left(\frac{1}{2} G_{\mu\nu} G_{\mu\nu} + (D_\mu \phi)^2 + \frac{\Lambda^6}{\phi^2} \right), \quad (3.6)$$

where $a_\mu = a_\mu^a t_a$ is a propagating, trivial-topology gauge field in the adjoint representation remaining after coarse-graining. The *effective field strength* is defined as usual

$$G_{\mu\nu} \equiv \partial_\mu a_\nu - \partial_\nu a_\mu - ie[a_\mu, a_\nu] = G_{\mu\nu}^a t_a, \quad (3.7)$$

with e the *effective gauge coupling*. The effective coupling constant e is not the same as the coupling constant of the fundamental theory. The evolution of this coupling constant as function of dimensionless temperature $e(\lambda)$ follows from demanding thermodynamical consistency [25]. As already mentioned, the coupling behaves logarithmically at the *critical temperature* λ_c , $e(\lambda)|_{\lambda_c} \sim -\log(\lambda - \lambda_c)$, and the theory undergoes a *second order phase transition* to the preconfining phase. We remark here that, for temperatures higher than λ_c , local gauge transformations can always be found such that the Polyakov loop $\text{Pol}[a_\mu^{\text{bg}}]$ is transformed from $\text{Pol} = -\mathbf{1}_2$ to $\text{Pol} = \mathbf{1}_2$. This reflects the electric \mathbf{Z}_2 degeneracy of the thermal ground state estimate, and the theory for $\lambda > \lambda_c$ is thus *deconfining*. Further details can be found in the literature [25, 29]. The covariant derivative D_μ imposes *minimal coupling* between the effective $k = 0$ gauge field and the $|k| = 1$ coarse-grained inert scalar field, and is written as

$$D_\mu \phi = \partial_\mu \phi - ie[a_\mu, \phi]. \quad (3.8)$$

Note how the effective action in (3.6) at resolution $|\phi|$ splits into a classical Yang-Mills term describing the propagation and interactions among topologically trivial fluctuations, an interaction term between $k = 0$ and $|k| = 1$ configurations given by the square of the covariant derivative acting on ϕ , $(D_\mu \phi)^2$ (Higgs mechanism for two out of three propagating directions in the $SU(2)$ algebra), and a potential V for the field ϕ [25].

The Euler-Lagrange equations governing the effective theory can be read from the Lagrangian (3.6)

$$D_\mu G_{\mu\nu} = ie[\phi, D_\nu \phi]. \quad (3.9)$$

The inert scalar ground state configuration (3.5) and the *pure gauge configuration*

$$a_\mu^{\text{gs}} = \mp \delta_{\mu 4} \frac{2\pi}{e\beta} t_3, \quad (3.10)$$

are *ground state solutions* of (3.9) since $G_{\mu\nu}[a_\kappa^{\text{gs}}] = D^\nu[a_\kappa^{\text{gs}}]\phi = 0$. Apart from (small) radiative corrections and up to global gauge transformations, (3.5) and (3.10) constitute a

good first estimate of the thermal ground state of the effective theory in the deconfining phase. Accordingly, a good first estimate of the *energy density of the thermal ground state* is given by

$$\rho^{\text{gs}} \equiv \mathcal{L}_{\text{eff}}[a_\mu^{\text{gs}}] = \text{tr} \frac{\Lambda^6}{\phi^2} = 4\pi\Lambda^3 T, \quad (3.11)$$

which is interpreted as a temperature dependent cosmological constant. Together, ϕ and a_μ^{gs} represent an *a priori estimate of the bare thermal ground state* which turns out to be quite accurate.

For later use, we write (3.11) in SI units. The temperature T is rescaled as $T \rightarrow k_B T$, the mass scale Λ as $\Lambda \rightarrow \frac{\Lambda}{\hbar c}$, and the *energy density of the thermal ground in the deconfining phase* depends on the temperature through the expression

$$\rho^{\text{gs}} = 4\pi \left(\frac{\Lambda}{\hbar c} \right)^3 k_B T. \quad (3.12)$$

This energy density will later serve as a criterion for thermodynamical consistency in the presence of external fields.

3.3 Thermal quasiparticles and Feynman rules

3.3.1 Mass spectrum

In the effective theory of deconfining Yang-Mills thermodynamics, each broken generator t_a of the original gauge symmetry, causes the original massless mode associated with t_a to acquire a mass m_a [29]

$$m_a^2 = -2e^2 \text{tr} [\phi, t_a]^2. \quad (3.13)$$

To interpret (3.13) physically, we impose *unitary gauge* for the thermal ground state

$$\phi = 2|\phi|t_3, \quad (3.14a)$$

$$a_\mu^{\text{gs}} = 0. \quad (3.14b)$$

In this gauge we have

$$m \equiv m_1 = m_2 = 2e(\lambda)|\phi| = 2\Lambda \frac{e(\lambda)}{\sqrt{\lambda}} = 2\Lambda e \left(\frac{2\pi}{\Lambda} T \right) \sqrt{\frac{\Lambda}{2\pi T}}, \quad (3.15a)$$

$$m_3 = 0. \quad (3.15b)$$

In the fundamental theory, all gauge modes are massless, while in the effective theory two of the three gauge modes acquire mass at tree-level. Note that the mass m in (3.15a) is temperature-dependent. Recall that, at the critical temperature $\lambda_c \equiv \frac{2\pi}{\Lambda} T_c$, the effective coupling $e(\lambda)$ shows a logarithmic singularity $e(\lambda)|_{\lambda_c} \sim -\log(\lambda - \lambda_c)$ for $\lambda \searrow \lambda_c$. This signals a phase transition to the preconfining regime. Near this critical temperature, the mass m in (3.15a) diverges, and interactions between massless and massive modes decouple. That is, radiative corrections to (3.15b) becomes exactly zero.

The unbroken gauge subgroup $U(1)$ is responsible for the remaining *massless* mode after coarse-graining. It is this remaining symmetry, and the vanishing of radiative corrections to (3.15b) at T_c , that will lead us to speculate about the fundamental origin of the Standard Model photon (see section 3.4).

But first, we review the Feynman rules in the effective theory.

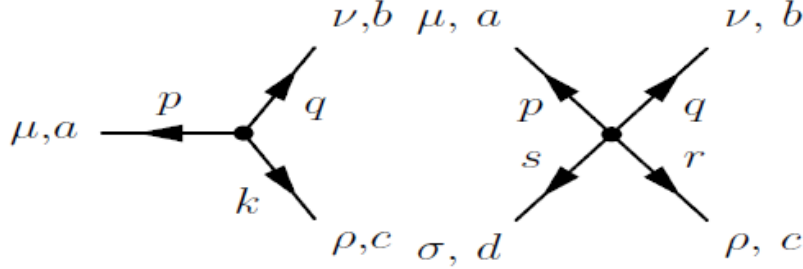


Figure 3.2: 3- and 4- vertices. Taken from [59]

3.3.2 Finite temperature Feynman rules in unitary gauge

In unitary-Coulomb gauge, which is a physical, completely fixed gauge, the real-time propagators of the fields are obtained by a Wick rotation to real time¹ of the usual Matsuraba imaginary time propagators [35, 41, 42]. In the real-time formulation of finite-temperature field theory [41] it is possible to discern quantum from thermal fluctuations. To tell the former from the latter is necessary since quantum fluctuations away from the mass-shell will be limited by the physical resolution $|\phi|$ in the unitary-Coulomb gauge. Also, the fields $a_\mu^{1,2}$ may only propagate thermally [25]. The Feynman rules for the $SU(2)$ vertices are taken from the literature as well, by substituting the fundamental gauge constant $g \rightarrow e$.

To conform with the nomenclature of [59] we refer to the fluctuative $SU(2)$ directions 1 and 2 as tree-level heavy (TLH) and to direction 3 as tree-level massless (TLM). In unitary-Coulomb gauge (3.14) the *real-time bare thermal propagators* in momentum space are then given by [59]

$$D_{ab,\mu\nu}^{\text{TLH},0}(p) = -\delta_{ab} \tilde{D}_{\mu\nu} [2\pi\delta(p^2 - m^2)n_B(|p_0|/T)] , \quad (3.16)$$

$$D_{ab,\mu\nu}^{\text{TLM},0}(p) = -\delta_{ab} \left\{ P_{\mu\nu}^T \left[\frac{i}{p^2} + 2\pi\delta(p^2)n_B(|p_0|/T) \right] - i \frac{u_\mu u_\nu}{\mathbf{p}^2} \right\} , \quad (3.17)$$

where $n_B(x) = 1/(e^x - 1)$ denotes the Bose-Einstein distribution function and

$$\tilde{D}_{\mu\nu} = \left(g_{\mu\nu} - \frac{p_\mu p_\nu}{m^2} \right) . \quad (3.18)$$

The four-vector $u_\mu = (1, 0, 0, 0)$ specifies the restframe of the thermal bath and the *3-space transverse* projection operator $P_T^{\mu\nu}$ is defined as

$$P_T^{00} = P_T^{0i} = P_T^{i0} = 0 , \quad (3.19)$$

$$P_T^{ij} = \delta^{ij} - p^i p^j / \mathbf{p}^2 . \quad (3.20)$$

TLM modes carry a color index 3 while TLH modes have a color index 1 and 2. The three-

¹This method becomes problematic for self interactions and loop calculations of higher order than two [11]. It has been shown that such difficulties do not apply to our approach to $SU(2)$ thermodynamics [26]. Note also that a change of signature from Euclidean to Minkowskian is trivial as far as the physics of the ground state estimate of section 3.2.2 and the associated dynamical gauge-symmetry breaking are concerned: neither ground state pressure, energy density or quasiparticle mass depend on Euclidean time.

and four-gauge-boson vertices are given as (see figure 3.2)

$$\Gamma_{[3]abc}^{\mu\nu\rho}(p, q, k) = e(2\pi)^4 \delta(p + q + k) \epsilon_{abc} \times [g^{\mu\nu}(q - p)^\rho + g^{\nu\rho}(k - q)^\mu + g^{\rho\mu}(p - k)^\nu] \quad (3.21)$$

$$\begin{aligned} \Gamma_{[4]abcd}^{\mu\nu\rho\sigma}(p, q, s, r) = & -ie^2(2\pi)^4 \delta(p + q + s + r) [\\ & \epsilon_{abe}\epsilon_{cde}(g^{\mu\rho}g^{\nu\sigma} - g^{\mu\sigma}g^{\nu\rho}) \\ & + \epsilon_{ace}\epsilon_{bde}(g^{\mu\nu}g^{\rho\sigma} - g^{\mu\sigma}g^{\nu\rho}) \\ & + \epsilon_{ade}\epsilon_{bce}(g^{\mu\nu}g^{\rho\sigma} - g^{\mu\rho}g^{\nu\sigma})]. \end{aligned} \quad (3.22)$$

Finally, recall that, before calculation, each loop-diagram has to be divided by i and the number of its vertices (symmetry factor) [41].

The maximal off-shellness of effective gauge modes as well as the momentum transfer in four-vertices are constrained by coarse-graining down to a resolution $|\phi|$ [25, 28]. TLM modes (3.17) may never be off-shell beyond

$$|p^2| \leq |\phi|^2. \quad (3.23)$$

TLH modes on the other hand may only fluctuate thermally, that is, on-shell. Condition (3.23) *also fixes the momentum transfer* in a three-vertex by momentum conservation. Momentum transfers in an effective four vertex cannot be larger than $|\phi|^2$ [25].

We now have all the information on hand that we need to calculate in the effective thermal theory. The only step left is to *fix the scale* Λ so that we may get quantitative results. This is achieved by identifying the Standard Model $U(1)$ propagating photon with the massless $SU(2)$ mode in the effective theory. This is discussed in section 3.4.

Afterwards, we introduce the polarization tensor for the TLM mode, and proceed to calculate its influence on photon propagation. This is the subject of section 3.5.

3.4 The $SU(2)_{\text{CMB}}$ hypothesis and some implications

The nonperturbative approach to the thermodynamics of the $SU(2)$ Yang-Mills gas reviewed in the preceding sections can now be summarized as follows: An adjoint scalar field ϕ^a is defined by coarse-graining over trivial-holonomy field configurations with topological charge $|k| = 1$. A thermal ground state composed of ϕ^a and the pure-gauge field configuration a_μ^{gs} , considered together with topologically trivial ($|k| = 0$) gauge field fluctuations, is seen to *effectively* describe the fundamental $SU(2)$ Yang-Mills theory at finite-temperature. In the effective theory, two of the three fundamental gauge modes of the local $SU(2)$ symmetry become massive due to ϕ^a by the Higgs mechanism. The remaining $U(1)$ symmetry is responsible for the masslessness of the third gauge mode.

At this point, it is worthwhile to consider whether this symmetry is realized in nature. An intriguing possibility is the identification with the $U(1)_Y$ gauge group of the Standard Model. As argued in [17, 24, 27, 30, 58], this would immediately fix the critical temperature T_c with the cosmic microwave background temperature $T_{\text{CMB}} = 2.725 \text{ K}$. It follows for the

$SU(2)$ Yang-Mills scale

$$\begin{aligned}\Lambda \equiv \Lambda_{\text{CMB}} &= 2\pi \frac{k_B T_c}{\lambda_c} = 2\pi \frac{k_B T_{\text{CMB}}}{\lambda_c} \\ &= 1.70433 \cdot 10^{-23} \text{ J} \\ &= 1.06376 \cdot 10^{-4} \text{ eV},\end{aligned}\tag{3.24}$$

with $\lambda_c = 13.87$. Once we have fixed the Yang-Mills scale $\Lambda \equiv \Lambda_{\text{CMB}}$ we can proceed to calculate the polarization tensor of the TLM mode. This is done in the next section.

3.5 Polarization tensor and photon propagation

Having identified the massless mode of the coarse-grained effective theory with the familiar $U(1)$ photon, we now proceed to investigate what effect the existence of a thermal ground state may have in the physics of photon propagation. We expect the thermal ground state to interact with the massless mode via the massive vectors. This interaction is encoded in the *polarization tensor* $\Pi^{\mu\nu}(p_0, \vec{p})$, which we compute perturbatively at one-loop level. The rest of the chapter is dedicated to the main results of this computation.

3.5.1 Prerequisites

The dispersion relations for the massless gauge modes are given by the poles of the full thermal propagator $D_{ab,\mu\nu}^{TLM}(k)$. In general, any *dressed* thermal propagator $\mathcal{D}_{\mu\nu}$ can be written as the geometric series

$$\mathcal{D}_{\mu\nu} = \mathcal{D}_{\mu\nu}^0 + \mathcal{D}_{\mu\sigma}^0 \Pi^{\sigma\rho} \mathcal{D}_{\rho\nu}^0 + \dots,\tag{3.25}$$

where $\mathcal{D}_{\mu\nu}^0$ is the bare thermal propagator and the *polarization tensor* $\Pi^{\mu\nu}$ is defined as the sum of *one-particle irreducible* (1PI) diagrams with 2 external lines [53]. The series (3.25) can be written as

$$\mathcal{D}_{\mu\nu} = \mathcal{D}_{\mu\nu}^0 + \mathcal{D}_{\mu\sigma}^0 \Pi^{\sigma\rho} \mathcal{D}_{\rho\nu}^0.\tag{3.26}$$

Defining the inverse propagator as $\mathcal{D}_{\mu\sigma}^{-1} \mathcal{D}^{\sigma\nu} = g_\mu{}^\nu$, we get an equation for the polarization tensor

$$\Pi_{\mu\nu} = \mathcal{D}_{\mu\nu}^{-1} - \mathcal{D}_{\mu\nu}^{0-1}.\tag{3.27}$$

Further, $\Pi^{\mu\nu}$ is transverse [41]

$$p^\mu \Pi_{\mu\nu} = 0.\tag{3.28}$$

Here, p^μ is the 4-momentum vector of the thermal excitation. By separating the space-time transverse projector operator

$$P^{\mu\nu} \equiv g^{\mu\nu} - p^\mu p^\nu / p^2,\tag{3.29}$$

in the space transverse projector P_T and space longitudinal projector P_L

$$\begin{aligned}P_T^{00} &= P_T^{0i} = P_T^{i0} = 0, \\ P_T^{ij} &= \delta^{ij} - p^i p^j / \mathbf{p}^2, \\ P_L^{\mu\nu} &= -P^{\mu\nu} - P_T^{\mu\nu},\end{aligned}\tag{3.30}$$

we can expand the space-time transverse polarization tensor $\Pi_{\mu\nu}$ as

$$\Pi_{\mu\nu}(p_0, \mathbf{p}) = G(p_0, \mathbf{p})P_{T\mu\nu} + F(p_0, \mathbf{p})P_{L\mu\nu}, \quad (3.31)$$

with scalar functions G and F . Before analytic continuation from imaginary time, the full interacting propagator $D_{ab,\mu\nu}^{TLM}(k)$ for the massless mode of the effective theory can be written in the *Coulomb gauge* in the Euclidean formulation as the linear combination [35, 59]

$$D_{ab,\mu\nu}^{TLM}(p) = -\delta_{ab} \left\{ P_{\mu\nu}^T \frac{1}{G - p^2} + \frac{p^2}{\mathbf{p}^2} \frac{1}{F - p^2} u_\mu u_\nu \right\}, \quad (3.32)$$

where $u^\mu = (1, 0, 0, 0)$ specifies the *restframe* of the many-body system. Note that, as expected, while the first term in the right hand side of expression (3.32) describes *transverse propagation*, $P_T^{\mu\nu} D_{\mu\nu}^{TLM} \sim (G - p^2)^{-1}$, the second term describes *longitudinal propagation* $P_L^{\mu\nu} D_{\mu\nu}^{TLM} \sim (F - p^2)^{-1}$. The corresponding *dispersion relations* are then determined for all modes by the poles of (3.32). For the *transverse modes*, this results in

$$p_0^2 = \mathbf{p}^2 + G(p_0, \mathbf{p}). \quad (3.33)$$

Separate $p_0 = \omega - i\gamma$, and assume *weak damping* $\gamma/\omega \ll 1$. The *transverse dispersion relation* is then given by

$$\omega^2(\mathbf{p}) = \text{Re } p_0^2 = \mathbf{p}^2 + \text{Re } G(\omega(\mathbf{p}), \mathbf{p}), \quad (3.34)$$

$$\gamma(\mathbf{p}) = \text{Im } p_0^2 = -\frac{1}{2\omega(\mathbf{p})} \text{Im } G(\omega(\mathbf{p}), \mathbf{p}). \quad (3.35)$$

Similarly, for the longitudinal mode

$$\omega_L^2(\mathbf{p}) = \mathbf{p}^2 + \text{Re } F(\omega_L(\mathbf{p}), \mathbf{p}), \quad (3.36)$$

$$\gamma_L(\mathbf{p}) = -\frac{1}{2\omega_L(\mathbf{p})} \text{Im } F(\omega_L(\mathbf{p}), \mathbf{p}), \quad (3.37)$$

where we added the subscript L to differentiate from the transverse relations. Taking \mathbf{p} parallel to the z -axis, we can extract from (3.31) expressions for the scalar functions G , F as components of $\Pi_{\mu\nu}$

$$G(\omega(\mathbf{p}), \mathbf{p}) = \Pi_{11}(\omega(\mathbf{p}), \mathbf{p}) = \Pi_{22}(\omega(\mathbf{p}), \mathbf{p}), \quad (3.38)$$

$$F(\omega_L(\mathbf{p}), \mathbf{p}) = \frac{p^2}{\mathbf{p}^2} \Pi_{00}. \quad (3.39)$$

3.5.2 Polarization tensor at the one-loop level

In order to calculate the polarization tensor one has to sum all 1PI diagrams to the required precision. Figure 3.3 shows the diagrams contributing to the photon polarization tensor $\Pi^{\mu\nu}$ at the one-loop level as a function of incoming momentum p . The total polarization tensor is just the sum of the two diagrams

$$\Pi^{\mu\nu}(p) = \Pi_A^{\mu\nu}(p) + \Pi_B^{\mu\nu}(p). \quad (3.40)$$

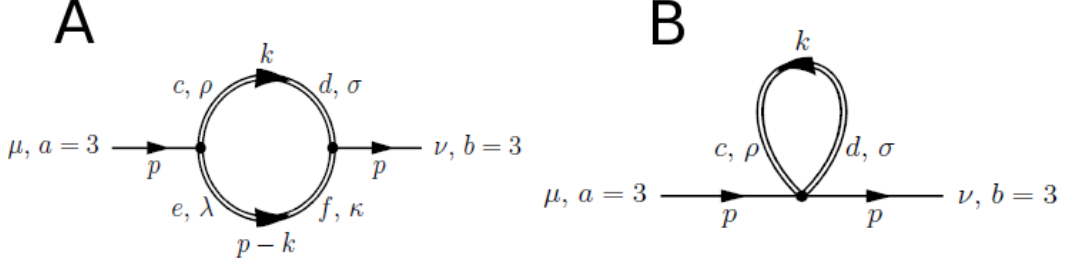


Figure 3.3: The photon is represented by single-line propagators, double-line propagators correspond to massive modes. Taken from [59].

Diagram A can be written by following the Feynman rules described in section 3.3.2, which results in

$$\begin{aligned}
 \Pi_A^{\mu\nu}(p) = & \frac{1}{2i} \int \frac{d^4k}{(2\pi)^4} e^2 \epsilon_{ace} [g^{\mu\rho}(-p-k)^\lambda + g^{\rho\lambda}(k-p+k)^\mu + g^{\lambda\mu}(p-k+p)^\rho] \\
 & \times (-\delta_{cd}) \left(g_{\rho\sigma} - \frac{k_\rho k_\sigma}{m^2} \right) \left[\frac{i}{k^2 - m^2} + 2\pi\delta(k^2 - m^2) n_B(|k_0|/T) \right] \\
 & \times \epsilon_{dbf} [g^{\sigma\nu}(-k-p)^\kappa + g^{\nu\kappa}(p+p-k)^\sigma + g^{\kappa\sigma}(-p+k+k)^\nu] \\
 & \times (-\delta_{ef}) \left(g_{\lambda\kappa} - \frac{(p-k)_\lambda(p-k)_\kappa}{(p-k)^2} \right) \\
 & \times \left[\frac{i}{(p-k)^2 - m^2} + 2\pi\delta((p-k)^2 - m^2) n_B(|p_0 - k_0|/T) \right].
 \end{aligned} \tag{3.41}$$

Here $m = 2e|\phi| = 2e\sqrt{\Lambda^3/2\pi T}$ is the induced mass of the two other gauge modes in the effective theory (see (3.15)), and $n_B(x)$ is the Bose-Einstein function.

Diagram B is associated with the following expression

$$\begin{aligned}
 \Pi_B^{\mu\nu}(p) = & \frac{1}{i} \int \frac{d^4k}{(2\pi)^4} (-\delta_{ab}) \left(g_{\rho\sigma} - \frac{k_\rho k_\sigma}{m^2} \right) [2\pi\delta(k^2 - m^2) n_B(|k_0|/T)] \\
 & \times (-ie^2) [\epsilon_{abe}\epsilon_{cde}(g^{\mu\rho}g^{\nu\sigma} - g^{\mu\sigma}g^{\nu\rho}) \\
 & + \epsilon_{ace}\epsilon_{bde}(g^{\mu\nu}g^{\rho\sigma} - g^{\mu\sigma}g^{\nu\rho}) + \epsilon_{ade}\epsilon_{bce}(g^{\mu\nu}g^{\rho\sigma} - g^{\mu\rho}g^{\nu\sigma})].
 \end{aligned} \tag{3.42}$$

As shown in [46], G and F may be calculated selfconsistently by numerical methods from this expressions for the polarization tensor. This is described in the following sections.

3.5.3 Transversal modes

Transversal propagation is determined by the scalar function $G(\omega, \mathbf{p})$, which can be calculated from the polarization tensor by use of equation (3.38). In both (3.41) and (3.42), the *off-shellness* of the k integration is restricted in the effective theory by the maximal resolution $|\phi|$ after coarse-graining, see (3.23). This results in the *support condition*

$$|(p+k)^2| = |G + 2p \cdot k + 4e^2|\phi|^2| \leq |\phi|^2 = \frac{\Lambda^3}{2\pi T}, \tag{3.43}$$

where we have used $p^2 = G$ and $k^2 = 4e^2|\phi|^2$. The k integration in (3.41) and (3.42) is to be taken over all values of k such that (3.43) is fulfilled. It can be shown that diagram A, which is given by equation (3.41), is identically zero over the support (3.43) [46]. Since (3.41) is the only imaginary contribution at the one-loop level, there is no finite transverse photon width (3.35).

The scalar function $G(\omega, \mathbf{p})$ can then be calculated up to one-loop from diagram B, that is equation (3.42), by integrating over the support determined by the inequality (3.43). To evaluate (3.42), transform the integral to dimensionless variables

$$\xi \equiv \frac{k_3}{|\phi|}, \quad \rho \equiv \frac{1}{|\phi|} \sqrt{k_1^2 + k_2^2}, \quad \varphi \equiv \arctan \frac{k_2}{k_1}. \quad (3.44)$$

Equation (3.38) gives G when \mathbf{p} is taken parallel to the z -axis. Recall the definition of *dimensionless temperature*

$$\lambda \equiv \frac{2\pi T}{\Lambda}, \quad (3.45)$$

and obtain an integral expression for the radiatively induced *screening function* G , normalized to $G \rightarrow G/T^2$

$$\begin{aligned} \frac{G}{T^2} &= \frac{\Pi^{11}}{T^2} = \frac{\Pi^{22}}{T^2} \\ &= \int d\xi \int d\rho \, e(\lambda)^2 \lambda^{-3} \left(-4 + \frac{\rho^2}{4e(\lambda)^2} \right) \rho \frac{n_B \left(2\pi \lambda^{-3/2} \sqrt{\rho^2 + \xi^2 + 4e(\lambda)^2} \right)}{\sqrt{\rho^2 + \xi^2 + 4e(\lambda)^2}} \end{aligned} \quad (3.46)$$

$$\equiv \int d\xi \int d\rho \, h_G(\xi, \rho, \lambda), \quad (3.47)$$

where we have noted the λ -dependence of the coupling e by writing it explicitly. The integration must be done over the support (3.43), which we also write in dimensionless variables. Define the *dimensionless momentum* X

$$X \equiv \frac{|\mathbf{p}|}{T} = \frac{|p_3|}{T}, \quad (3.48)$$

and the *support function* s_{\pm}

$$s_{\pm}(\xi, \rho, \lambda, X, g) \equiv \left| \frac{g\lambda^3}{(2\pi)^2} + \frac{\lambda^{3/2}}{\pi} \left(\pm \sqrt{X^2 + g} \sqrt{\rho^2 + \xi^2 + 4e^2} - \xi X \right) + 4e^2 \right|. \quad (3.49)$$

Then the support condition (3.43) can be written in dimensionless form as [46]

$$s_{\pm}(\xi, \rho, \lambda, X, g) \leq 1, \quad (3.50)$$

with $g \equiv G/T^2$. The doubling of inequality (3.43) comes from writing the delta function in (3.42) in terms of k^0 [59]

$$\delta(k^2 - m^2) = \delta\left(k^0 + \sqrt{|\mathbf{k}|^2 + m^2}\right) + \delta\left(k^0 - \sqrt{|\mathbf{k}|^2 + m^2}\right). \quad (3.51)$$

Define the function $H_G(\lambda, X, g)$ as the integral of $h_G(\xi, \rho, \lambda)$ summed over the support defined by $s_{\pm}(\xi, \rho, \lambda, X, g) \leq 1$

$$H_G(\lambda, X, g) \equiv \sum_{\sigma=+,-} \int_{-\infty}^{\infty} d\xi \int_0^{\infty} d\rho \theta(1 - s_{\sigma}(\xi, \rho, \lambda, X, g)) h_G(\xi, \rho, \lambda). \quad (3.52)$$

where $\theta(x)$ is the Heaviside step function. Equation (3.46) then becomes

$$g - H_G(\lambda, X, g) = 0. \quad (3.53)$$

It turns out that (3.53) is enough to uniquely determine G [46]. For a given temperature T and momentum $\mathbf{p} = |\mathbf{p}|\hat{\mathbf{z}}$, the integral (3.52) can be calculated numerically as a function of λ , X and g . The value of g consistent with its defining equation (3.47) can then be determined by searching for the root of expression (3.53) using standard numerical methods. This root g of (3.53) happens to be unique for each momentum and temperature. This is all done using the Mathematica numerical software. Our algorithmic procedure is then as follows: For a given fixed temperature T and various values of X within an interval $[0, X_{max}]$, the value of g consistent with (3.47) is calculated by finding the root of (3.53). Each point is then used to interpolate $g(X, T)$ in X over $[0, X_{max}]$.

In figure 3.4a we have plotted the resulting function $G(X, T)/T^2$ for different temperatures. Note the existence of both an *screening* region where $G(X, T) > 0$ and an *antiscreening* region where $G(X, T) < 0$. Asymptotically, G goes to zero, its maxima and minima also tend to zero with increasing T .

With G nonzero we expect the dispersion law (3.34) to deviate from the massless case $G = 0$. Defining the *dimensionless frequency*

$$Y \equiv \frac{\omega}{T}, \quad (3.54)$$

we write the transverse dispersion law (3.34) as

$$Y = \sqrt{X^2 + \frac{G(X, T)}{T^2}}. \quad (3.55)$$

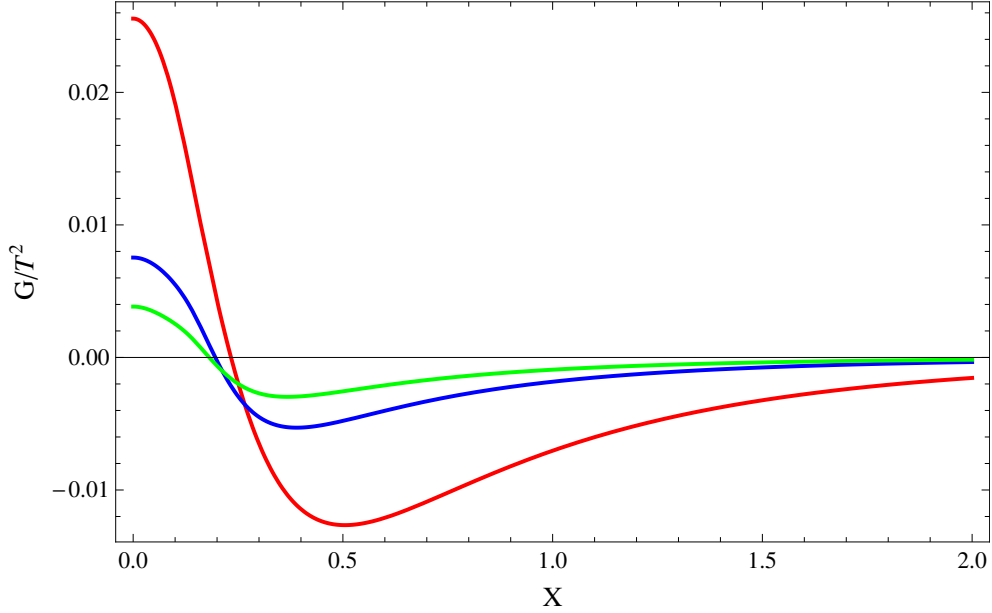
This dispersion relation for the transverse modes is plotted in figure 3.4b for different temperatures. The *cutoff frequency* ω^* is defined as

$$\omega^*(T) \equiv \sqrt{G(X=0, T)} = Y(X=0, T)T = Y^*(T)T. \quad (3.56)$$

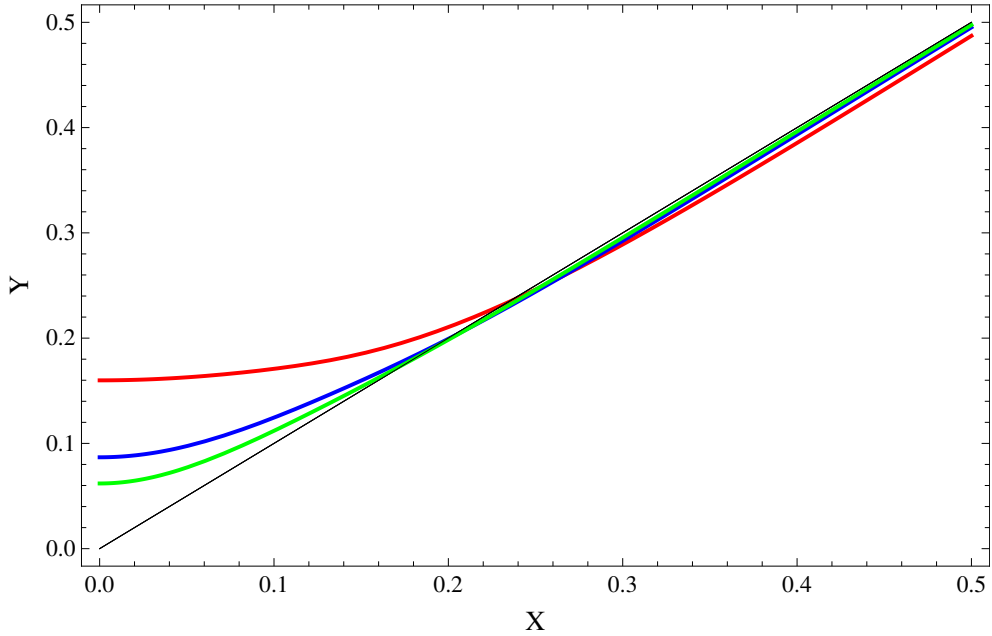
As seen in figure 3.4b, the cutoff frequency is the *minimal* frequency available for transverse propagation at a given temperature. From the same figure is also clear that Y^* decreases with increasing temperature. The functional relation $Y^*(T)$ is very important for our experimental considerations, since it defines the upper boundary of the *screening region* $Y \leq Y^*$ where photon propagation is forbidden. The experimental consequences of such screening effects will be investigated in chapter 5. In the next section, an expression for $Y^*(T)$ will be derived from curve fitting.

3.5.4 Some properties of the photon screening function G

In this section we give numerical fits for three characteristic points of the screening function. We work in SI units, so as to build an intuition on experimental orders of magnitude.



(a) The dimensionless screening function G/T^2 calculated for a given temperature T and momentum $X = p_3/T$ by solving for the unique root of equation (3.53). To obtain a complete plot in a given interval of X , the values of G for a given T were successively calculated for different values of X partitioning the interval. The curves shown correspond to the temperatures $T = 5\text{K}$ (red), $T = 8\text{K}$ (blue) and $T = 10\text{K}$ (green).



(b) The dimensionless dispersion law $Y(X) = \sqrt{X^2 + G/T^2}$ calculated from G . Note that the value of the cutoff frequency $Y^* \equiv Y(X = 0)$ for each temperature falls with T . The plotted temperatures are $T = 5\text{K}$ (red), $T = 8\text{K}$ (blue) and $T = 10\text{K}$ (green). The U(1) dispersion law $Y = X$ is shown as a black line.

Figure 3.4: Transverse screening mass G/T^2 (a) and dispersion relations (b).

In section 3.5.3 we defined the *cutoff frequency* as the minimal available frequency for any given temperature, $h\nu^*(T) = c\sqrt{G(|\mathbf{p}|=0, T)}$. We calculated ν^* for temperatures between 2 and 165 Kelvin. The results are depicted in figure 3.5. Figure 3.5b shows how ν^* grows with decreasing temperature, reaching a maximum at about 5.4 Kelvin of about $\nu^* = 17\text{GHz}$, then decreases and suddenly drops to zero below 4.5K. To calculate the fit, we have assumed a *power law* functional relation of the form

$$\nu^*(T) = c + bT^\gamma. \quad (3.57)$$

We excluded from the fit data points below 7K, as seen in figure 3.5b. The Mathematica software was used to fit the data points to (3.57), resulting in the expression

$$\frac{\nu^*(T)}{\text{GHz}} = 42.71 \left(\frac{T}{\text{K}} \right)^{-0.53} + 0.22. \quad (3.58)$$

How well this fit matches the data is shown in figure 3.5.

Another interesting characteristic frequency is the *crossover frequency* ν_c , defined as

$$G(\nu_c, T) = 0. \quad (3.59)$$

This is the frequency at which the screening function G goes from screening to antiscreeing. Just as ν^* , ν_c drops to zero below 4.5 Kelvin. A fit of the data points to a power law of the form (3.57) gives as result

$$\frac{\nu_c(T)}{\text{GHz}} = 1.83 \left(\frac{T}{\text{K}} \right)^{1.12} + 13.48. \quad (3.60)$$

This is plotted in figure 3.6.

In chapter 5 we introduce the *radiance* function of a black emitter. It will be shown that the ratio between an $SU(2)$ and an $U(1)$ emitter is given by the term

$$\left(1 - \frac{c^2 G}{(h\nu)^2} \right) \theta(\nu - \nu^*). \quad (3.61)$$

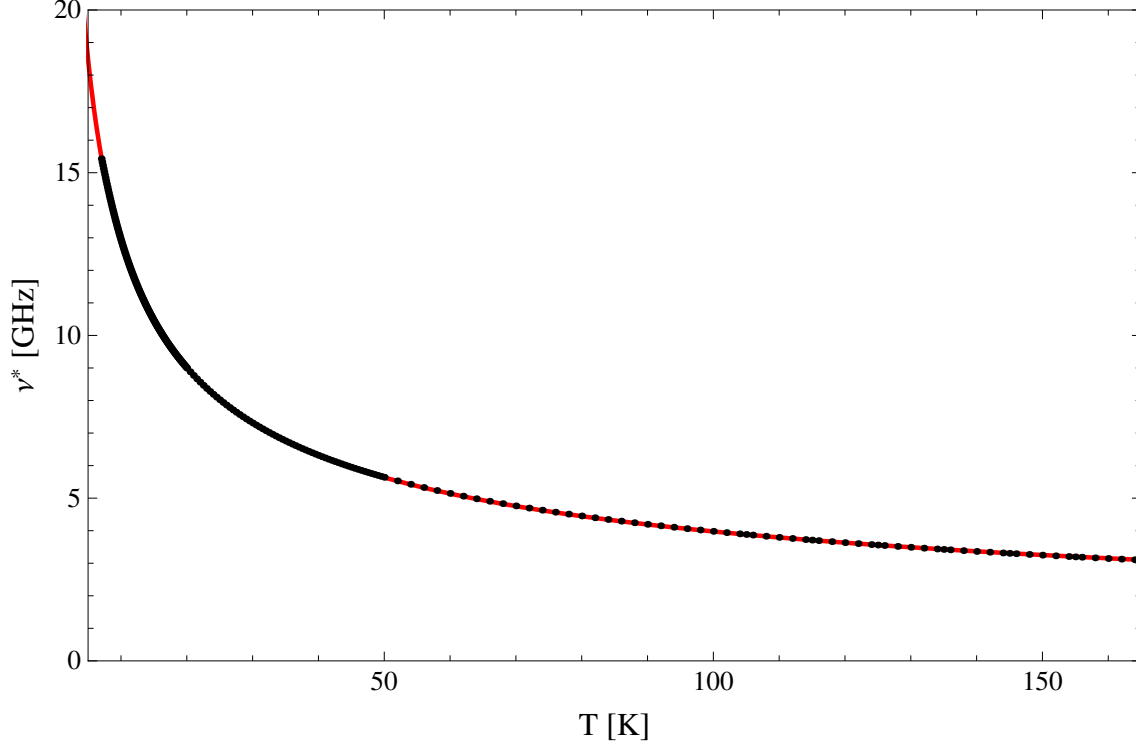
The maximal difference between $U(1)$ and $SU(2)$ radiance in the antiscreeing regime, where G is negative, is then given at the frequency ν_M where G/ν^2 reaches a *minimum*

$$\frac{G(\nu_M, T)}{\nu_M^2} = \frac{G(\nu, T)}{\nu^2} \Big|_{\min}. \quad (3.62)$$

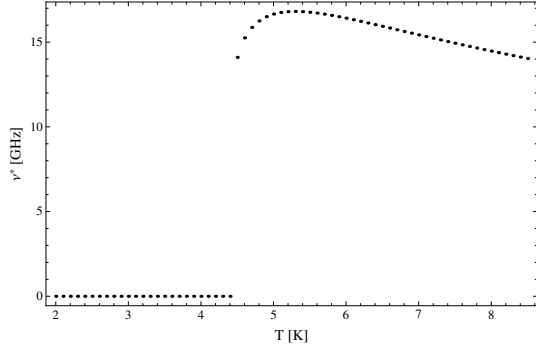
Thus ν_M is the frequency of *maximal antiscreeing*. A fit of the data to a power law of the form 3.57 gives

$$\frac{\nu_M(T)}{\text{GHz}} = 3.45 \left(\frac{T}{\text{K}} \right)^{1.08} + 12.90. \quad (3.63)$$

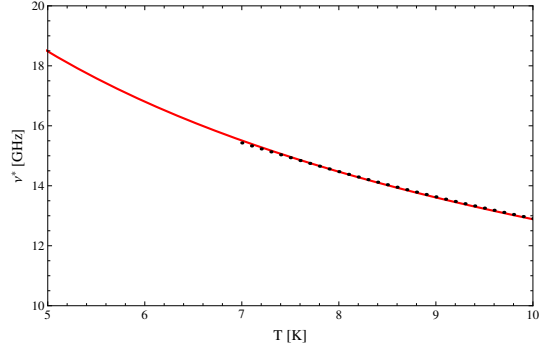
Figure 3.6 shows the calculated points overlaid with the fitted curve.



(a) The set of cutoff frequencies $\{\nu_i^*\}$ calculated from a discrete set of temperatures $\{T_i\}$ between 2 and 165 Kelvin, shown here as black dots, overlapped with the curve $\nu^*(T) = 0.22 + 42.71 \cdot T^{-0.53}$ fitted from the dataset $\{\nu_i^*, T_i\}$.



(b) Closeup of the dataset $\{\nu_i^*, T_i\}$ near the temperature $T = 4.5\text{K}$ for which the cutoff frequency ν^* rapidly falls to zero. The temperature region between 2K and 7K was not included in the calculation of best-fit parameters.



(c) Closeup of the dataset $\{\nu_i^*, T_i\}$ near $T = 7\text{K}$ which was used as the lower bound of the curve fit.

Figure 3.5: The cutoff frequency ν^* was fitted to a power function in T , using a dataset $\{\nu_i^*, T_i\}$ calculated from discrete set of temperatures $\{T_i\}$ between 2 and 165 Kelvin. The original set had $i = 1, \dots, 306$ data-points. The first 50 of those, corresponding to temperatures between 2K and 7K where ignored in the calculation of best-fit parameters. Taking ν^* in GHz and T in Kelvin, the best fit for the remaining 256 points in the dataset is given by the power law $\nu^*(T) = 0.22 + 42.7T^{-0.53}$.

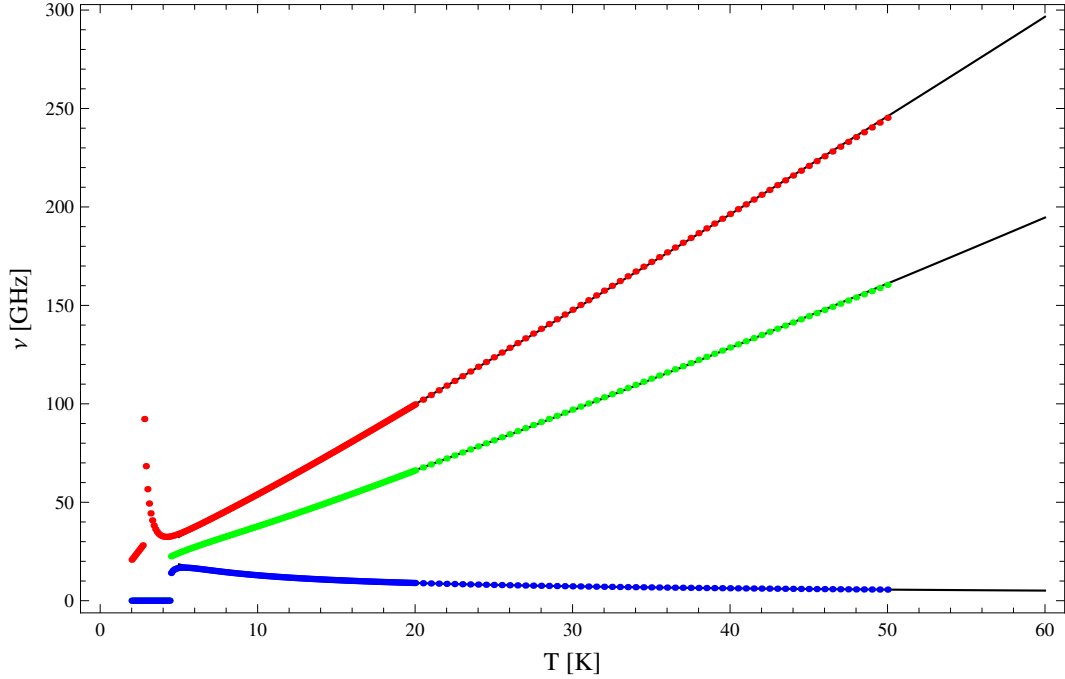


Figure 3.6: The T -dependence of the characteristic points of G : $\nu^*(T)$ (blue), $\nu_c(T)$ (green), and $\nu_M(T)$ (red). Taken from [13].

3.5.5 Longitudinal mode

Consider now the propagation of longitudinal modes, characterized by the poles of the term $\propto u_\mu u_\nu$ in (3.32). On shell, $p^2 = F$, and (3.39) simplifies to

$$X^2 \equiv \frac{\mathbf{p}^2}{T^2} = \frac{\Pi_{00}}{T^2}. \quad (3.64)$$

To calculate this expression numerically, we first assume that diagram B of figure 3.42 is the only contribution to the polarization tensor. Afterwards, we check that diagram A in figure 3.3, vanishes on-shell $F = p^2$. The expression for $\Pi^{00} \equiv \Pi_B^{00}$ can be read from equation (3.42)

$$\begin{aligned} X^2 &= \frac{\Pi_B^{00}}{T^2} \\ &= \int d\xi \int d\rho \, 2e^2 \lambda^{-3} \left(3 + \frac{\rho^2 + \xi^2}{4e^2} \right) \rho \frac{n_B \left(2\pi \lambda^{-3/2} \sqrt{\rho^2 + \xi^2 + 4e^2} \right)}{\sqrt{\rho^2 + \xi^2 + 4e^2}} \end{aligned} \quad (3.65)$$

$$\equiv \int d\xi \int d\rho \, h_F(\xi, \rho, \lambda). \quad (3.66)$$

The integrations are subject, as in the transverse case, to the following constraint

$$s_\pm(\xi, \rho, \lambda, X, f) \leq 1, \quad (3.67)$$

with the *support function* s_{\pm} defined as

$$s_{\pm}(\xi, \rho, \lambda, X, f) \equiv \left| \frac{f\lambda^3}{(2\pi)^2} + \frac{\lambda^{3/2}}{\pi} \left(\pm \sqrt{X^2 + f} \sqrt{\rho^2 + \xi^2 + 4e^2} - \xi X \right) + 4e^2 \right|, \quad (3.68)$$

with $f \equiv F/T^2$. As we did in section 3.5.3 for the transverse case, we express the inequality (3.50) by using the Heaviside step function $\theta(x)$, and define a function $H_F(\lambda, X, f)$ as the integral of $h_F(\xi, \rho, \lambda)$ in (3.66) summed over the support determined by (3.68)

$$H_F(\lambda, X, f) \equiv \sum_{\sigma=+,-} \int_{-\infty}^{\infty} d\xi \int_0^{\infty} d\rho \theta(1 - s_{\sigma}(\xi, \rho, \lambda, X, f)) h_F(\xi, \rho, \lambda). \quad (3.69)$$

Then the consistency condition for the integral equation (3.65) is just the expression

$$X^2 - H_F(\lambda, X, f) = 0. \quad (3.70)$$

Using the same method as in section 3.5.3, which is to search for the root of equation 3.70 in f , given fixed values of X and λ , results in numerical difficulties, due to the spectral function $F(X)$ being *double valued*. The longitudinal screening function F , in contrast to G , *separates in different branches*. Therefore, the searching algorithm has to be modified to look for the roots of (3.70) in X , with fixed values of f and T . This root turns out to be unique. The search results are displayed in figure 3.7a, where we have plotted $F(X)/T^2$ for different temperatures. Note the existence of two branches of F . Furthermore, X is confined to a finite domain between $X = 0$ and $X = 0.4$, as shown in the plot. This strange behaviour is reflected in the longitudinal dispersion law of figure 3.7b.

Using similar numerical methods as those described above, we have checked that diagram A, given by expression (3.41), vanishes on shell $F = p^2$.

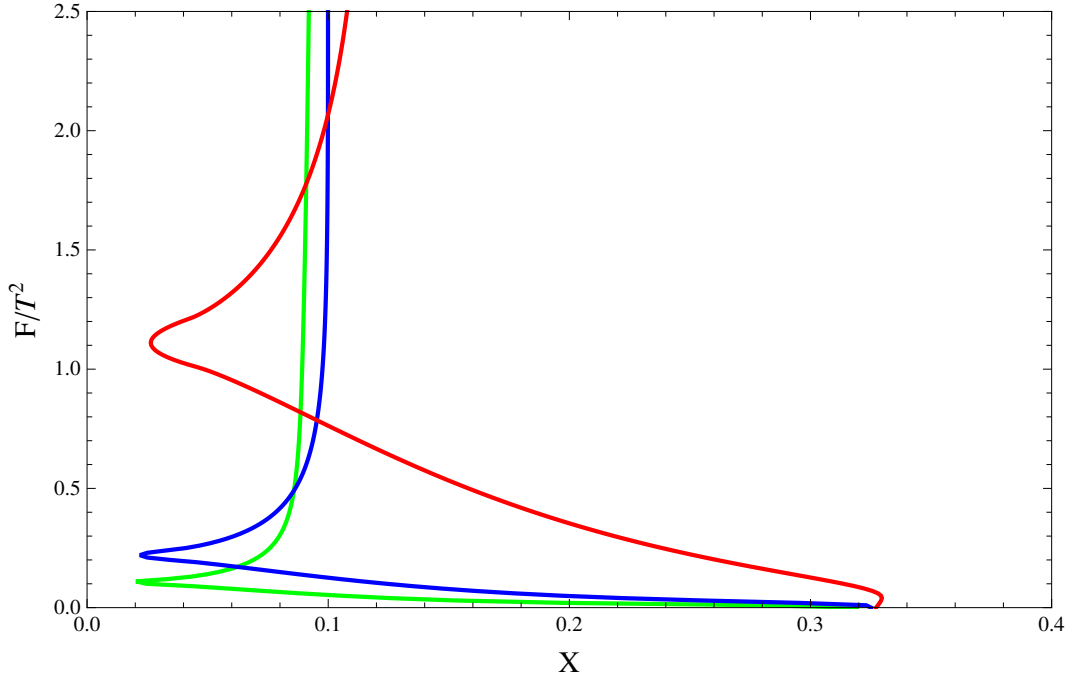
In dimensionless quantities the longitudinal dispersion law reads

$$Y_L \equiv \frac{\omega_L}{T} = \sqrt{X^2 + \frac{F(X, T)}{T^2}}. \quad (3.71)$$

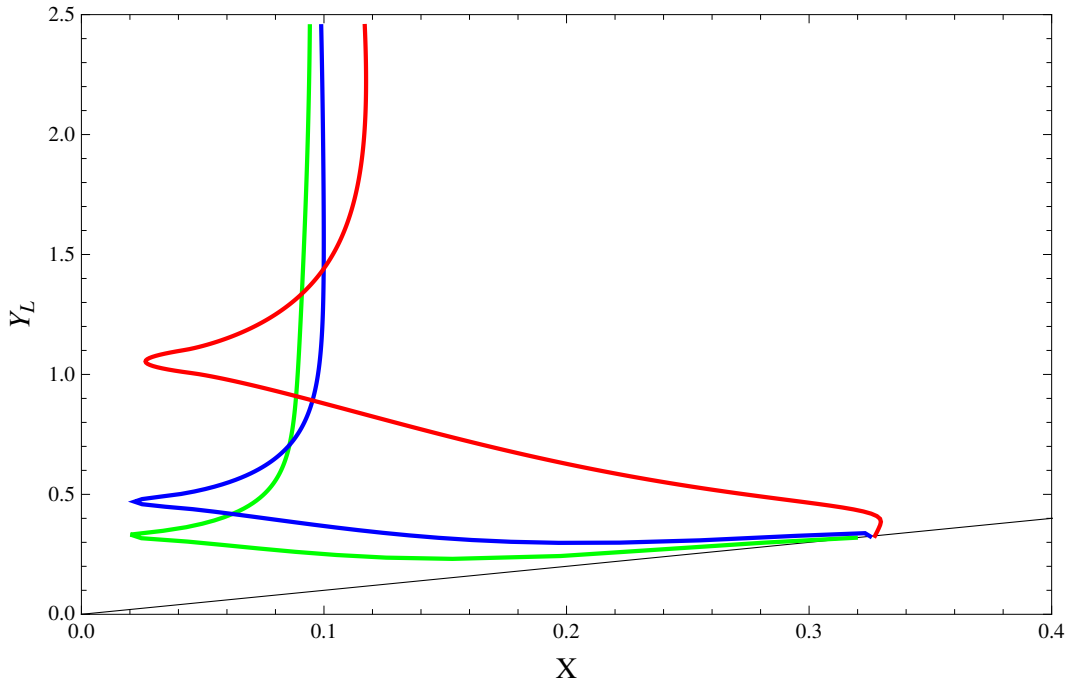
This relation is plotted in figure 3.7b for three different temperatures. Notice the existence of various branches, consequence of the double-valuedness of $F(X)$. The lower branch shows a dispersion law with negative slope, reaching its maximum available spatial momentum at the point where $Y(X) = X$. Further, the upper branch of Y_L becomes superluminal at very low X , or large wavelength X^{-1} , and diverges to infinity very quickly. This suggests that the longitudinal modes are unphysical.

Consider also the magnetic-electric dual interpretation for the thermal SU(2) Yang-Mills theory described in [25], where the propagating electric field in the SU(2) theory becomes a magnetic field in the thermal photon plasma. Recall that longitudinal oscillations describe *electric charge density* waves [35]. In the dual interpretation, the long wavelength branching modes in figure 3.7b become *magnetic* density waves, and cannot transfer energy in any interaction with electric charges. We gather that no thermalization can occur for these modes.

From the above arguments we can only conclude that the longitudinal modes are, if not unphysical, at least unable to propagate nor transport energy. Thus, we may ignore the longitudinal modes in our further discussion. The only excitations of the SU(2) thermal photon gas we will consider are the transverse modes of the tree-level massless gauge field.



(a) The dimensionless longitudinal screening function F/T^2 . As seen in the plot, $F(X)$ is double valued, so the searching algorithm used for the transverse modes had to be modified to look for the roots of (3.70) in X , with fixed values of F/T^2 and T . This root turns out to be unique. The curves shown correspond to the temperatures $T = 5\text{K}$ (red), $T = 8\text{K}$ (blue) and $T = 10\text{K}$ (green).



(b) The longitudinal dispersion law $Y_L(X) = \sqrt{X^2 + F/T^2}$ calculated from F . Note the two branches, consequence of the double-valuedness of F . The plotted temperatures are $T = 5\text{K}$ (red), $T = 8\text{K}$ (blue) and $T = 10\text{K}$ (green). The $U(1)$ dispersion law $Y = X$ is shown as a black line.

Figure 3.7: Longitudinal screening mass F/T^2 (a) and dispersion relations (b).

3.6 Resummation of one-loop radiative corrections

Apart from the effect on photon propagation, the transverse screening function G may be used to calculate thermodynamical properties of the SU(2) gas. Through the procedure of *resummation*, corrections to the energy density and pressure induced by interaction of SU(2) photons with the thermal ground state can be extracted. We will find such corrections to be linear in the temperature. The thermodynamical consistency of this resummation approach is also discussed in this section.

3.6.1 Prerequisites

Recall from section 3.2 that the ground state of the thermal SU(2) Yang-Mills gas is composed of a scalar field ϕ (3.5) and a pure-gauge configuration (3.10). From the effective action (3.6) the energy-momentum tensor $\theta_{\mu\nu}^{\text{gs}}$ of this configuration may be calculated,

$$\theta_{\mu\nu}^{\text{gs}} = -4\pi\Lambda T g_{\mu\nu}. \quad (3.72)$$

Take the SU(2) gas to be a *perfect fluid* in thermal equilibrium, $\theta_{\mu\nu}^{\text{gs}} = (P^{\text{gs}} + \rho^{\text{gs}})u_\mu u_\nu + P^{\text{gs}}g_{\mu\nu}$, with the restframe specified by the 4-velocity vector u_μ . Then we read from (3.72) that $\rho^{\text{gs}} = -P^{\text{gs}} = 4\pi\Lambda T$. As given in (3.11), the (classical) ground state configuration has a nontrivial energy density which grows linearly with temperature. For later comparison with higher-order corrections, we write this result in the form

$$\frac{\rho^{\text{gs}}}{T^4} = -\frac{P^{\text{gs}}}{T^4} = 2(2\pi)^4 \lambda^{-3} \sim 3117.09 \lambda^{-3}, \quad (3.73)$$

where as before the dimensionless temperature is defined as $\lambda = \frac{2\pi T}{\Lambda}$.

Note also that the ground state pressure P^{gs} in (3.73) is negative. This may be interpreted microscopically as magnetic monopole-antimonopole [37, 38, 43, 51] *attractive* interactions due to the dominance in thermal fluctuations of small-holonomy caloron configurations [9].

Equation (3.73) gives the tree-level contribution to the gas thermodynamics. What about higher order corrections? As shown in [18], linear contributions $\Delta P^{\text{gs},1\text{-loop}}$ and $\Delta \rho^{\text{gs},1\text{-loop}}$ to P^{gs} and ρ^{gs} , respectively, arise from the free fluctuations of tree-level massive modes at high temperature. This correction is given by

$$\frac{\Delta \rho^{\text{gs},1\text{-loop}}}{T^4} = \frac{\Delta P^{\text{gs},1\text{-loop}}}{T^4} = -\frac{1}{4} a^2 = -2(2\pi)^4 \lambda^{-3} \sim -3117.09^4 \lambda^{-3}, \quad (3.74)$$

where $a \equiv \frac{2e|\phi|}{T} = \frac{8\sqrt{2}\pi^2}{\lambda^{3/2}}$ is the temperature scaled mass [18].

Note that, since both P^{gs} and $\Delta P^{\text{gs},1\text{-loop}}$ are linear in temperature, a Legendre transformation to the energy density $\rho = T \frac{dP}{dT} - P$ must vanish. But $\rho^{\text{gs}} + \Delta \rho^{\text{gs},1\text{-loop}} = 0$ also vanishes, therefore both corrections are *thermodynamically consistent*.

In the following, we show how a correction to the base energy and pressure of the ground state can arise by assuming selfconsistent propagation at the 1-loop level of tree-level massless modes. This correction will depend linearly on temperature, again signaling ground state effects on photon propagation, and vice versa.

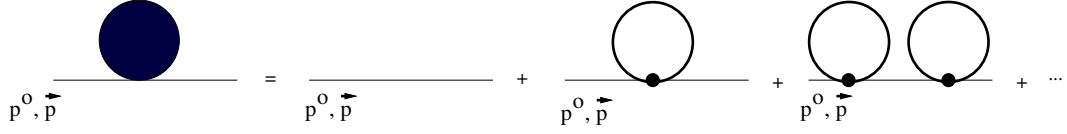


Figure 3.8: The Dyson series for the dressed propagator of the massless mode, containing only tadpole diagrams, since it is the only nonvanishing diagram on the induced mass shell, see section 3.5. A thin line refers to the propagation of the tree-level massless, a thick line to the propagation of tree-level massive modes. Taken from [12].

3.6.2 Resummation

A *resummed* perturbation expansion is given by replacing the bare propagator with the dressed one. In figure 3.8 the diagrammatic expansion of the dressed propagator up to one-loop is shown. Since diagram A in figure 3.3, as given by 3.41, vanishes in the effective theory (see section 3.5), we only need to consider the one-loop tadpole (diagram B in figure 3.3). We can then calculate resummed thermodynamical quantities by the usual method of expanding $\ln Z$ in *bubble diagrams*, but replacing the bare propagator with its resummed (dressed) version.

But we already calculated the dressed one-loop propagator (determined by the one-loop polarization tensor). As we reviewed in 3.5.1, the dressed propagator in figure 3.8, as a result of photon interactions with the ground state, displays a modified dispersion law for the propagating, transverse massless modes. From section 3.5.3 we recall the dimensionless dispersion relation

$$Y = \sqrt{X^2 + \frac{G(X, T)}{T^2}}, \quad (3.55)$$

and the definitions $Y \equiv \frac{\omega}{T}$, $X \equiv \frac{|\mathbf{p}|}{T}$. Thus, we can insert the modified dispersion relation (3.55) in the thermodynamical integrals for *energy density* and *pressure*

$$\rho = \frac{1}{\pi^2} \int d\mathbf{p} \mathbf{p}^2 \frac{\omega}{e^{\beta\omega} - 1}, \quad (3.75)$$

$$P = -\frac{1}{\pi^2} \int d\mathbf{p} \mathbf{p}^2 \ln(1 - e^{-\beta\omega}). \quad (3.76)$$

derived from the partition function for the noninteracting (zero chemical potential) massless boson with two degrees of freedom [35]

$$\ln Z = -2V \int \frac{d^3\mathbf{p}}{(2\pi)^3} \left[\frac{1}{2}\beta\omega + \ln 1 - e^{-\beta\omega} \right]. \quad (3.77)$$

Then, we get the *1-loop resummed* energy density and pressure

$$\frac{\rho^{1\text{-loop, res}}}{T^4} = \frac{1}{\pi^2} \int_0^\infty dX X^2 \frac{\sqrt{X^2 + G/T^2}}{e^{\sqrt{X^2 + G/T^2}} - 1}, \quad (3.78)$$

$$\frac{P^{1\text{-loop, res}}}{T^4} = -\frac{1}{\pi^2} \int_0^\infty dX X^2 \ln(1 - e^{-\sqrt{X^2 + G/T^2}}), \quad (3.79)$$

where we have rescaled by T^4 to make both expressions dimensionless. Define the dimensionless corrections $\Delta\bar{P}$ and $\Delta\bar{\rho}$ to the contributions of free, massless particles as

$$\Delta\bar{\rho} \equiv \frac{\Delta\rho^{1\text{-loop, res}}}{T^4} = \frac{\rho^{1\text{-loop, res}}}{T^4} - \frac{\pi^2}{15}, \quad (3.80)$$

$$\Delta\bar{P} \equiv \frac{\Delta P^{1\text{-loop, res}}}{T^4} = \frac{P^{1\text{-loop, res}}}{T^4} - \frac{\pi^2}{45}. \quad (3.81)$$

Corrections (3.80) and (3.81) can be calculated, by first calculating G as shown in section 3.5.3, as a function of temperature. Figure 3.9 depicts both $\Delta\bar{P}$ and $\Delta\bar{\rho}$ as functions of the dimensionless temperature λ in the high-temperature region $100 \leq \lambda \leq 500$ (recall that $\lambda_c = 13.87$). The calculated data points can be fitted to a curve assuming power law dependency

$$\Delta\bar{\rho} = c_\rho \lambda^\gamma, \quad (3.82)$$

$$\Delta\bar{P} = c_P \lambda^\delta. \quad (3.83)$$

The best fit is given for the parameter values

$$c_\rho = 3.9577, \quad \gamma = -3.02436, \quad (3.84)$$

$$c_P = 8.4963, \quad \delta = -3.00904. \quad (3.85)$$

First note that the resummed corrections are linear, similar to (3.73), but three orders of magnitude smaller. Equations (3.84), (3.85) can thus be interpreted as corrections to the tree-level ground state estimates. The linear dependency is then not surprising, since selfconsistent propagation is affected by the quasiparticle mass of tree-level heavy modes in the tadpoles of figure 3.8, which in turn reflect the a priori estimate for the energy density of the thermal ground state.

In calculating the contribution of higher irreducible loop orders to the polarization tensor we observe a hierarchic decrease and expect a termination at a finite order. For the effective theory of SU(2) Yang-Mills thermodynamics described in this chapter, it can be shown that the contribution of higher irreducible loop orders to the polarization tensor quickly decreases at higher loop orders [26, 36]. Further contributions of these loop orders to the one-loop resummation calculated here should therefore be small enough to be safely ignored.

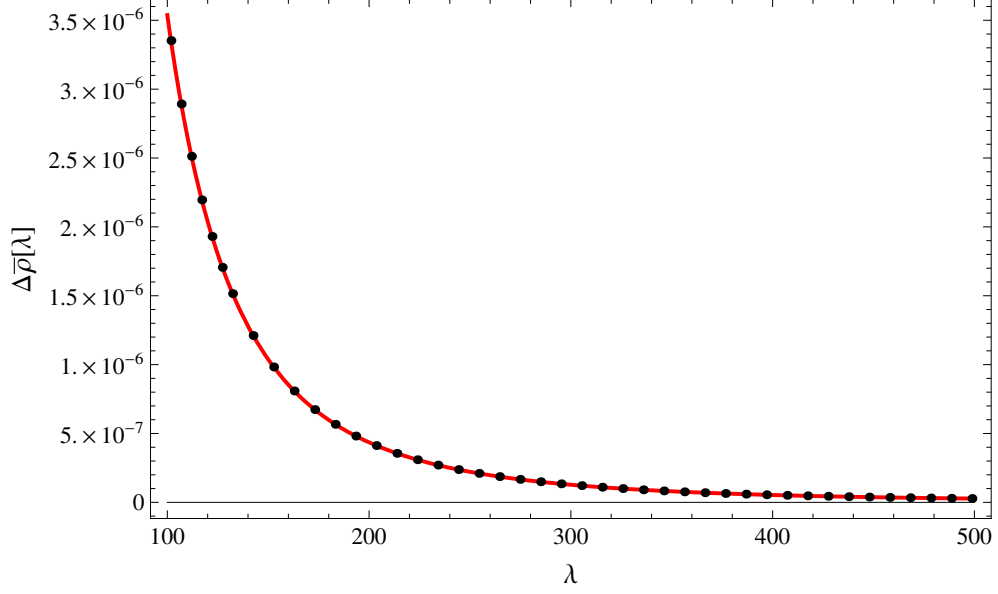
3.6.3 Thermodynamical consistency

We have seen that the a priori pressure and energy estimates for the ground state plus corrections, which incorporate fluctuations of the tree-level massive modes, obey the usual Legendre relations of the form $\rho = T \frac{dP}{dT} - P$. What about the resummed corrections defined in (3.80), (3.81)?

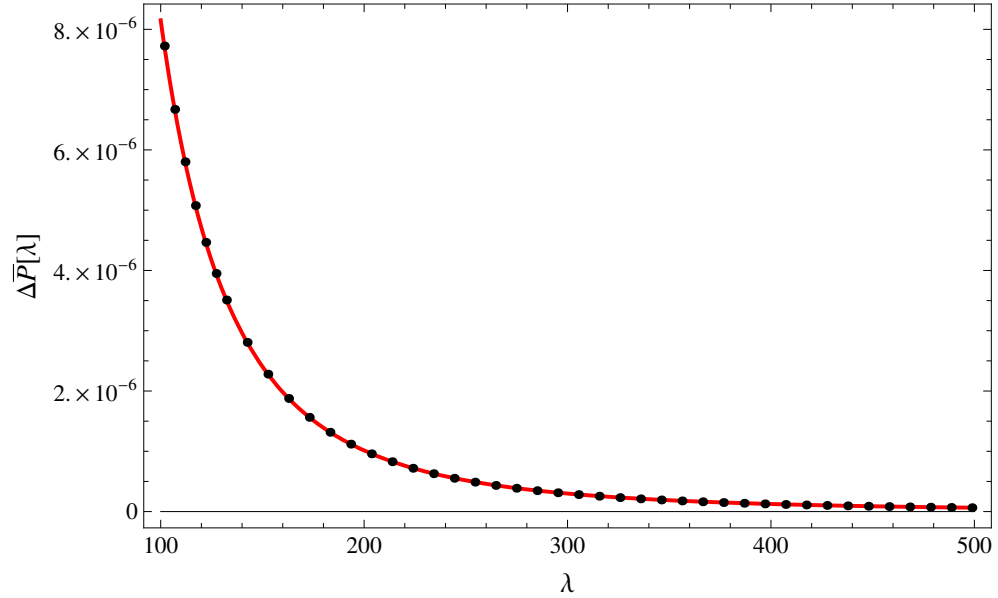
Directly defining $\Delta\rho_L^{1\text{-loop, res}}$ as the Legendre transformation of $\Delta P^{1\text{-loop, res}}$,

$$\Delta\rho_L^{1\text{-loop, res}} \equiv T \frac{d\Delta P^{1\text{-loop, res}}}{dT} - \Delta P^{1\text{-loop, res}}, \quad (3.86)$$

we can compare both the energy density $\Delta\rho_L^{1\text{-loop, res}}$ resulting from the Legendre relation (3.86) and the resummed energy density $\Delta\rho^{1\text{-loop, res}}$ by calculating the ratio of both functions $\Delta\rho_L^{1\text{-loop, res}}/\Delta\rho^{1\text{-loop, res}} = \Delta\bar{\rho}_L/\Delta\bar{\rho}$. Such a comparison is plotted in figure 3.10. It is clear that the ratio is far from unity, and both densities show opposite signs.



(a) The resummed one-loop dimensionless correction to the energy density, as defined in equation (3.80). Fitting of the data to a power law of the form (3.82) results in the expression $\Delta\bar{\rho} = 3.9577 \cdot \lambda^{-3.02436}$.



(b) The resummed one-loop dimensionless correction to the pressure, as defined in equation (3.81). Fitting of the data to a power law of the form (3.83) results in the expression $\Delta\bar{P} = 8.4963 \cdot \lambda^{-3.00904}$.

Figure 3.9: The calculated high-temperature λ dependence of (a) $\Delta\bar{\rho}$ and (b) $\Delta\bar{P}$. Dots correspond to computed values, the line is a numerical fit to the power functions defined in equations (3.82) and (3.83).

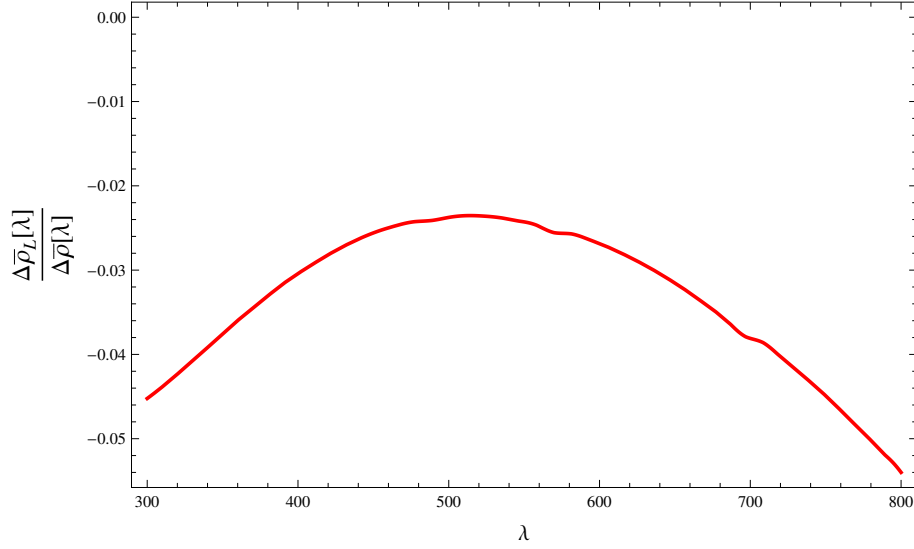


Figure 3.10: The λ dependence of the ratio $\frac{\Delta \bar{\rho}_L[\lambda]}{\Delta \bar{\rho}[\lambda]}$, where $\Delta \rho_L^{1-\text{loop, res}} \equiv T^4 \Delta \bar{\rho}_L$ is defined in equation (3.86), and λ is the dimensionless temperature. The plot shows how the corrections to pressure and energy density due to one-loop resummation as calculated in the text are not thermodynamically selfconsistent, since radiative corrections shifting the dispersion law of tree-level massive modes were not considered in the calculation.

How should we understand this apparent inconsistency? Remember that by using the bare (free) propagators of the TLM vector modes in our calculations, we ignored one-loop corrections to the propagation of these modes. Without taking into account radiative corrections for the massive modes, such inconsistencies were to be expected. One may stay consistent only up to a given loop order, and then every resummed propagator must be considered.

Nevertheless, the linear correction given by expressions (3.82) and (3.83) with fitted parameters (3.84) and (3.85) can still be interpreted as the contribution to the thermal gas energy and pressure by photon propagation among *stable* monopole-antimonopole pairs, which in turn influence the ground state physics.

Chapter 4

Inhomogeneous Thermodynamics

In the nonperturbative approach to the thermal SU(2) Yang-Mills gas discussed in chapter 3, the assumption of homogeneous and isotropic thermodynamics was of central importance. In particular, it led to the inference that the modulus $|\phi|$ of the adjoint scalar field ϕ^a should be constant (see section 3.1), and that the ground state field configuration a_μ^{gs} must be *pure gauge* (see equation (3.10)). The thermal ground state composed by the inert scalar field ϕ and the pure gauge solution a_μ^{gs} then serve as a homogeneous and isotropic background to the dynamics of topologically trivial fluctuations.

Thus, the question arises as to whether this assumption can be relaxed. Namely, if it is possible to expand the nonperturbative treatment of chapter 3 to consider the case of inhomogeneous thermodynamics, and whether the physical description of a thermal ground state made up by a scalar field together with a background gauge field configuration remains valid. The second question that arises is, under what circumstances is such a description *not* valid? Is it always the case that a ground state $(\phi, a_\mu^{\text{gs}})$ exists over which trivial fluctuations propagate?

Both problems are not only of theoretical interest, but important for experimental considerations as well. If we hope to realize an SU(2) thermal photon gas in the laboratory, we need to specify under what experimental circumstances the theoretical formalism reviewed in chapter 3 is valid. Further, and in the same vein, we need to know if there are any possible experimental conditions where the ground state description of the SU(2) gas breaks down.

This chapter is an attempt to answer both questions and gain insight into the possibility of experimentally realizing the thermal SU(2) ground state.

First we tackle the problem of generalizing the approach of chapter (3) to inhomogeneous thermodynamics. A particular solution to the SU(2) equations of motion with scalar field has been found, which in the context of nonperturbative Yang-Mills thermodynamics and under the adiabatic approximation allows for temperature profiles without disturbing the ground state. The derivation of this solution is given in appendix A. In this chapter, we use a practical ansatz for the spatial a^3 vectors, then calculate with the help of (A.17'') and (A.24) the rest of the gauge and scalar fields. With a solution at hand, we investigate what kind of thermal gradients are produced, and under which boundary conditions.

For the second problem, we invoke a recent resonant cavity experiment at low temperatures by Tada et. al. [66] as an example of how the thermal SU(2) ground state may be deformed to be indistinguishable from the dynamics of a U(1) gas.

4.1 The SU(2) thermomagnetic effect

In this section, we present a solution to the SU(2) Yang-Mills equations of motion that does not assume space homogeneity. Instead, the temperature profile is allowed to vary along a coordinate axis. As we will see, under certain assumptions, this temperature profile implies the existence of non-trivial gauge field configurations, giving rise to a *magnetic field*, which may be interpreted as emerging from the temperature gradient. This has some parallels with the *thermoelectric effect* in solids. Indeed, the SU(2) thermomagnetic effect can be understood as a rearrangement of topological magnetic charges in the ground state because of thermal diffusion.

4.1.1 Basic approach

We will abandon the requirement of constant temperature for the thermal system, and instead assume a space-dependent temperature distribution in one dimension, $T(\vec{x}) = T(z)$. Such a temperature distribution will in turn affect the thermal ground state through the modulus of the scalar field $|\Phi|(\vec{x}) = |\Phi|(z) = \sqrt{\frac{\Lambda^3}{2\pi T(z)}}$. Here we use the notation of appendix A and label the inhomogeneous scalar field as capital Φ , to differentiate from the homogeneous inert field ϕ of chapter 3. We are interested in the effects of a non-zero temperature gradient on the gauge field configurations which solve the Yang-Mills equation of motion.

In the SU(2) gas, position-dependence of the modulus of Φ implies the position-dependence of the mass for the two massive modes. We expect that the pure-gauge ground state configurations of the form (3.10) will no longer be solutions of the equations of motion with space-dependent ground state, but will be replaced by a non-homogeneous configuration reacting to the deformation of Φ . The non-homogeneities in the gauge field lead to the emergence of non-scalar (isotropy breaking) quantities such as a magnetic field $\vec{\nabla} \times \vec{a}^3$.

The deformation of Φ will also influence radiative corrections for the propagation of the transverse massless mode. Since radiative corrections are small in the effective theory compared to the tree-level (bare) ensemble, we may ignore such corrections. Therefore, we only search for classical solutions to the Yang-Mills equations of motion (3.9) with a space-dependent scalar field $|\Phi|(z)$ taken as a source term. This is carried out in appendix A.

4.1.2 Adiabatic approximation

An important consideration we must bear in mind is that the field energy density of such inhomogeneous field configurations described in section 4.1.1 *must never be greater* than the energy density of the SU(2) ground state over the entire domain of the fields. Such an *energy hierarchy* is condition *sine qua non* to ensure the existence of the coarse-grained scalar field. Otherwise, the ensemble dynamics could no longer be described by topologically trivial fluctuations over a static background, and the effective theory described in chapter 3 would not be applicable. We therefore demand that the energy scale of the scalar field Φ be larger than any other scale of the system. This is the *adiabatic approximation*.

In our particular solution to the equations of motion with z -dependent scalar field Φ , a nontrivial magnetic field \mathbf{B} with energy density $\rho_{\mathbf{B}} = \frac{1}{2}|\mathbf{B}|^2$ emerges. The adiabatic

approximation then demands

$$\rho_{\mathbf{B}}(z) < \rho^{\text{gs}}(z). \quad (4.1)$$

Condition (4.1) guarantees that the effective theory summarized in chapter 3 remains a good description of the $\text{SU}(2)$ ground state.

4.1.3 Restrictions on possible solutions

To use the results of appendix A, we first need a good ansatz for the vector \vec{a}^3 . To have a physical interpretation the solutions derived from the ansatz should be such that

1. The temperature field $T(z)$ has a parametrization such that a baseline temperature $T_{\min} \equiv \lim_{z \rightarrow \infty} T(z)$ can always be specified, with T_{\min} greater than the critical temperature T_c of the deconfining phase, $T_{\min} > T_c \sim 2.73 \text{ K}$.
2. The conditions needed for the validity of the adiabatic approximation, described in section 4.1.2, particularly equation (4.1), must hold.

Note that condition 1 rules out using simple power laws such as $a_i^3 \sim z^\gamma$ as ansatz, since after inserting in equations (A.17'') and (A.24), the temperature field always shows the limit $\lim_{z \rightarrow \infty} T(z) \sim z^{-2\gamma}$ which is either 0 or infinity, depending on the sign of γ . One could try numerically searching for solutions $a^3(z)$ of the equation

$$\frac{1}{2}(a^3)^2 - \frac{1}{4e^2} \sqrt{-\frac{a^3}{\partial_z^2 a^3}} \partial_z^2 \sqrt{-\frac{\partial_z^2 a^3}{a^3}} = \frac{\Lambda^3}{2\pi} T^{-1}(z). \quad (4.2)$$

for a specific distribution $T(z)$. Equation (4.2) is arrived at by inserting (A.17'') in (A.25) and taking $a_1^3 = a_2^3 \equiv a^3$.

But this was too much of an overhead for our purposes. In the next section, we will offer a simple ansatz which fulfills both requirements 1 and 2 using just two parameters. We then discuss how it describes deformations from homogeneous thermodynamics.

4.1.4 A particular ansatz

In this section, we will introduce a simple rational function as an ansatz to derive inhomogeneous field and temperature configurations. We will check that the requirements outlined in section 4.1.3 be fulfilled, then discuss the derived field solutions, in particular the resulting temperature distribution. This exercise will help us build a basic intuition for the possible ways that an homogeneous temperature distribution may be deformed without disturbing the ground state physics of the $\text{SU}(2)$ gas.

In the following, unless otherwise stated, we work in natural units $\hbar = k_B = c = 1$, so energy and temperature have dimension eV, length dimension $(\text{eV})^{-1}$, etc. We use dimensionless coordinate variables, which are made dimensionless by rescaling with the factor $\frac{\Lambda}{2\pi}$ (the factor 2π is for numerical convenience only). Recall that Λ is the $\text{SU}(2)$ Yang-Mills scale and has dimension of energy, $[\Lambda] = \text{eV}$, so lengths are rescaled by multiplication with $\frac{\Lambda}{2\pi}$. Coordinate variables are then rescaled as $\hat{z} \equiv \frac{\Lambda}{2\pi} z$.

Define now the z -dependent function

$$g(\hat{z}; g_0, g_1) = g_0 \left(\frac{\Lambda}{2\pi} \right)^2 \frac{\hat{z}^2 + g_1}{\hat{z}^2 + 1}, \quad (4.3)$$

with dimensionless parameters g_0 and g_1 . By definition, the function 4.3 has dimension of energy squared, $[g] = (\text{eV})^2$.

From appendix A, we learn that from a reasonable ansatz for $\vec{a}^3(\vec{x}) = \vec{a}^3(z)$ we can calculate a complete solution to the equations of motion (A.1). Using (4.3) as an ansatz, we write

$$a_1^3(\hat{z}) = a_2^3(\hat{z}) \equiv a^3(\hat{z}) = \sqrt{\frac{1}{2}g(\hat{z})}. \quad (4.4)$$

Note that the energy dimensions on the right and left hand side of (4.4) coincide. Definition (4.4) requires the parameter g_0 to be positive. We also take $g_1 > 0$ so as to tentatively allow all $\hat{z} > 0$. From (A.17''), (A.24) and (3.2), we can calculate

$$a_0(\hat{z}) = \frac{\Lambda}{2\pi} \sqrt{-\frac{\partial_{\hat{z}}^2 a^3}{2e^2 a^3}}, \quad (4.5)$$

$$|\Phi|^2(\hat{z}) = \frac{1}{2}(a^3)^2 - \left(\frac{\Lambda}{2\pi}\right)^2 \frac{\partial_{\hat{z}}^2 a_0}{4e^2 a_0}, \quad (4.6)$$

$$T(\hat{z}) = \frac{\Lambda^3}{2\pi|\Phi|^2}. \quad (4.7)$$

The magnetic field for this field configuration can be calculated from (4.4)

$$|\mathbf{B}|(\hat{z}) = |\mathbf{rot} \vec{a}^3| = \sqrt{2} \frac{\Lambda}{2\pi} \partial_{\hat{z}} a^3, \quad (4.8)$$

$$\rho_{\mathbf{B}}(\hat{z}) = \frac{1}{2}|\mathbf{B}|^2. \quad (4.9)$$

Finally, recall the energy density of the thermal ground state, which is given by equation (3.11)

$$\rho^{\text{gs}}(\hat{z}) = 4\pi\Lambda^3 T(\hat{z}). \quad (3.11)$$

Notice that $\lim_{\hat{z} \rightarrow \infty} |\Phi|^2 = \lim_{\hat{z} \rightarrow \infty} \frac{1}{2}(a^3)^2 = \left(\frac{\Lambda}{4\pi}\right)^2 g_0$, since from (4.5) we read $\lim_{\hat{z} \rightarrow \infty} a_0 \sim \frac{\Lambda}{2\pi} \hat{z}^{-1}$ and $\lim_{\hat{z} \rightarrow \infty} \frac{\partial_{\hat{z}}^2 a_0}{a_0} = 0$. Then from equation (4.7) it is seen that

$$\lim_{\hat{z} \rightarrow \infty} T(\hat{z}) = 8\pi\Lambda g_0^{-1}. \quad (4.10)$$

So the baseline temperature at infinity can be fixed by adjusting g_0 . This fulfills our first condition. In order to have $T_{\min} > T_c$ we need

$$\begin{aligned} T_{\min} &= 8\pi\Lambda g_0^{-1} > T_c = \frac{\Lambda}{2\pi} \lambda_c \\ \implies g_0 &< \frac{16\pi^2}{\lambda_c}. \end{aligned} \quad (4.11)$$

For $\lambda_c = 13.87$ [31], this means $g_0 < 11.39$. We also demand that the temperature profile decrease asymptotically to T_c , but this means that a^3 must be *monotonically increasing* for large \hat{z} . From (4.4) and the definition of g (4.3) we see that this can be achieved by having $g_1 < 1$.

The second condition, that the magnetic field energy density always be smaller than that of the ground state, is difficult to check analytically for all \hat{z} . But we can at least make sure that it holds asymptotically. Recall that in the limit of large \hat{z} , $|\Phi|^2$ behaves as $\frac{1}{2}(a^3)^2$. Then the ground state energy density at large \hat{z} is given as

$$\lim_{\hat{z} \rightarrow \infty} \rho^{\text{gs}}(\hat{z}) = 32\pi^2 \Lambda^4 g_0^{-1}. \quad (4.12)$$

The magnetic field energy density at large \hat{z} can also be calculated

$$\lim_{\hat{z} \rightarrow \infty} \rho_{\text{B}}(\hat{z}) = \left(\frac{\Lambda}{2\pi}\right)^2 \lim_{\hat{z} \rightarrow \infty} (\partial_{\hat{z}} a^3)^2 = g_0 \left(\frac{\Lambda}{2\pi}\right)^4. \quad (4.13)$$

Condition (4.1) then reads

$$g_0 < (\sqrt{2}\pi) 16\pi^2. \quad (4.14)$$

But $\sqrt{2}\pi > \lambda_c^{-1}$, so the restriction $T_{\text{min}} > T_c$ already ensures the energy hierarchy required by the adiabatic condition *in the large \hat{z} limit*. For small \hat{z} , we will need to test (4.14) explicitly.

Summarizing, we see that for $0 < g_1 < 16\pi^2 \lambda_c^{-1}$ and $0 < g_1 < 1$, the ansatz (4.14) inserted in (4.4) results in field configurations that do indeed fulfill the conditions in section 4.1.3, at least asymptotically. We test these configurations in the next section.

4.1.5 Some examples

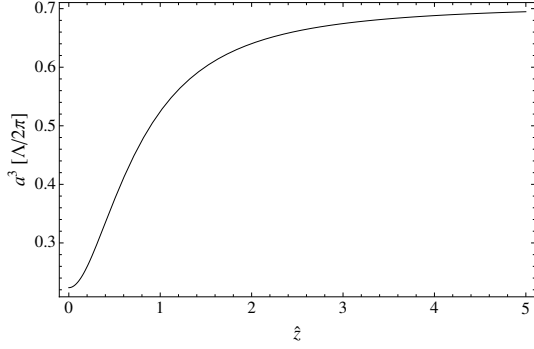
Now we try our solution using ansatz parameters $g_0 = 1$, $g_1 = 0.1$. The resulting fields are plotted in figure 4.1, in units of the SU(2) Yang-Mills scale $\frac{\Lambda}{2\pi}$ and in dimensionless coordinates.

Note how $a^3(\hat{z})$ (figure 4.1a) tends to a constant value $\frac{1}{\sqrt{2}} \frac{\Lambda}{2\pi}$ at infinity. Plotting $a_0(\hat{z})$ (figure 4.1b), we encounter our first problem. $a_0(\hat{z})$ becomes imaginary at $\hat{z}_0 = 0.39$, which is also the point where the real part of $a_0(\hat{z})$ becomes zero. The temperature field (figure 4.1c) shows non-monotonic behaviour in the region where $\text{Re } a_0(\hat{z}) = 0$. It assumes a minima at $T = 0$, which contradicts the requirement that $T(\hat{z}) > T_{\text{min}}$. This is not surprising. In section 4.1.4 we showed that the function g , defined in (4.3) and used as ansatz for the field a^3 fulfills the requirements outlined in section 4.1.3 *asymptotically*. We need to restrict the domain of our solutions from $\hat{z} \in [0, \infty]$ to $\hat{z} \in [\hat{z}_{\text{min}}, \infty]$ with \hat{z}_{min} large enough that the problems outlined above disappear.

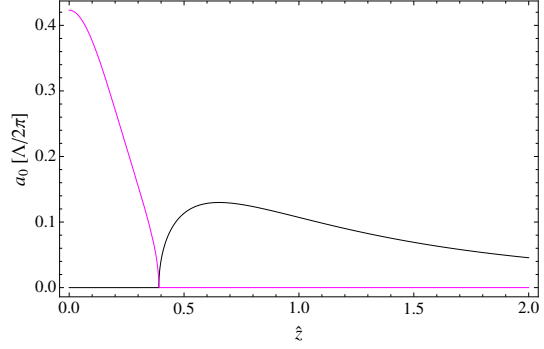
Figure 4.1c shows two maxima for the temperature field $T(\hat{z})$. After the second maxima, $T(\hat{z})$ appears to decrease asymptotically to a constant value, which is the behaviour we are looking for. It seems therefore appropriate to define \hat{z}_{min} to be the value of \hat{z} at which the second maxima of $T(\hat{z})$ occurs, since this would give us a monotonically decreasing temperature distribution. In this case then, $\hat{z}_{\text{max}} = 0.836$. Note also that $\hat{z}_{\text{max}} > \hat{z}_0$. The domain $[\hat{z}_{\text{min}}, \infty]$ should therefore be free of imaginary fields.

For simplicity, we define a coordinate translation $\hat{z} \rightarrow \hat{z} - \hat{z}_{\text{max}}$, and consider only $\hat{z} > 0$. This is the region we are interested in from now on.

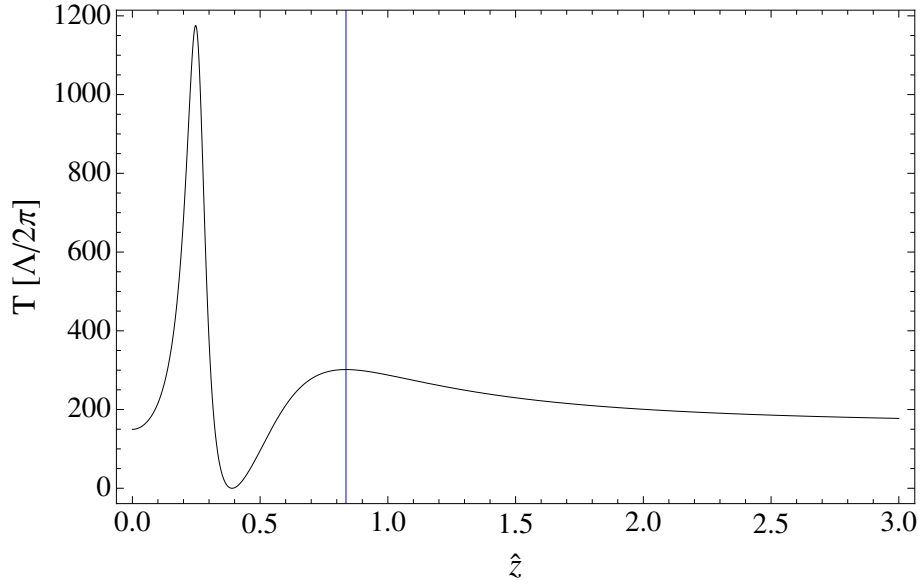
In figure 4.2 we have plotted the translated fields a_0 and T . We interpret figure 4.2b physically as a temperature gradient. In figure 4.2c we have plotted this gradient in SI units. We see that for parameters $g_0 = 1$ and $g_1 = 0.1$, the resulting temperature distribution



(a) The field $a^3(\hat{z})$ plotted in units of the SU(2) Yang-Mills scale $\frac{\Lambda}{2\pi}$, calculated from (4.4)

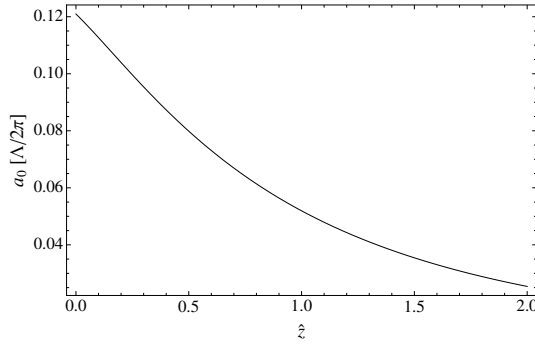


(b) The field $a_0(\hat{z})$ plotted in units of the SU(2) Yang-Mills scale $\frac{\Lambda}{2\pi}$, calculated from (4.5). The real part of a_0 is plotted in black, the imaginary part in blue.

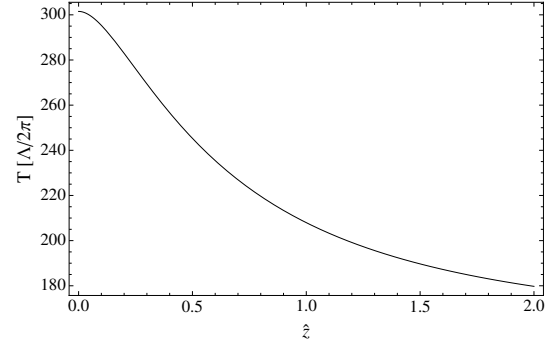


(c) The temperature field, plotted in units of the SU(2) Yang-Mills scale $\frac{\Lambda}{2\pi}$, calculated from (4.7). The maxima of $T(\hat{z})$ in the domain where $\text{Im } a_0(\hat{z}) = 0$ is shown by the blue line and lies at $\hat{z}_{max} = 0.836$.

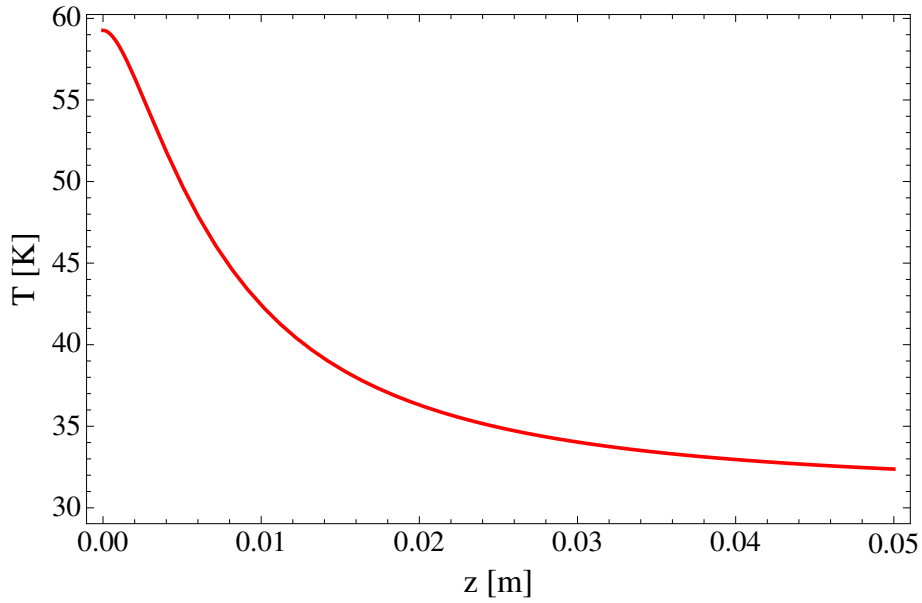
Figure 4.1: Various fields calculated from ansatz (4.3) with parameters $g_0 = 1$, $g_1 = 0.1$. \hat{z} is dimensionless.



(a) The field $a_0(\hat{z})$ plotted in units of the SU(2) Yang-Mills scale $\frac{\Lambda}{2\pi}$, after translation $\hat{z} \rightarrow \hat{z} - \hat{z}_{max}$.



(b) The temperature field $T(\hat{z})$ plotted in units of the SU(2) Yang-Mills scale $\frac{\Lambda}{2\pi}$, after translation $\hat{z} \rightarrow \hat{z} - \hat{z}_{max}$ so that it has a maxima $\hat{z} = 0$.



(c) The temperature field $T(\hat{z})$ from figure 4.2b plotted in SI units. It starts from a maximum value of $T_{max} = 59.26\text{K}$ and asymptotically decreases to a value $T_{min} = 31.04\text{K}$. This gradient is a result of the ansatz in (4.3) with parameters $g_0 = 1$ and $g_1 = 0.1$.

Figure 4.2: The fields (a) $a_0(\hat{z})$ and (b) $T(\hat{z})$ are translated in \hat{z} so that the maximum of the temperature now lies at $\hat{z} = 0$. The ansatz parameters are the same as in figure 4.1, $g_0 = 1$, $g_1 = 0.1$. \hat{z} is dimensionless. In (c) we have plotted the temperature field in SI units. It decreases from a maxima $T_{max} = 59.26\text{K}$ to a baseline value $T_{min} = 31.04\text{K}$.

decreases from a maxima $T_{\max} = 59.26\text{K}$ to a baseline value $T_{\min} = 31.04\text{K}$. The length scale of this gradient is of the order of centimeters.

This temperature gradient is a scalar perturbation of the equations of motion for the SU(2) fields, and *causes* the field configurations (4.4), (4.5), which are static nonzero solutions of the perturbed equations of motion. Then we can interpret the resulting magnetic field $B(\hat{z})$, plotted in figure 4.3a, as a *thermomagnetic field* generated by perturbing the coarse-grained SU(2) Yang-Mills thermal ground state with a temperature gradient of the form (4.7). The interpretation that the thermal gradient causes the magnetic field and not the other way around is forced upon us by the requirement that the ground state energy scale, and therefore the thermal gradient, is the dominant energy scale of the system. Note from figure 4.3a that it goes to zero very quickly.

The thermomagnetic field in figure 4.3a contributes to the energy density of the (perturbed) vacuum with ρ_B as given in equation (4.9). This energy density is plotted in figure 4.3b in units of the SU(2) Yang-Mills scale $\frac{\Lambda}{2\pi}$. Comparing ρ_B with the energy density of the ground state (figure 4.3c), we see ρ_B lies about 8 orders of magnitude *below* ρ^{gs} over the entire domain. The condition (4.1) imposed by the adiabatic approximation is satisfied. Solutions calculated from $g_0 \sim 1$ and $g_1 \sim 0.1$ are therefore acceptable deformations of the thermodynamically homogeneous SU(2) Yang-Mills ground state.

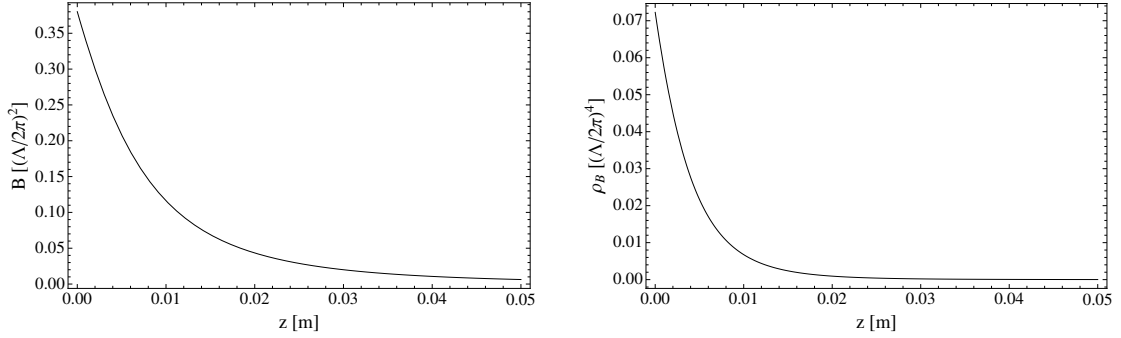
To show the effect of parameter g_1 , we increase g_1 while leaving g_0 constant, and calculate another set of solutions using $g_0 = 1$ and $g_1 = 0.999$. We have plotted the resulting energy density and temperature profile in figure 4.4. Note that the baseline temperature $T_{\min} = 31.04\text{K}$ remains unchanged, since it only depends on g_0 as was shown before. The new maximum, however, lies at $T_{\max} = 31.67\text{K}$. Increasing g_1 has resulted in a smaller value T_{\max} . This parameter is therefore responsible for setting the maximal temperature of the profile. It can also be checked numerically that in the limit $g_1 \rightarrow 1$, $\partial_z T(z) \rightarrow 0$ and the temperature is constant over the entire domain, with $T(z) = T_{\max} = T_{\min} = 8\pi\Lambda g_0^{-1}$. Ansatz (4.3) shows a continuous limit (numerically) to the homogeneous case.

Finally, we remark that in the context of nonperturbative SU(2) thermodynamics, a *dual interpretation* is necessary [25], in which the magnetic fields in the effective theory are understood as *electric fields* in nature. The thermomagnetic effect described here is therefore a *thermoelectric effect* in nature.

4.2 Decoupling from the ground state

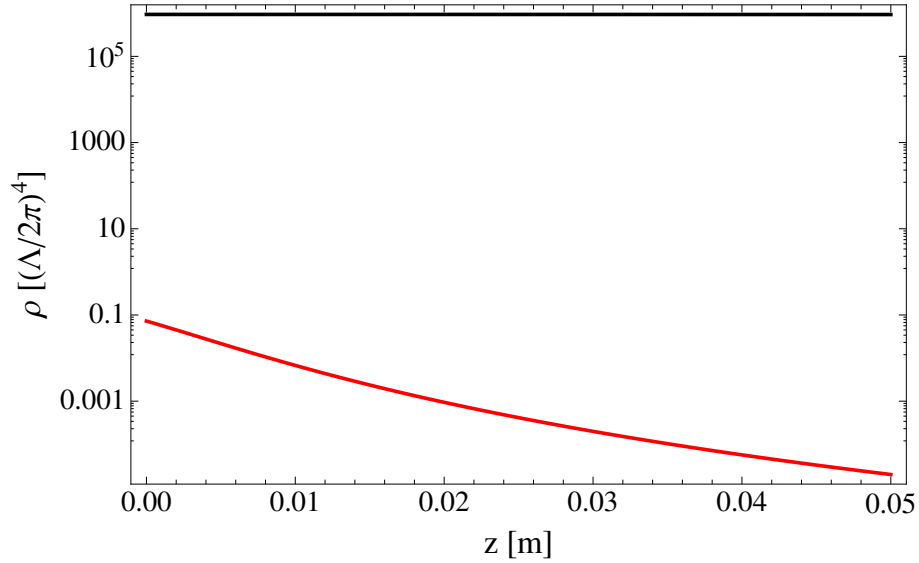
We have seen how it is possible to disturb the homogeneity of the thermal ground state in such a way that it still remains an effective description of the thermal SU(2) gas. The deciding criterion is the energy scale hierarchy. As long as the ground state energy density is the dominant scale, deformations from the totally homogeneous case are still consistent with the existence of a coarse-grained ground state. In our particular solution, such distortions were also accompanied by non-trivial gauge field configurations responsible for the emergence of a magnetic field. In order to remain consistent with the adiabatic approximation, the field energy of such configurations must always be considerable lower than that of the thermal ground state.

In our experimental endeavours, for reasons discussed in chapter 5, it will not only prove useful to know under what conditions the temperature or field energy deformations



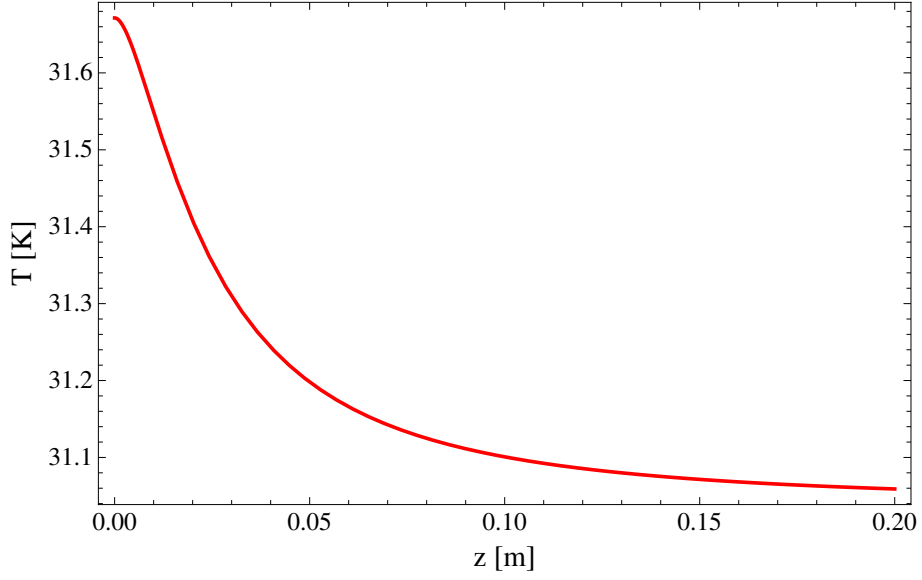
(a) The modulus of the magnetic field $B(\hat{z})$ plotted in units of the SU(2) Yang-Mills scale $\frac{\Lambda}{2\pi}$, calculated from (4.8). The coordinate z is plotted in meters.

(b) The magnetic energy density $\rho_B(\hat{z})$ plotted in units of the SU(2) Yang-Mills scale $\frac{\Lambda}{2\pi}$, calculated from (4.9). The coordinate z is plotted in meters.

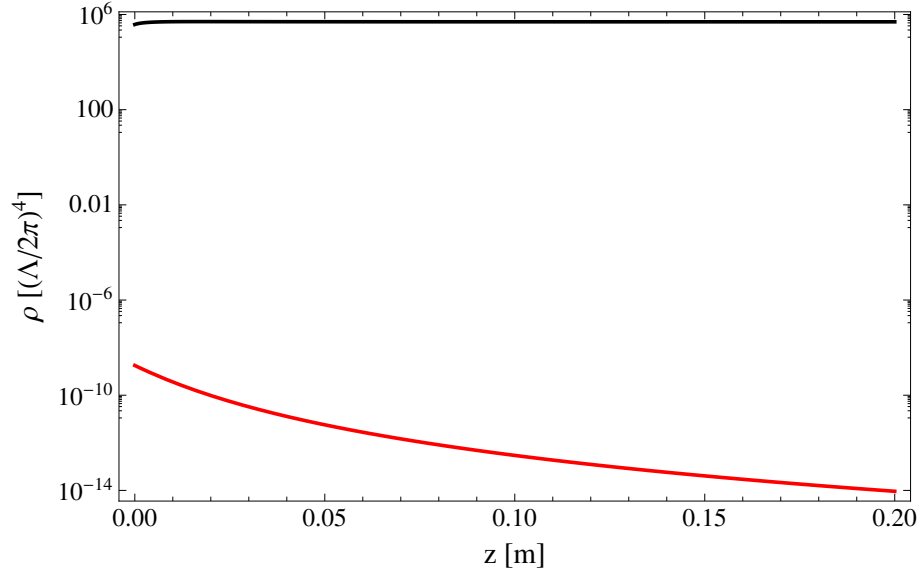


(c) The magnetic field energy density $\rho_B(\hat{z})$ (in red) calculated from the generated magnetic field $B(\hat{z})$, and the energy density of the thermal ground state $\rho^{gs}(T(\hat{z}))$ (in black), plotted in units of the SU(2) Yang-Mills scale $\frac{\Lambda}{2\pi}$. ρ^{gs} lies roughly 8 orders of magnitude above ρ_B .

Figure 4.3: The magnetic field $B(\hat{z})$, its energy density $\rho_B(\hat{z})$, and a comparison with the ground state energy density $\rho^{gs}(\hat{z})$. The ansatz parameters are the same as in figure 4.1, $g_0 = 1$, $g_1 = 0.1$. The coordinate z is plotted in meters.



(a) The temperature field $T(z)$ plotted in SI units. It starts from a maximum value of $T_{\max} = 31.67\text{K}$ and asymptotically decreases to a value $T_{\min} = 31.04\text{K}$. This gradient is a result of the ansatz in (4.3) with parameters $g_0 = 1$ and $g_1 = 0.999$.



(b) The magnetic field energy density $\rho_B(z)$ (in red) calculated from the generated magnetic field $B(\hat{z})$, and the energy density of the thermal ground state $\rho^{gs}(T(z))$ plotted in natural units.

Figure 4.4: (a) Temperature field and (b) energy densities calculated from ansatz (4.3) with parameters $g_0 = 1$, $g_1 = 0.999$. The coordinate z is plotted in meters.

conserve the ground state, but also under what conditions they cause a decoupling from it, effectively creating U(1) conditions. In this section, we investigate the possibilities of creating an effective U(1) system.

4.2.1 Electromagnetic field decoupling

As explained in the preceding section, the energy scale of the ground state energy must be the largest scale of the system if the effective theory is to remain valid. But what happens when this hierarchy is destroyed, and the SU(2) ground state energy density becomes small relative to another energy scale?

An example of such an experimental situation is given by the single-photon counting experiment described in [66]. ^{85}Rb atoms in the $111_{s_{1/2}}$ Rydberg state flying through a resonant cavity are excited upwards to the $111_{p_{3/2}}$ state by absorption of thermal photons of frequency 2527 MHz, and then are counted by a method of selective ionization. Thus the experiment is sensible to the mean photon number $\bar{n}(T)$ inside the cavity at a given temperature and cavity resonant frequency. The measurement was performed for temperatures T ranging from 67 mK up to 1 K. During the measurements, a static electric stray field of magnitude $|\vec{E}| \sim 25 \frac{\text{mV}}{\text{cm}}$ was present in the cavity. No deviation of $\bar{n}(T)$ from the U(1) expected Bose-Einstein distribution was observed. Yet under the SU(2) hypothesis, absolutely no photon propagation should be possible.

From what we have learnt in this chapter, we can guess that this could have to do with the energy hierarchy inside the cavity. The energy density ρ_E of the external electric field in SI units is given by

$$\rho_E = \frac{\epsilon_0}{2} \vec{E}^2, \quad (4.15)$$

where $\epsilon_0 = 8.854187817 \cdot 10^{-12} \text{ J}/(\text{V}^2\text{m})$. The energy density of the SU(2) thermal ground state ρ^{gs} in SI units is

$$\rho^{\text{gs}} = 4\pi \Lambda^3 \frac{k_B}{(\hbar c)^3} T, \quad (4.16)$$

where $\Lambda = 2\pi \frac{k_B T_c}{\lambda_c}$, $T_c = 2.725 \text{ K}$ and $\lambda_c = 13.87$, see section 3.4. To maintain energy scale hierarchy, the electric field energy density should be smaller than the energy density of the ground state, $\rho_E < \rho^{\text{gs}}$. For an static electric field magnitude of $|\vec{E}| \sim 25 \text{ mV/cm}$, this would imply a ground state temperature of the order of at least 10^3 K . That is, the effective radiation temperature implied by the stray electric field $|\vec{E}|$ is at least three orders of magnitude above the thermalized radiation at 1 K (and below) inside the cavity. With such a large energy disparity, a decoupling of the ground state physics from the propagation properties of photons must have occurred. Ground state induced effects on the photon disappear and the dispersion law becomes indistinguishable from that of the conventional U(1) theory.

As we will see in chapter 5, this decoupling effect can be used to compare and test for the presence of an SU(2) thermal ground state.

4.3 Summary

In this section we have investigated the different possibilities of deforming the thermal ground state. We have learnt that energy scale hierarchy determines the validity of the

effective theory and thus the presence of SU(2) effects.

To realize SU(2) black cavities experimentally, we should therefore be wary of stray electric or magnetic fields with energy densities much larger than that of the effective ground state such as those present in the cavity experiments of Tada et. al. [66]. For example, at $T = 10$ K, the energy density of the ground state becomes comparable to that of an electric field of magnitude $|\vec{E}| \sim 2.47$ mV/cm. To protect scale dominance of the thermal ground state, the cavity should be shielded from stray electromagnetic fields *much smaller* than 2.47 mV/cm, of the order magnitude of at most $|\vec{E}| \sim 10^{-3}$ mV/cm.

Similarly, to mirror the conditions of the Tada et. al. experiment and produce a black U(1) emitter at $T = 10$ K, the cavity should be transcended with electric fields of magnitude of at least $|\vec{E}| \sim 10^3$ mV/cm.

This knowledge will be useful later when we design an experiment to compare between both regimes.

Chapter 5

Radiometry and Bolometry of SU(2) Photons

In this chapter we first review some basic definitions regarding energy transfer, with the goal of arriving at an expression for the *spectral black-body radiance* without assuming a U(1) dispersion law. Next we examine the basic concepts of antenna theory and re-derive a formula for the *antenna temperature*. Again, this is done without making any dispersion law explicit. Both sections are included in this work since, apart from reviewing basic concepts, we need to check that the usual formulae given in the literature also apply in the case of a non-trivial dispersion law. This will, indeed, turn out to be the case (up to the appearance of a *screening region*, as described in chapter 3), but it is not *a priori* clear and needs to be shown explicitly. The third section describes briefly what a radiometer system is, and, most importantly, the possible sources of measurement error and the maximum possible *radiometer sensitivity*. Finally, sections 5.4 and 5.5 discuss the possibility of detecting the SU(2) thermal ground state by radiometric means and possible experimental realizations, relying on concepts introduced throughout the chapter.

Unless stated otherwise, we always use natural units, $\hbar = c = k_B = 1$, until section 5.4 in which we describe calculated predictions of experimental results using SI units exclusively.

5.1 Thermal radiation and energy propagation

Following [22, 70], in this section we review basic concepts on radiation propagation. The results derived in this chapter will be important when characterising *thermal energy transfer*. Specifically the expression for *black-body radiance* is obtained without making use of any explicit dispersion law. The SI units of important radiometric quantities introduced in this section will be written beside their equation number.

Recall that the fundamental self-interacting SU(2) gauge modes become weakly interacting thermal quasiparticles in the effective theory [27, 47]. This allows the local *spectral decomposition* of any quantity X characterising some aspect of energy transfer by photon propagation. The spectral components X_k or X_ω of X can always be defined by only considering contributions from monochromatic radiation of mode \mathbf{k} or frequency ω . Then

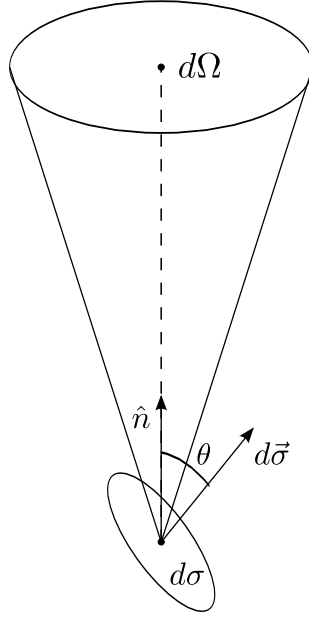


Figure 5.1: The flux through an area element $d\sigma$ propagating along the subtended angle $d\Omega$, see text.

the total quantity X on a system is given by the integration over its available modes

$$X = \int dk X_k = \int d\omega X_\omega. \quad (5.1)$$

By a change of variable we can relate both k -mode and ω -mode spectral decompositions

$$X_\omega = |\partial_{\mathbf{k}}\omega_{\mathbf{k}}|^{-1} X_k. \quad (5.2)$$

5.1.1 Radiant power

In the following we will deal with the characterisation and measurement of the electromagnetic field in vacuum. The labels *energy* or *radiant energy* will always refer to the energy stored in the propagating photon field as reviewed in Appendix B. *Radiant power* Φ is then defined as the change in radiant energy Q per unit time

$$\Phi \equiv \frac{dQ}{dt}. \quad [\text{W}] \quad (5.3)$$

We will also often refer to "energy rays" or "energy beams". The ray concept, borrowed from geometrical optics, provides an intuitive characterisation for the propagation of energy from source to detector. This intuitive description is made precise by identifying "ray" with the *Poynting vector* of the propagating electromagnetic field. When expanding in single Fourier modes, the Poynting Vector is parallel to the *wave vector* \mathbf{k} of the plane wave, see section B.2.

5.1.2 Radiance

Consider now an elementary beam of incoherent radiant power Φ in a homogeneous and isotropic medium passing through a surface element $d\vec{\sigma}$, which propagates further within

the solid angle $d\Omega$ with axis vector \hat{n} , see Fig. 5.1. Then the *radiance* (or *brightness*) at a point in $d\sigma$, defined as the radiant power per unit solid angle (in the direction of the ray) and per unit projected area (perpendicular to the ray), can be written as

$$L \equiv \frac{d^2\Phi}{d\Omega (d\vec{\sigma} \cdot \hat{n})} = \frac{d^2\Phi}{d\Omega (d\sigma \cos \theta)} . \quad [\text{W m}^{-2} \text{ sr}^{-1}] \quad (5.4)$$

Consider now two area elements $d\vec{\sigma}_1, d\vec{\sigma}_2$, separated by a distance R , through which an incoherent beam of radiant energy propagates along a ray vector \hat{n} . Let θ_1, θ_2 be the angles between \hat{n} and each of the surface's normals. Then the solid angle subtended by each area element at the opposite end is

$$d\Omega_i = \frac{d\vec{\sigma}_i \cdot \hat{n}}{R^2} = \frac{d\sigma_i \cos \theta_i}{R^2} , \quad i = 1, 2 .$$

It follows that $d\Omega_1 d\sigma_2 \cos \theta_2 = d\Omega_2 d\sigma_1 \cos \theta_1$.

Since it was assumed that the beam passing through $d\vec{\sigma}_1$ and $d\vec{\sigma}_2$ is contained entirely within each area element, we conclude from energy conservation that the power $d\Phi$ passing through both areas is the same. Then $d^2\Phi_1 = d^2\Phi_2$ and one obtains for the radiance L_i at each element

$$L_1 = \frac{d^2\Phi}{d\Omega_2 (d\sigma_1 \cos \theta_1)} = \frac{d^2\Phi}{d\Omega_1 (d\sigma_2 \cos \theta_2)} = L_2 .$$

L is thus conserved along a ray within an homogeneous and isotropic medium. This is why radiance is a useful concept for describing energy transfer.

5.1.3 Transfer of radiant energy

Let a radiating source be characterised by its radiance L . Then the *power flux* S emitted by the source of radiance L and passing through an area element $d\sigma$ is given by an integration over the solid angle Ω_s subtended by the source

$$S = \int_{\Omega_s} d\Omega \cos \theta L(\theta, \phi) , \quad (5.5)$$

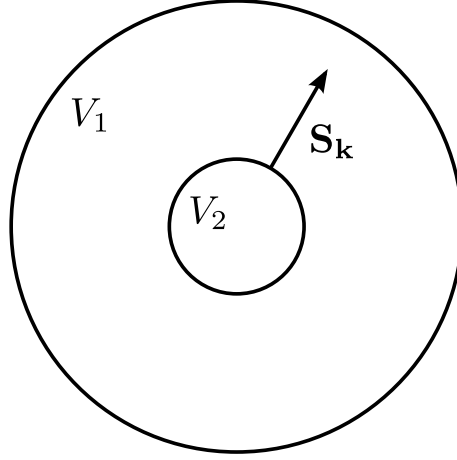
where θ is the angle between the normal $d\vec{\sigma}$ to the area element and the axis \hat{n} of Ω_s , compare with Fig. 5.1. Accordingly, the *total power* is found by integrating S_σ over a total area A of a detecting device

$$\Phi = \int_A d\sigma S_\sigma . \quad (5.6)$$

Note that the linear superposition of power is only possible by assuming no interference effects, that is, by assuming *incoherent radiation*. Since we will be dealing with *thermalized radiation*, this assumption will be met ideally.

5.1.4 Radiance formula for thermalized black-body emitters

We will now derive the known Planck radiance formula for black-body emitters in thermal equilibrium with radiation [54]. Special attention will be paid to the assumptions under which the derivation holds, and no special dispersion law will be singled out. We believe it

Figure 5.2: Spherical volumes V_1 and V_2

necessary to do this calculation in detail since most presentations in the literature assume U(1) dispersion relations. The dispersion law for the U(1) photon is just the linear function $\omega_{\mathbf{k}} = c|\mathbf{k}|$, but in the SU(2) case, $\omega_{\mathbf{k}} = \sqrt{\mathbf{k}^2 + G}$ and it is not clear that the classical U(1) result for the black-body radiance remains valid, since the functional dependence of the energy density for each Fourier mode of its wave vector is nontrivial (see section 3.5). In the following, in order to write thermalized radiation as a sum over plane waves, we will also need the results from Appendix B.

Consider a spherical black-body surface volume element ∂V_2 of radius r_2 positioned at the centre of an isothermal spherical black enclosure V_1 at the same temperature, and let the surfaces $\partial V_1, \partial V_2$ be thermally coupled by exchange of radiant energy. Thermal coupling must hold for every *available* mode of the cavity, so thermal equilibrium must hold for available mode individually. Assuming *energy and charge conservation*, the *continuity equation*

$$\partial_t \int_V d^3\mathbf{x} \rho + \oint_{\partial V} d\sigma \cdot \mathbf{S} = 0, \quad (\text{B.58})$$

must hold, and the radiant power emitted by ∂V_2 in the mode corresponding to the wave vector \mathbf{k} and collected by ∂V_1 must be

$$\Phi_{\mathbf{k} \ 2 \rightarrow 1} = -\partial_t Q_{\mathbf{k} \ 2} = -\partial_t \int_{V_2^c} d^3x \rho_{\mathbf{k}} = \oint_{\partial V_2} d\vec{\sigma} \cdot \mathbf{S}_{\mathbf{k}}. \quad (5.7)$$

Here the integration volume V_2^c is the volume bounded by ∂V_2 and infinity. From the symmetry of the problem and thermodynamical equilibrium, the Poynting vector \mathbf{S} of the thermalized electromagnetic field at ∂V_2 is normal to the surface, and constant everywhere. This allows us to write the spectral expression (5.7) as

$$\Phi_{\mathbf{k} \ 2 \rightarrow 1} = |\mathbf{S}_{\mathbf{k}}| \oint_{\partial V_2} d\sigma = |\mathbf{S}_{\mathbf{k}}| 4\pi r_2^2, \quad (5.8)$$

where $|\mathbf{S}_{\mathbf{k}}|$ is the magnitude of the Poynting vector for the mode \mathbf{k} at the boundary ∂V_2 .

Consider now the spectral power $\Phi_{\mathbf{k}1 \rightarrow 2}$ emitted by ∂V_1 and absorbed at ∂V_2 . Using (5.6), we may write it as

$$\Phi_{\mathbf{k}1 \rightarrow 2} = \int_{\partial V_2} d\sigma \int_{\Omega_1} d\Omega \cos \theta_n L_{\mathbf{k}}(\theta, \phi), \quad (5.9)$$

where θ_n is the angle between the normals of each area element at ∂V_2 and the solid angle $\Omega_1 = 4\pi$ subtended by ∂V_1 . From spherical symmetry, $\theta_n = 0$. Further, it is easy to show [22] that for the black-body emitter, its spectral radiance $L_{\mathbf{k}bb}$ must, by definition, be *independent* of the polar angles θ, ϕ

$$L_{\mathbf{k}}(\theta, \phi) = L_{\mathbf{k}bb}(\theta, \phi) = L_{\mathbf{k}bb}(0, 0) = L_{\mathbf{k}bb}. \quad (5.10)$$

We may then write

$$\Phi_{\mathbf{k}1 \rightarrow 2} = \int_{\partial V_2} d\sigma \int_{\Omega_1} d\Omega L_{\mathbf{k}bb} = 4\pi L_{\mathbf{k}bb} \int_{\partial V_2} d\sigma = 16\pi^2 L_{\mathbf{k}bb} r_2^2. \quad (5.11)$$

Since we have assumed thermalization for each available mode \mathbf{k} in the cavity, it follows that $\Phi_{\mathbf{k}2 \rightarrow 1} = \Phi_{\mathbf{k}1 \rightarrow 2}$, and we obtain a general expression for the *spectral black-body radiance* $L_{\mathbf{k}bb}$ in a thermalized cavity

$$L_{\mathbf{k}bb} = \frac{1}{4\pi} |\mathbf{S}_{\mathbf{k}}|. \quad (5.12)$$

Our conclusion is also valid for any other geometrical configuration. This can be argued as follows.

In general, cavity geometry influences the homogeneity and isotropy of thermal radiation inside the enclosure. For a rectangular cavity of side lengths $L_i, i = 1, 2, 3$, and volume $V = L_1 L_2 L_3$, for example, the correction $\delta D(\nu)$ caused by *geometric discretization effects* to the ideal *spectral density* $D_0(\nu) = \frac{8\pi V}{c} \left(\frac{\nu}{c}\right)^2$ of electromagnetic modes in a lossless closed cavity of same volume V is given by the expression (in SI units) [4]

$$\frac{\delta D(\nu)}{D_0(\nu)} = - \left(\frac{c}{\nu}\right)^2 \frac{1}{8\pi V} (L_1 + L_2 + L_3). \quad (5.13)$$

But by choosing the geometric dimensions of the cavity to be large enough, these discretization effects can be made arbitrary small in the spectral region of interest. With this in mind, here and in the following we will always presume the cavity to be large enough so that homogeneity and isotropy may be assumed up to any order.

Take now a black-body cavity with arbitrary geometry, and choose an spherical infinitesimal volume element dV_0 positioned at a point r_0 inside the enclosure. In thermal equilibrium, the radiation field is homogeneous and isotropic, so that the propagation of radiation from the cavity walls through dV_0 may be modelled by assuming an outer spherical surface S_0 centered in r_0 emitting radially at dV_0 . By the same argument, since dV_0 encloses homogeneous isotropically propagating thermal radiation, it may be seen as a spherical black-body emitting at S_0 . But this results in exactly the same geometrical configuration as before. We conclude that for a cavity with arbitrary geometry and sufficiently large dimensions¹ that discretization effects can be ignored, with walls in *thermal equilibrium with the radiation field* equation (5.12) holds.

¹What "sufficiently large" means depends of course on the cavity geometry. In this work, we restrict ourselves to rectangular cavities, where corrections are given by (5.13).

We now use the results of Appendix B to express L_{bb} as an integral over Fourier modes. Recall the expression for the *energy density* ρ of *thermalized* U(1) photon radiation at temperature $T \equiv \beta^{-1}$, first derived by Planck [54] (here written in natural units $\hbar = c = k_B = 1$)

$$\rho(\beta) = 2 \int \frac{d^3\mathbf{k}}{(2\pi)^3} \frac{\omega_{\mathbf{k}}}{e^{\beta\omega_{\mathbf{k}}} - 1}. \quad (5.14)$$

To describe the both the thermalized U(1) and SU(2) photon field using the expressions derived in Appendix B, we demand that equation

$$\rho = \frac{Q}{V} = 2 \frac{1}{V} \int \frac{d^3\mathbf{k}}{(2\pi)^3} (2N_k^2 \omega_{\mathbf{k}}) \omega_{\mathbf{k}}, \quad (B.47') \quad (5.47')$$

which gives the energy density of a given U(1) photon configuration in vacuum (defined by N_k), to coincide with (5.14). The factor 2 in (B.47') is due to summing over two transverse polarization states. The energy density of the SU(2) photon gas is given by (B.59), which sums only over *transverse* polarization states, since the longitudinal polarization, which has a very narrow wave vector support, cannot transport energy (see section 3.5.5). Equation (B.59) has the same form of (B.47'), but with $\omega_{\mathbf{k}}$ given by the SU(2) transverse dispersion law (3.34) (written here in SI units)

$$(\hbar\omega_{\mathbf{p}})^2 = (c\mathbf{p})^2 + G(\omega, \mathbf{p}; T, \Lambda). \quad [J^2] \quad (5.15)$$

That is, we can use the same spectral decomposition (B.47') when describing the total field energy in both theories, with the only replacement being the non-trivial dispersion law for the photon of SU(2) Yang-Mills thermodynamics (see chapter 3). This is important, so we will repeat it here: *We use the same expression (B.47') for both the U(1) and the non-abelian SU(2) Yang-Mills photon*, the vast dynamical difference between both is already taken into account by the different dispersion laws.

Comparing both (5.14) and (B.47') gives us the correct *thermal normalization factors* for the spectral decomposition (B.47')

$$N_k = \sqrt{\frac{V n_B(\beta\omega_{\mathbf{k}})}{2\omega_{\mathbf{k}}}}, \quad (5.16)$$

where $n_B(\beta\omega_{\mathbf{k}}) \equiv (e^{\beta\omega_{\mathbf{k}}} - 1)^{-1}$ is the *Bose-Einstein distribution function*.

The *spectral energy density* is then given as

$$\begin{aligned} \frac{Q}{V} &= \int d\mathbf{k} \rho_{\mathbf{k}} = 2 \int \frac{d^3\mathbf{k}}{(2\pi)^3} n_B(\beta\omega_{\mathbf{k}}) \omega_{\mathbf{k}} = \frac{1}{\pi^2} \int dk \mathbf{k}^2 n_B(\beta\omega_{\mathbf{k}}) \omega_{\mathbf{k}}, \\ \implies \rho_{\mathbf{k}} &= \frac{1}{\pi^2} n_B(\beta\omega_{\mathbf{k}}) \mathbf{k}^2 \omega_{\mathbf{k}}. \end{aligned} \quad (5.17)$$

The *energy propagation velocity* $\mathbf{v}_{\mathbf{k}}$ of a mode \mathbf{k} can be defined [7] so that

$$\rho_{\mathbf{k}} \mathbf{v}_{\mathbf{k}} = \mathbf{S}_{\mathbf{k}}. \quad (5.18)$$

For each mode, it can be shown that this propagation velocity, by definition, is just the k -gradient of the dispersion law [7]

$$\mathbf{v}_{\mathbf{k}} = \nabla_{\mathbf{k}} \omega_{\mathbf{k}}, \quad (5.19)$$

whatever the functional expression for the dispersion law is.

Inserting (5.17), (5.18), and (5.19) into (5.12), we obtain the *spectral radiance of a black-body emitter in thermalized radiation*

$$L_{\mathbf{k} \, bb} = \frac{1}{4\pi} |\rho_{\mathbf{k}} \nabla_{\mathbf{k}} \omega_{\mathbf{k}}| = \frac{1}{4\pi^3} \frac{\omega_{\mathbf{k}}}{e^{\beta \omega_{\mathbf{k}}} - 1} \mathbf{k}^2 |\partial_{\mathbf{k}} \omega_{\mathbf{k}}|. \quad (5.20)$$

Using (5.2), we can also write the same expression as a function of *frequency*. The *radiance per frequency interval of a black-body emitter in thermalized radiation* is then, written in natural units, given as

$$L_{\omega \, bb} = \frac{1}{4\pi^3} \frac{\omega_{\mathbf{k}}}{e^{\beta \omega_{\mathbf{k}}} - 1} \mathbf{k}^2. \quad [\text{eV}^4] \quad (5.21)$$

To write (5.21) in SI units, remember that the (angular) frequency and wave vector are rescaled as $\omega_{\mathbf{k}} \rightarrow \hbar \omega_{\mathbf{k}}$, $\mathbf{k} \rightarrow c\hbar \mathbf{k}$ and the inverse temperature as $\beta \rightarrow \frac{1}{k_B T}$. Moreover, radiance has dimension eV^4 in natural units, so we need to divide expression (5.21) with $(\hbar c)^2$ to return to SI units. We obtain

$$L_{\nu \, bb} = \frac{1}{2\pi^2} \frac{h\nu}{e^{h\nu/k_B T} - 1} k^2. \quad [\text{W m}^{-2} \text{sr}^{-1} \text{Hz}^{-1}] \quad (5.22)$$

The additional factor of 2π comes from the change of variable $d\omega \rightarrow 2\pi d\nu$. The formulae (5.21), (5.22) characterise radiation in thermal equilibrium with a black-body, independently of any functional relation between \mathbf{k} and $\omega_{\mathbf{k}}$.

Later, (5.22) will be used to calculate the *power output* of any measuring device observing thermal radiation.

5.1.5 Radiance of the SU(2) thermal gas

In this section we compare radiance functions of both the U(1) and SU(2) theories. The radiance function $L_{\nu \, bb}^{U(1)}(\nu, T)$ for the U(1) photon gas in SI units can be read off from Eq. (5.22). Inserting the U(1) dispersion law $\hbar \omega_{\mathbf{k}} = c\hbar |\mathbf{k}| = h\nu$ results in the expression

$$L_{\nu \, bb}^{U(1)}(\nu, T) = \frac{2h}{c^2} \frac{\nu^3}{e^{h\nu/k_B T} - 1}. \quad [\text{W m}^{-2} \text{sr}^{-1} \text{Hz}^{-1}] \quad (5.23)$$

To write the radiance function $L_{\nu \, bb}^{SU(2)}(\nu, T)$ for the SU(2) case, we recall the SU(2) dispersion relation (3.34) $\hbar \omega_{\mathbf{k}} = \sqrt{(c\hbar \mathbf{k})^2 + G(\omega, \hbar \mathbf{k}; T, \Lambda)}$. Recall that the SU(2) photon gas shows a *screening region* so that propagation is forbidden below a cutoff frequency ν^* , see section 3.5. That is, the only modes allowed in the cavity are those with frequencies $\nu > \nu^*$. That only those modes can contribute to the spectral radiance is ensured by multiplying with a θ -function. In the end, we obtain

$$\begin{aligned} L_{\nu \, bb}^{SU(2)}(\nu, T) &= \frac{2h}{c^2} \frac{\nu^3}{e^{h\nu/k_B T} - 1} \left(1 - \frac{c^2 G}{(h\nu)^2}\right) \theta(\nu - \nu^*) \\ &= L_{\nu \, bb}^{U(1)} \left(1 - \frac{c^2 G}{(h\nu)^2}\right) \theta(\nu - \nu^*). \end{aligned} \quad [\text{W m}^{-2} \text{sr}^{-1} \text{Hz}^{-1}] \quad (5.24)$$

Note that outside the screening region, that is, for $\nu > \nu^*$, the radiance (5.24) for the SU(2) gas factorizes into the factor $(1 - \frac{c^2 G}{(h\nu)^2})$ times the U(1) radiance (5.23). As discussed in [46, 59], the function G goes to zero power-like for increasing temperature and exponentially for increasing frequency. So we expect a return to the U(1) case for high enough temperatures and energies, since in that limit the factor $(1 - \frac{c^2 G}{(h\nu)^2}) \rightarrow 1$, $\nu^* \rightarrow 0$, and both radiance functions $L_{\nu bb}^{U(1)}(\nu, T)$ and $L_{\nu bb}^{SU(2)}(\nu, T)$ become indistinguishable.

In the case of low energy and temperature, however, we do expect the SU(2) photon gas to show considerable deviation from the U(1) case. This suggests the possibility of *experimental detection* of the SU(2) gas by radiation measurements at low frequency and temperature. This possibility will be explored further in section 5.4.

Examples of the calculated radiance for different temperatures are plotted in figures 5.3 to 5.6. To plot the SU(2) radiance, the cutoff frequency ν^* was calculated as shown in section 3.5.4. Note the screening region at low frequencies where the radiance of the SU(2) gas vanishes. The *crossover frequency* ν_c , discussed in section 3.5.4 is also easily visible in all plots.

5.2 Basics of the theory of antennas

In order to test experimentally the most important prediction of the SU(2) photon theory, and thus ascertain the presence of a thermodynamical ground state composed by topological field configurations as described in chapter 3, we need to be able to detect thermal radiation at low frequencies and temperatures. In the preceding section we derived an expression for the radiance of black-body emitters which characterises energy propagation. Now we turn to the problem of how to measure such an altered propagation.

The experimental science and technology of the measurement of electromagnetic radiation is called *radiometry* [67]. A typical radiometric set up always consists of a *radiation source*, an *aperture* or *optical system*, and a *detector*. The aperture collects the radiation from the source and redirects it to the detector. The detector converts radiation into a well defined signal that can then be measured within a certain precision and further processed.

In the microwave region of the electromagnetic spectrum – which, as we will later see, is where the predicted differences between U(1) and SU(2) propagation occur – an *antenna* is often used as the aperture. An antenna is defined [40, 67] as the region of transition between an electromagnetic wave propagating in free space and a guided wave propagating in a *transmission line* ².

In this section, we review some concepts relating to energy collection through antennas. The most important result will be an expression for the *antenna temperature* T_A , which quantifies the power output of an antenna in relation to its incident thermal radiation, derived here without assuming any explicit dispersion law. The detection of the collected thermal radiation is the subject of section 5.3.

Further properties that characterise antennas are geometric in nature, such as the *antenna radiation pattern* and the *antenna effective area*. Geometric factors also determine such coefficients as *beam efficiency*, which characterises undesired signal contribution by side-lobe radiation. These characteristics will play a minor role for us since we will be

²A *transmission line* is a device allowing for propagation of radio-frequency energy from one point to another. Antennas *radiate* or *receive* energy, while transmission lines *transport* energy. See also section 5.3

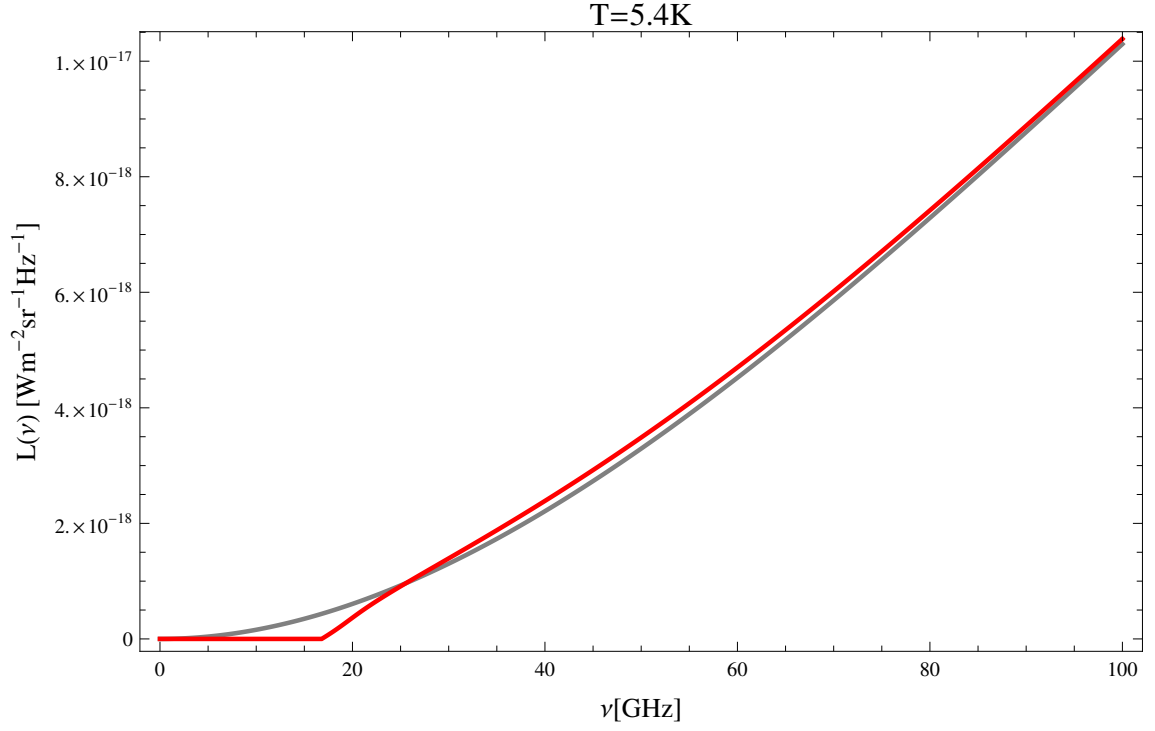


Figure 5.3: Comparison of the spectral radiance of an $SU(2)$ photon gas (red) and a $U(1)$ gas (grey) at a temperature $T=5.4\text{K}$. Note the spectral gap in the low-frequency region.

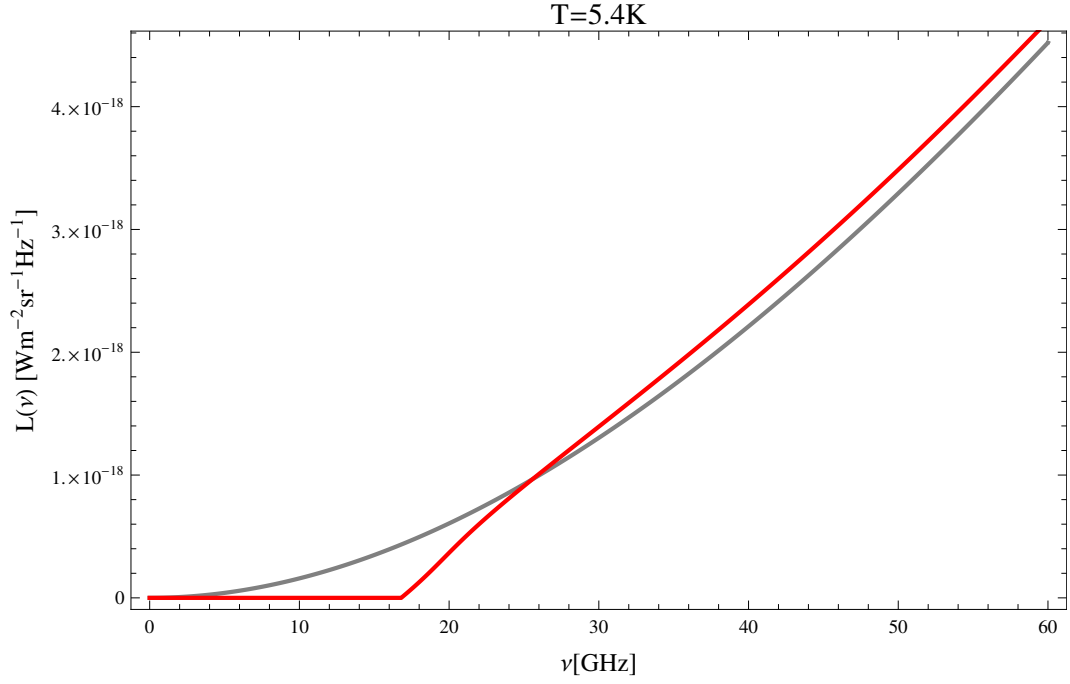


Figure 5.4: Zoom-in of figure 5.3

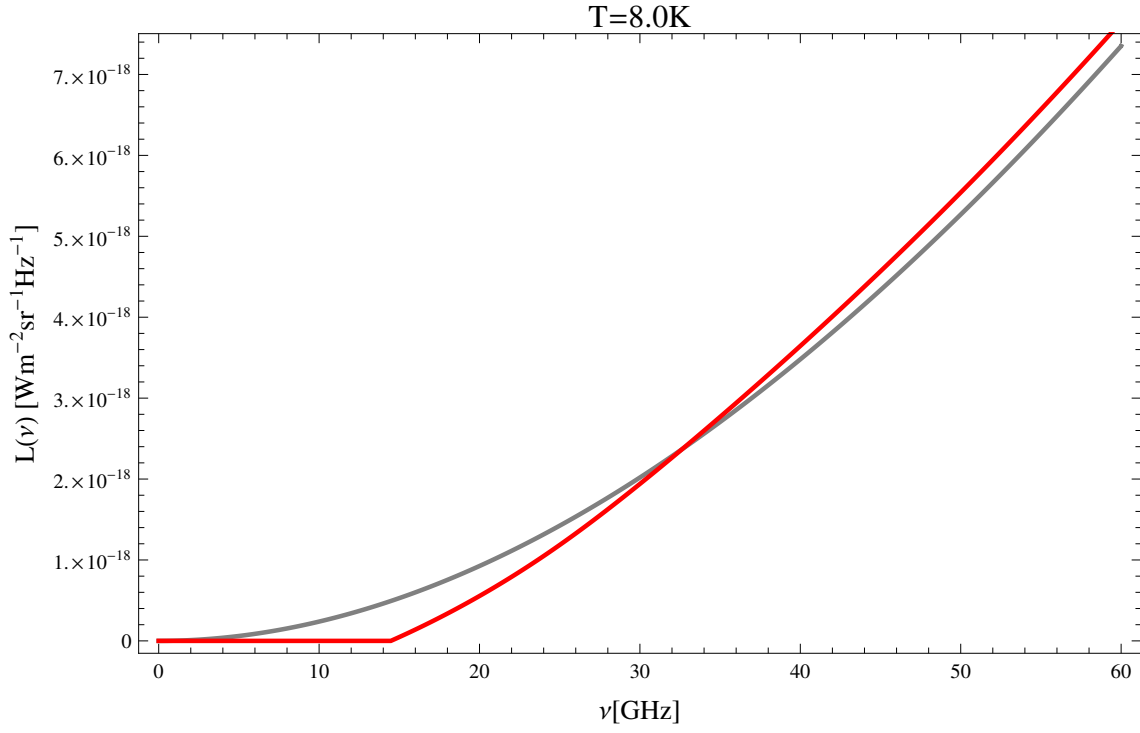


Figure 5.5: Comparison of the spectral radiance of an SU(2) photon gas (red) and a U(1) gas (grey) at a temperature $T=8.0\text{K}$. Note the spectral gap in the low frequency region.

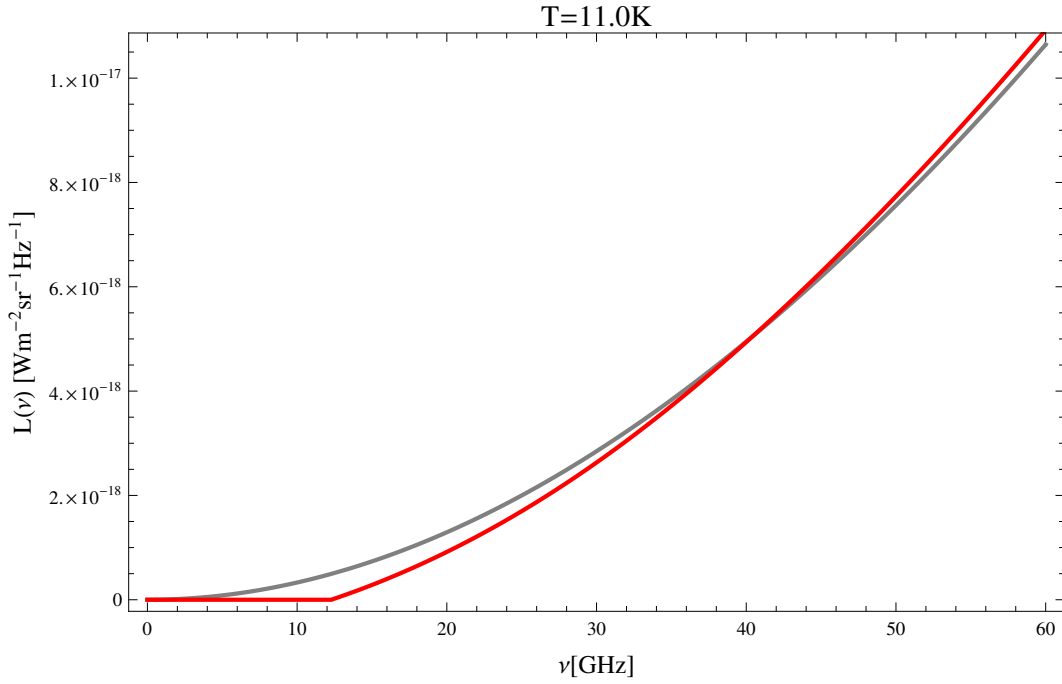


Figure 5.6: Comparison of the spectral radiance of an SU(2) photon gas (red) and a U(1) gas (grey) at a temperature $T=11.0\text{K}$. Note the spectral gap in the low frequency region.

dealing with isotropic and homogeneous radiation. Still, these geometric factors need to be understood before we arrive at a formula for T_A . We briefly review these subjects before arriving at our main expression for the antenna temperature.

5.2.1 Antenna parameters

This section serves as a quick introduction to all antenna parameters we will require in the following sections to describe and calculate through our experiment. A thorough review of the subject can be found in [40].

Consider a transmitting antenna placed at the origin. For sufficiently large r , we may consider the radiated modes as plane waves. This zone is called the *far field*, and we always work in this limit unless stated otherwise.

With the antenna positioned at the origin, we expect the far field electric and magnetic vectors to be mutually perpendicular and normal to the unit vector \hat{r} . The Poynting vector \mathbf{S} must be radial. In the case of isotropic antenna radiation, the total radiated power given by integrating over the surface of a spherical volume V centered at the origin becomes in this limit

$$\Phi = \oint_{\partial V} d\vec{\sigma} \cdot \mathbf{S} = 4\pi r^2 S_r, \quad (5.25)$$

since the radial component S_r is constant over all directions. In general, antenna radiation patterns are not isotropic, and almost always distributed around a narrow solid angle called the *main lobe*. S_r is no longer isotropic and the polar dependency of antenna radiation is characterised by the *antenna radiation pattern*

$$F(r, \theta, \phi) \equiv r^2 S_r(\theta, \phi), \quad (5.26)$$

so that the total radiated power in the far field is given by

$$\Phi = \int d\Omega F(\theta, \phi), \quad (5.27)$$

where we have omitted the r -dependence, which in the far-field reduces to equation (5.26), $F(\theta, \phi) \equiv r^2 S_r$. For an isotropic antenna, (5.27) reduces, of course, to (5.25).

Imagine now a radiating antenna which we supply with *input power* P_i . From the second law of thermodynamics we may assume that a fraction of P_i is dissipated as heat from the antenna. Let P_o be the actual *radiated power* from the antenna aperture, and define the *antenna radiation efficiency* η as the ratio P_o/P_i . We can define a polar version of this factor as well, the *antenna gain function* $G(\theta, \phi)$, as the ratio between radiated power per solid angle $d\Phi/d\Omega = F(\theta, \phi)$ and total input power per solid angle $P_i/4\pi$

$$G(\theta, \phi) \equiv \frac{4\pi F(\theta, \phi)}{P_i}. \quad (5.28)$$

Defining the *normalized antenna radiation pattern*

$$F_n(\theta, \phi) = \frac{F(\theta, \phi)}{F(\theta, \phi)|_{\max}}, \quad (5.29)$$

the *pattern solid angle* Ω_P , which characterises the effective width of the radiation pattern,

$$\Omega_P \equiv \int_{4\pi} d\Omega F_n(\theta, \phi), \quad (5.30)$$

the *antenna directivity* $D(\theta, \phi)$

$$D(\theta, \phi) \equiv \frac{F_n(\theta, \phi)}{\frac{1}{4\pi} \int_{4\pi} d\Omega F_n(\theta, \phi)} = D_0 F_n(\theta, \phi), \quad (5.31)$$

and the *maximum directivity* D_0

$$D_0 \equiv \frac{4\pi}{\Omega_P} = \frac{4\pi}{\int_{4\pi} d\Omega F_n(\theta, \phi)} = \frac{4\pi S_r(\theta, \phi)|_{max}}{\int_{4\pi} d\Omega S_r(\theta, \phi)}, \quad (5.32)$$

we can write (5.28) as [67]

$$G(\theta, \phi) = \eta D_0 F_n(\theta, \phi) = \eta 4\pi \frac{F_n(\theta, \phi)}{\Omega_P}. \quad (5.33)$$

Thus an equation for the radiated power per solid angle emerges

$$\frac{d\Phi}{d\Omega} = \frac{P_i}{\Omega_P} \eta F_n(\theta, \phi). \quad (5.34)$$

Note that (5.34) depends linearly on the input power P_i . Moreover η , Ω_P and the polar angle dependency $F_n(\theta, \phi)$ are all intrinsic characteristics of the radiating antenna. That is, once they have been calibrated, the power output of an antenna is then fully determined by the input power P_i feeding the antenna.

So far we have considered *transmitting antennas*, and defined the antenna radiation pattern and directivity as the characterising angular distribution of *transmitted power*. What about the *power gain* of an antenna when collecting radiation? The *reciprocity theorem* [60, 70] shows that, under general assumptions (e.g. isotropy of the medium), the *transmitting* and *receiving* antenna parameters are the same. The directivity and radiation pattern characterise the *angular cross section* of the antenna, and it is the same for both transmission and reception of power. In this sense, problems of radiation emission and radiation detection by an antenna are *interchangeable*.

5.2.2 Antenna effective area

Power transmission and reception by an antenna may be described, in the far field at least, by borrowing from optics the idea of wave diffraction by a geometric aperture A . This results in the *Fresnel-Kirchhoff diffraction formula* [60], which reduces the computation of the antenna far field radiation, given the field at the physical antenna aperture A_P , to a scalar diffraction problem with *effective* geometric antenna aperture A_E . It is found that this effective aperture, or *effective area*, depends on the wavelength of the diffracted radiation. Since we would like to apply the same methods to the radiometry of SU(2) photons, we must be careful that these results should not depend *explicitly* on the dispersion law. This is a priori not clear and needs to be checked. That the Fresnel-Kirchhoff diffraction formula does not depend explicitly on a U(1) linear dispersion law and thus holds also for SU(2) photons by implicitly allowing for functional dependencies such as

(3.34) is checked in appendix C. Here we use this result to arrive at an expression for the *antenna effective area* which we need to relate electromagnetic fields in the far field to electromagnetic fields in the aperture, to calculate the *incoming power* at the aperture. This is done by first calculating the *transmitted power* through the aperture, and then invoking the reciprocity theorem. We follow somewhat the presentation in [67] but without assuming any explicit dispersion law.

Consider a transmitting antenna, with its physical aperture area A_P , and a monochromatic field distribution $E_{\mathbf{k}}$ of constant phase defined over the surface A_P . This is realised by having the Poynting vector of the monochromatic planar wave be normal to the aperture surface. We say that the aperture is *illuminated* by the monochromatic field distribution $E_{\mathbf{k}}$ of constant phase. Evaluating the total power Φ crossing through the aperture gives

$$\begin{aligned}\Phi &= \int_A dx_a dy_a \hat{n} \cdot \mathbf{S}_{\mathbf{k}}(x_a, y_a) = \int_A dx_a dy_a S_{\mathbf{k}}(x_a, y_a) \\ &= \frac{1}{2} \frac{|\mathbf{k}|}{\omega_{\mathbf{k}}} \int_{A_P} dx_a dy_a |E_{\mathbf{k}}(x_a, y_a)|^2,\end{aligned}\quad (5.35)$$

where \hat{n} is the normal vector to the aperture, and we have expressed the modulus of the Poynting vector $S_{\mathbf{k}}$ by that of the electric field (compare with (B.64)). The integration variables x_a and y_a parametrize the aperture surface.

Because of energy conservation, (5.35) must be equal to the power radiated in the far field by the antenna, where radial symmetry holds and the monochromatic field propagates as an spherical wave after diffraction through the physical aperture

$$\Phi = \int_{4\pi} d\Omega r^2 S_r(\theta, \phi). \quad (5.36)$$

Hence

$$\int_{4\pi} d\Omega S_r(\theta, \phi) = \frac{1}{2r^2} \frac{|\mathbf{k}|}{\omega_{\mathbf{k}}} \int_{A_P} dx_a dy_a |E_{\mathbf{k}}(x_a, y_a)|^2. \quad (5.37)$$

Take the maximum value S_0 of the power density radiated by the antenna. Assume a symmetric radiation pattern distribution along the z-axis (for example that of a horn antenna), then the maximum can be calculated by using equations (C.18), (C.17) and setting $\theta = \phi = 0$ [67]

$$S_0 = S_{\mathbf{k}}(0, 0) = \frac{1}{8\pi^2} \frac{|\mathbf{k}|^2}{r^2} \frac{|\mathbf{k}|}{\omega_{\mathbf{k}}} |h_{\mathbf{k}}(0, 0)|^2 = \frac{1}{8\pi^2} \frac{|\mathbf{k}|^2}{r^2} \frac{|\mathbf{k}|}{\omega_{\mathbf{k}}} \left| \int_{A_P} dx_a dy_a E_{\mathbf{k}}(x_a, y_a) \right|^2. \quad (5.38)$$

Inserting both (5.37) and (5.38) in (5.32) gives

$$D_0 = \frac{1}{\pi} |\mathbf{k}|^2 \frac{\left| \int_{A_P} dx_a dy_a E_{\mathbf{k}}(x_a, y_a) \right|^2}{\int_{A_P} dx_a dy_a |E_{\mathbf{k}}(x_a, y_a)|^2}. \quad (5.39)$$

This is the *maximum directivity* D_0 for a monochromatic field $E_{\mathbf{k}}$ diffracting through the physical antenna aperture A_P . For *constant illumination*, $E_{\mathbf{k}} = \text{const}$, the above equation reduces to

$$D_0 = \frac{1}{\pi} |\mathbf{k}|^2 A_P. \quad (5.40)$$

Otherwise, from Schwartz's Inequality for complex valued functions follows

$$\left| \int_{A_P} dx_a dy_a E_{\mathbf{k}}(x_a, y_a) \right|^2 \leq A_P \int_{A_P} dx_a dy_a |E_{\mathbf{k}}(x_a, y_a)|^2$$

This motivates the definition of an *effective antenna aperture* A_E [67]

$$A_E \equiv \frac{\left| \int_{A_P} dx_a dy_a E_{\mathbf{k}}(x_a, y_a) \right|^2}{\int_{A_P} dx_a dy_a |E_{\mathbf{k}}(x_a, y_a)|^2}, \quad (5.41)$$

so that in general $A_E \leq A_P$ and

$$D_0 = \frac{1}{\pi} |\mathbf{k}|^2 A_E. \quad (5.42)$$

Each monochromatic mode \mathbf{k} interacts with the physical antenna as if its aperture had the *effective area* $A_E = A_{E, \mathbf{k}}$ and *directivity* $D = D_{0, \mathbf{k}} F_{n, \mathbf{k}}(\theta, \phi)$, see Eqs. (5.41) and (5.42). In the effective Fresnel-Kirchhoff theory, the antenna *pattern solid angle* also becomes a function of wave number \mathbf{k}

$$\Omega_{P, \mathbf{k}} = \frac{4\pi^2}{A_{\mathbf{k}}} \frac{1}{|\mathbf{k}|^2}. \quad (5.43)$$

Recall from the reciprocity theorem that this also holds for an antenna *receiving* power.

Now let an antenna sit at the origin while collecting monochromatic power of wave number \mathbf{k} from a source emitting with radiance $L_{\mathbf{k}}$ (with respect to the origin). What is the power output P_A of the antenna? From (5.5) and (5.6) we can write the expression for spectral power as

$$\Phi_{\mathbf{k}} = \int_A d\sigma \int_{\Omega_s} d\Omega \cos \theta L_{\mathbf{k}}(\theta, \phi).$$

Before applying this formula to our antenna problem, we must take the area integrated over as the effective antenna area $A = A_{E, \mathbf{k}}$. Also, we must replace $\cos \theta$ with $\eta F_{n, \mathbf{k}}$, since the portion of energy passing through the effective area is no longer given by projecting the incoming ray to the surface normal, but by the normalized radiation pattern multiplied with the radiation efficiency factor. It is $\eta F_{n, \mathbf{k}}$ that projects energy collection, see (5.34). Finally we arrive at a formula for the monochromatic power $P_{\mathbf{k}}$ collected by the antenna

$$P_{\mathbf{k}} = A_{\mathbf{k}} \int_{\Omega_s} d\Omega \eta F_{n, \mathbf{k}}(\theta, \phi) L_{\mathbf{k}}(\theta, \phi), \quad (5.44)$$

with Ω_s the solid angle subtended by the source. Then the *total power output* P_A received by an antenna of radiation efficiency η and radiation pattern $F_n(\theta, \phi)$ from a source with radiance $L_{\mathbf{k}}(\theta, \phi)$ subtending the solid angle Ω_s results from integrating over all available modes

$$P_A = \eta \int d|\mathbf{k}| P_{\mathbf{k}} = \eta \int dk A_{\mathbf{k}} \int_{\Omega_s} d\Omega F_{n, \mathbf{k}}(\theta, \phi) L_{\mathbf{k}}(\theta, \phi). \quad (5.45)$$

5.2.3 Antenna temperature

The concept of *antenna temperature* was first introduced by R. Dicke in a famous 1946 article on microwave radiometry [10], where the power output P_A of an antenna enclosed by a perfect black-body cavity was related to the temperature T of the radiation inside the enclosure, by equating P_A with the thermal (Nyquist) noise of a matched resistor. Here we re-derive the relation between radiation temperature and antenna power output, which will be needed to characterise our experiment.

To calculate the total power output P_A of an antenna *completely immersed* in thermal radiation inside a black cavity, we integrate (5.45) over the full solid angle $\Omega_s = 4\pi$ and each available mode \mathbf{k} . The thermal radiance is given by $L_{\mathbf{k} \text{ } bb}$. Since thermal radiation is unpolarized by definition, and antennas are *polarized* receivers [40, 67] we must divide expression (5.45) by two, since the antenna can only pick one of the two available *transverse polarizations*. This gives

$$\begin{aligned} P_A &= \frac{1}{2} \eta \int dk A_{\mathbf{k}} \int_{4\pi} d\Omega F_{n,\mathbf{k}}(\theta, \phi) L_{\mathbf{k} \text{ } bb} \\ &= \frac{1}{2} \eta \int dk L_{\mathbf{k} \text{ } bb} A_{\mathbf{k}} \int_{4\pi} d\Omega F_{n,\mathbf{k}}(\theta, \phi) , \end{aligned}$$

which by (5.30) and (5.43) simplifies as

$$P_A = \frac{1}{2} \eta \int dk L_{\mathbf{k} \text{ } bb} A_{\mathbf{k}} \Omega_{P,\mathbf{k}} = \frac{1}{2} \eta \int dk L_{\mathbf{k} \text{ } bb} \frac{4\pi^2}{|\mathbf{k}|^2} .$$

Changing variables to cancel the squared wavelength factor $\lambda^2 \equiv \frac{(2\pi)^2}{|\mathbf{k}|^2}$ we obtain finally

$$\begin{aligned} P_A &= \frac{1}{2} \eta \int d\omega_{\mathbf{k}} L_{\omega \text{ } bb} \frac{4\pi^2}{|\mathbf{k}|^2} \\ &= \frac{1}{2\pi} \eta \int d\omega_{\mathbf{k}} \frac{\omega_{\mathbf{k}}}{e^{\beta\omega_{\mathbf{k}}} - 1} . \end{aligned} \tag{5.46}$$

Note that since equation (5.46) is expressed only in terms of the frequency, it is *independent of any specific dispersion law for photons in the thermal gas*. The antenna power output P_A is only sensible to the available propagation modes of the thermal gas, which constrain the frequency spectrum available for integration in (5.46).

To write (5.46) in SI units recall again that converting from natural units one has $\omega_{\mathbf{k}} \rightarrow h\nu$, $\beta \rightarrow \frac{1}{k_B T}$. The ratio η is unit-less. To have appropriate dimensions, expression (5.46) must be divided by \hbar . Then the *total power* P_A collected by an antenna of radiation efficiency η fully immersed in thermal radiation is written in SI units as

$$P_A = \eta \int d\nu \frac{h\nu}{e^{h\nu/k_B T} - 1} . \tag{5.47}$$

In the *Rayleigh-Jeans regime* $h\nu \ll k_B T$, and we can approximate the exponential function in the denominator of (5.46) as $e^{h\nu/k_B T} = 1 + \frac{h\nu}{k_B T} + \dots$. In this regime,

$$P_A = k_B \eta T \int d\nu . \tag{5.48}$$

Let the antenna be connected to a receiver of bandwidth $\Delta\nu \equiv \nu_2 - \nu_1$, with $\nu_2 > \nu_1$ and both frequencies inside the Rayleigh-Jeans zone. If $\Delta\nu$ lies *entirely within the available cavity frequencies*, the power delivered from the antenna then results from integrating (5.48) over the whole bandwidth $\Delta\nu$

$$P_A = k_B \eta T \Delta\nu. \quad (5.49)$$

This simple but important equation confirms what we discussed before: The *output power* at the terminals of an antenna *fully immersed in thermal radiation* is *solely determined by the radiation cavity temperature T and accessible bandwidth $\Delta\nu$* . Let the radiation temperature in the cavity be $T = T_R$. We can then define the *temperature* T_A of an antenna placed inside the cavity, collecting radiation over a finite bandwidth $\Delta\nu$, as

$$T_A = \eta T_R = \frac{P_A}{k_B \Delta\nu}. \quad (5.50)$$

If $\Delta\nu$ does not lie within the region of allowed frequencies, there is no power output possible, $P_A = 0$ and the antenna temperature is zero.

The thermal U(1) gas

For the U(1) thermal photon gas, propagation over the entire spectrum $\nu > 0$ is possible (up to geometrical discretization effects which we may ignore, as discussed in section 5.1.4). Then (5.49) for the U(1) case is just

$$P_A^{U(1)} = k_B \eta T \Delta\nu. \quad (5.51)$$

The thermal SU(2) gas

As we saw in section 3.5, the frequency spectrum available to the SU(2) photon is bounded from below by a *cutoff frequency* $\nu^*(T)$. Below ν^* , *no propagation is possible*. Let the detectable antenna bandwidth be $\Delta\nu = \nu_2 - \nu_1 > 0$. An antenna completely bathed in thermal SU(2) radiation will provide the power output

$$P_A^{SU(2)} = \begin{cases} k_B \eta T \Delta\nu & \text{if } \nu_1 \geq \nu^* \\ k_B \eta T (\nu_2 - \nu^*) & \text{if } \nu_1 < \nu^* < \nu_2 \\ 0 & \text{otherwise.} \end{cases} \quad (5.52)$$

If the bandwidth $\Delta\nu$ lies entirely below the cutoff frequency ν^* , the antenna power output of a thermal SU(2) photon gas is zero³. This is in contrast to the U(1) case (5.51) which always produces a non-zero antenna temperature proportional to the radiation temperature in the cavity and bandwidth. The SU(2) gas dynamics manifests themselves as an *antenna temperature gap* below ν^* . This is the *key experimental prediction* from SU(2) thermodynamics, as developed in chapter 3, that is accessible by radiometric means. To measure the antenna temperature some type of radiometer must be connected to the output of the antenna. Such experimental configurations are described in the next section.

³Up to antenna and receiver noise, of course. This is discussed in section 5.3.

5.3 Radiometer systems

Before tackling the problem of experimental detection of the antenna temperature gap described in section 5.2.3, we need to familiarise ourselves with basic radiometric techniques. The purpose of this section is to give a basic review of the subject, a deeper treatment can be found in the literature [67, 63]. First we introduce basic concepts, then we describe in brief the two radiometer configurations one could employ to measure SU(2) effects. In this section we always take the radiometer bandwidth $\Delta\nu$ to lie outside the screening region of the SU(2) gas and within the Rayleigh-Jeans zone. This is just to simplify our introductory review. Discussions about screening effects and their radiometric detection are left to section 5.4.

5.3.1 Basic definitions

A radiometer system is a radiation measurement device composed of an antenna coupled to a receiver. The receiver selects a bandwidth $\Delta\nu$ for detection, and produces a signal characterizing the collected radiation.

In the ideal case, *power radiometers* produce a voltage signal which is directly proportional to the power output of the connected antenna, and by way of (5.49) also proportional to the antenna temperature

$$V_o = c G P_A = c G \Delta\nu k_B T_A. \quad (5.53)$$

Here G is the *amplification factor* of the radiometer, and c a calibration factor. A correct calibration is of absolute necessity if T_A in (5.53) is to be interpreted as a temperature at all. Different calibration methods are discussed in [63, 67]. In the following, we assume that the radiometer has been correctly calibrated, and absorb the factor c into G .

In general, random noise (mostly thermal in nature) intrinsic to the radiometer apparatus will distort the output voltage (5.53), so that it is not a strictly linear function of the antenna output power P_A . It can be shown however [63, 67] that radiometer noise is well modelled by considering it as an additive contribution to the measured signal (the antenna power output). We thus define the *radiometer noise power* P_N as the *power that would be measured by the radiometer viewing a source at zero absolute temperature*.

We can also write P_N in terms of a temperature, the *radiometer noise temperature* $T_N \equiv P_N/(G \Delta\nu k_B)$. Thus, radiometer noise may be interpreted as an additional temperature T_N collected along with the antenna temperature T_A by an ideal noiseless radiometer. The noise power (noise temperature) is an intrinsic characteristic of the radiometer. Allowing for thermal noise, the total radiometer output power then reads

$$\begin{aligned} V_o &= G(P_A + P_N) = G \Delta\nu k_B (T_A + T_N), \\ &\equiv G \Delta\nu k_B T_o, \end{aligned} \quad (5.54)$$

where we have defined the *radiometer output temperature* $T_o = V_o/(G \Delta\nu k_B)$. The radiometer output temperature characterizes the *average* power output of a radiometer. Thermal noise contributes to the stochastic fluctuations in the power output. These are in turn characterized by the *radiometer sensitivity* ΔT_o , which gives the minimum detectable change in the radiometer temperature. In the case of thermal radiation, both radiome-

ter temperature T_o and sensitivity ΔT_o fully characterize the radiometer output⁴. In the following, we describe two useful radiometer configurations, and give the corresponding formulas for radiometer temperature and sensitivity.

5.3.2 Total power radiometer

The *total power radiometer* is the most basic type of radiometer designed to measure antenna temperature. Its design is sketched in figure 5.7. An antenna of total temperature T_A is coupled via a transmission line to a receiver consisting of four basic stages. The first is *signal amplification*, which is carried out by an amplifier of *gain* G . This is followed by *bandwidth selection* by a filter of narrow bandwidth $\Delta\nu$. In the *detection* stage, the input signal is converted to a measurable voltage. For a total power radiometer this is achieved by a semiconductor diode working as a *square law detector*: The diode output voltage is proportional to the input signal power $P_A + P_N$. In the fourth and final stage, the voltage signal coming out of the detector is *smoothed by integration* over a time period τ to reduce random fluctuations. This integrator effectively acts as a low pass filter, suppressing frequencies higher than $1/\tau$, where τ is the *radiometer integration period*. Note that the integrator causes the radiometer output to be *Gauss-distributed*, independently of the stochastic distribution of the signal. This can be understood as follows: A single integration over a period τ of a signal with arbitrary stochastic distribution is equivalent to taking the average of many single measurements of said signal. But from the central limit theorem, this average will tend to be *normally distributed*. The radiometer output after integrations is thus fully characterized by the average output signal and its variance, independently of the stochastic distribution of the input signal.

The noise performance of the radiometer system (antenna plus receiver) can be characterized the radiometer noise temperature T_N . A useful model for T_N is given below.

The total power radiometer as depicted in figure 5.7 is therefore fully characterized by specifying a few parameters. While the stages of bandwidth selection and time integration are self-explanatory, we believe the subjects of signal amplification and radiometer noise temperature merit some further discussion.

Signal amplification

Signal amplification in modern radiometers is realized by semiconductor devices. In the microwave region ($\nu \sim 1 - 100\text{GHz}$), High Electron Mobility Transistors (HEMT) are the ideal solid state amplifier because of high signal gain and low noise. HEMTs are a form of Field Effect Transistors (FETs) so constructed that its charge carriers are confined to a very narrow 2-dimensional layer, forming a *two-dimensional electron gas* (2-DEG). Transport properties of this 2-DEG are superior to that of a usual FET since, due to the absence of donor impurities, scattering is greatly reduced, thus higher electron mobility and low intrinsic noise is achieved [1, 60]. This advantages comes at a cost, however. HEMTs at cryogenic temperatures suffer from relatively large fluctuations in the amplification factor (see e.g. [16]). Let the amplification factor variate in time as $G(t) = G + \delta G(t)$. Then the standard deviation $\Delta G \equiv \sqrt{\langle \delta G(t)^2 \rangle}$, called *gain variation*, is the *dominant* factor influencing radiometer sensitivity ΔT . A clever technique conceived by Dicke [10] avoids

⁴The signal from a radiometer looking at thermal radiation is normal-distributed [67]. See also section 5.3.2.

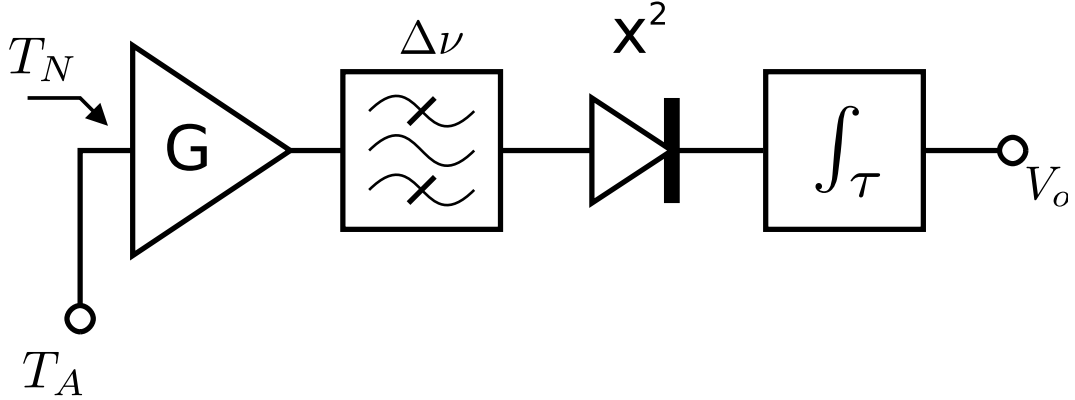


Figure 5.7: Diagram of a basic Total Power Radiometer: The input signal to the radiometer is characterized by the antenna temperature T_A , which is determined by the radiation collected in the antenna, and the intrinsic radiometer noise temperature T_N , which fully characterizes thermal noise in the radiometer. The signal is amplified with gain G , then filtered to select a narrow bandwidth $\Delta\nu$. The (microwave) signal power is detected by a square-law diode. Finally, the signal is integrated over a period τ to smooth out random fluctuations.

this difficulty by alternately measuring the signal and some other known reference at a higher frequency than the characteristic gain variation frequency of $G(t)$, called the *knee frequency* f_{knee} .

The defining parameters of an amplifier are thus its gain G , its mean fluctuation or gain variation ΔG and its *characteristic frequency* f_{knee} . The intrinsic amplifier noise contribution to total signal noise will be included in the *receiver temperature noise* T_{rec} to be defined below.

Noise and attenuation

Thermal noise due to random motion of electrons in a conductor is the basic source of random noise in a radiometer, but not the only one. Other types of noise include *quantum noise*, *shot noise* and *flicker noise* [67]. As the name suggests, quantum noise is a consequence of quantum-mechanical effects in conducting devices and manifests itself as discrete random fluctuations in the transported signal. In the Rayleigh-Jeans limit such quantum effects can be ignored. Shot noise arises from current flow fluctuations in conducting devices due to the discrete nature of charge carriers. Flicker noise is caused by surface irregularities in semiconductors. All this fluctuations contribute to the noise output power, which can be characterised by a noise temperature T_N , as explained above.

A perfect knowledge of each radiometer component would make it possible to calculate the random noise contribution of each waveguide, switch, resistor, etc. to the total radiometer noise. Instead, we use a very simple model that nevertheless is good enough for most purposes [67], where noise is characterized by a few measurable parameters.

Let an antenna with *radiation efficiency* η (see Sec. 5.2.1) be coupled through a transmission line of *loss factor* L to a receiver with characteristic *receiver temperature* T_{rec} . The antenna and transmission line are assumed to be in thermodynamical equilibrium, at

a *physical temperature* T_p . The *radiometer noise temperature* T_N is then given by [67]

$$T_N = (L - \eta) T_{p,A} + LT_{\text{rec}}. \quad (5.55)$$

The antenna radiation efficiency η and loss factor L of the transmission line can always be measured. The temperature $T_{p,A}$ is the *physical temperature* of the antenna and transmission line coupling at the time of measurement. This is different from the *antenna temperature* T_A which characterizes the *power* collected by the physical antenna aperture. The receiver temperature T_{rec} may be defined as the temperature that is measured by the receiver when disconnected from the antenna. It characterizes all noise sources internal to the receiver. It is strongly dependent on the *physical temperature* $T_{p,\text{rec}}$ of the receiver at the time of measurement. The value of T_{rec} and its dependence on $T_{p,\text{rec}}$ is specific for every receiver and must always be measured before any experiment. Here, however, we can only estimate T_{rec} based on the values given in the literature for radiometers designed to measure radiation in the range of temperatures and frequencies we are interested in. We use a simple ad-hoc model

$$T_{\text{rec}}(T_{p,\text{rec}}) = a_{\text{rec}} T_{p,\text{rec}} + c_{\text{rec}}. \quad (5.56)$$

where the receiver noise temperature T_{rec} is a linear function of its physical temperature $T_{p,\text{rec}}$. Parameters a_{rec} and c_{rec} are chosen so that $T_{\text{rec}}(T_{p,\text{rec}})$ roughly matches the same order of magnitude as given in the literature for a receiver working at temperature $T_{p,\text{rec}}$. This will be explained in more detail in section 5.4.

Total power radiometer output temperature and sensitivity

As discussed before, the total power radiometer outputs a voltage signal V_o which may be interpreted as a radiometer output temperature T_o , defined in equation (5.54). Here and in the following we assume that the radiometer has been properly calibrated so that we may always calculate T_o from V_o .

The measured *radiometer output temperature* T_o of the total power radiometer is then

$$\begin{aligned} T_o &= T_A + T_N \\ &= \eta T_A + (L - \eta) T_p + LT_{\text{rec}} = \eta T_A + (L - \eta) T_p + L(a_{\text{rec}} T_{p,\text{rec}} + c_{\text{rec}}). \end{aligned} \quad (5.57)$$

The radiometer sensitivity is determined by the average fluctuation of the output temperature. We anticipate that this average fluctuation is affected by the high gain variation of HEMT-type amplifiers. On the other hand, we expect the integrator to function as a low-pass filter and suppress fluctuation frequencies much higher than the inverse of the integration period. Both conjectures turn out to be true. Namely, it can be shown that the *sensitivity* of the total power radiometer with bandwidth $\Delta\nu$, integration period τ , gain G and gain variation ΔG is given by the expression [67]

$$\Delta T_o = T_o \sqrt{\frac{1}{\Delta\nu\tau} + \left(\frac{\Delta G}{G}\right)^2}, \quad (5.58)$$

with T_o given as in (5.57).

Note that both the integration period and gain variation appear as independent terms under the square root. This means that large uncertainties in the output temperature due to high gain variation ΔG cannot be compensated just by choosing a higher integration time. It is therefore very important to minimise gain variations as much as possible. Both expressions (5.57) and (5.58) will later be used to simulate experimental results.

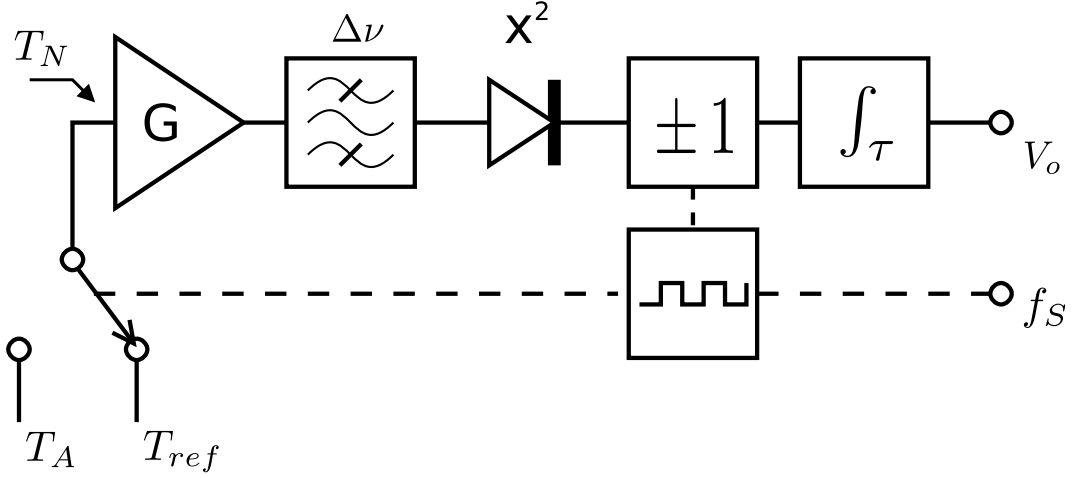


Figure 5.8: Diagram of a basic Dicke Radiometer: The receiver input is rapidly switched between the antenna signal characterized by T_A and a reference signal with temperature T_{ref} . The switching occurs at a frequency f_S chosen so that it is greater than the characteristic fluctuation frequency of the amplifier, $f_S > f_{knee}$. Then for each switching period the amplifier gain may be taken to be constant, and a *signal difference* $T_A - T_{ref}$ can consistently be defined. See text for details.

5.3.3 Dicke radiometer

A basic Dicke Radiometer configuration is shown in figure 5.8. It is based on a clever switching technique introduced in 1946 by Dicke [10] that suppresses noise power output produced due to amplifier instabilities in total power radiometers. Dicke's method effectively prevents amplifier gain fluctuations from degrading the sensitivity of the radiometer [10]. This is realized by *switching* the receiver input back and forth between the antenna signal T_A and a *reference signal* T_{ref} , at a *switching frequency* f_S greater than the characteristic amplifier frequency f_{knee} . After amplification and detection, the output of the square-law diode is multiplied before integration by $+1$ or -1 , depending on the position of the Dicke switch. The signal integrator then adds (or subtracts) the power coming out of the square-law diode into the total output signal V_o , which will be given by the difference between antenna and reference signals.. An expression for V_o can be derived as follows: Let the switching frequency f_S be large enough so that the amplifier gain $G(t) = G + \Delta G(t)$ may be regarded as constant over one switch period $1/f_S$, further let the integration period τ be much larger than $1/f_S$. Then for each switch period, the *power difference* $G(t)(P_A - P_{ref}) \equiv G(t) \Delta\nu k_B (T_A - T_{ref})$ at an arbitrary time t may be consistently defined, since within each period the amplifier gain can be assumed constant, $G(t) \approx G(t + 1/(2f_S))$.

The power difference is integrated over a period τ , and the average output voltage after integration is given directly by [63]

$$V_o = G(P_A + P_N) - G(P_{ref} + P_N) = G \Delta\nu k_B (T_A - T_{ref}) = G \Delta\nu k_B T_o. \quad (5.59)$$

The noise temperature T_N cancels in expression (5.59), and the radiometer output temperature T_o is just the difference between antenna and reference temperature. The average gain

G now multiplies a temperature *difference*. By choosing T_{ref} sufficiently close to T_N , we can thus suppress the effects of gain fluctuations in the measured signal. Ideally, $T_A = T_{\text{ref}}$ so that the output signal becomes precisely zero and the dependence on G vanishes.

Note however that in Eq. (5.59) we have assumed the noise power output of the radiometer to be just an additive contribution P_N to the total power output P_o . It was further assumed that the generated noise power is constant over both switch measurements. Nonlinear effects in the radiometer manifest themselves as a slight shift from the ideal case (5.59). This we discuss below.

Dicke radiometer output temperature and sensitivity

Here we give the output temperature and sensitivity formulas for a properly calibrated Dicke radiometer. We use (5.55) and (5.56) to model radiometer noise. A refinement of Eq. (5.59) must be made to account for nonlinear effects [33]. The *radiometer output temperature* T_o of a Dicke radiometer is then given by the expression

$$T_o = T_A - T_{\text{ref}} + T_{\text{off}}. \quad (5.60)$$

The switching noise temperature T_{off} results from non-idealities in radiometer components, even when comparing between identical signal temperatures [33]. It cannot be included within the receiver noise temperature T_N , since T_N cancels in our simple linear noise model. As given in [61], it is of the order of 10^{-1} K.

The minimum detectable temperature difference of a Dicke radiometer is given by a modification of (5.58) to take into account the diminishing influence of gain fluctuations

$$\Delta T_o = \sqrt{\frac{2}{B\tau} \left[(T_A + T_N)^2 + (T_{\text{ref}} + T_N)^2 \right] + \left(\frac{\Delta G}{G} \right)^2 (T_A - T_{\text{ref}})^2}, \quad (5.61)$$

where T_N is defined as in equation (5.55). As was expected, the effect of ΔG can be made negligible, by choosing $T_A - T_{\text{ref}}$ to be as close to zero as possible. This is the great advantage of a Dicke radiometer setup.

5.4 Radiometric detection of the SU(2) ground state

We now arrive at the main section of this chapter, where we describe possible ways to detect the presence of a thermal ground state.

5.4.1 Detection principle

There are two ways in which the problem of experimentally testing the SU(2) photon hypothesis can be approached.

1. Measure the total output power of the photon gas directly at the *radiation temperature* T_R and frequency ν . From (5.52), a very sharp decline of output power below the cutoff frequency $\nu^*(T_R)$ would corroborate the predicted *spectral gap*, and the SU(2) hypothesis.
2. Measure the output power difference between a prepared U(1) and an SU(2) photon gas cavity, both at *radiation temperature* T_R . From (5.51) and (5.52), this difference should be zero above the cutoff frequency $\nu^*(T_R)$ and non-zero below.

We saw in chapter 4 that the thermal ground state can be deformed by temperature gradients and still remain a good a priori description of the SU(2) gas in the adiabatic approximation. However, the thermal radiation formulas derived in this chapter always assume a homogeneous temperature distribution. To ensure the validity of these formulas, temperature gradients within the cavity should be carefully controlled to be as *small as possible*.

From section 4.2 we also know that it is possible to deform the SU(2) ground state with static electric fields so that the thermodynamical assumptions from which it was derived are no longer valid. The emitted radiation then becomes physically indistinguishable from that of the U(1) gas. When probing for SU(2) thermodynamics one should be very careful with the experimental conditions so as to avoid this. The cavity containing the SU(2) thermal gas should be shielded from any stray electromagnetic radiation. For the low temperature region of experimental interest, this shielding should guarantee an electromagnetic field energy density of at most $|\vec{E}| = 10^{-3}$ mV/cm.

On the other hand, the destruction of the SU(2) ground state gives us the possibility of generating U(1) behaviour to use as a reference. This will be exploited in the design of the experiment. The U(1) gas is realized by applying a sufficiently large static electric field. This is explained in the next section.

5.4.2 Experimental setup

The basic setup of our experiment is sketched in figure 5.9. Take a cryogenic chamber capable of operating in a specified temperature range $T_{min} \dots T_{max}$. This range will be determined later when the radiometer bandwidth is chosen. The dimensions of the cryogenic chamber should be large enough to accommodate two identical rectangular cavities. Let each cavity be of side length L_i , $i = 1, 2, 3$, and take each L_i to be large enough so that modifications due to cavity geometry to the Planck expression for black-body spectral energy density (5.14) may be safely ignored. These corrections are given in (5.13). The spectral region of experimental interest is $5 \text{ GHz} < \nu < 15 \text{ GHz}$ (see below). In this frequency range, taking each length to be of the order of $L_i \sim 1 \text{ m}$ ensures that discretization corrections (5.13) are at most of the order 10^{-4} [4] and may safely be ignored.

Label each cavity A and B, as shown in figure 5.9. The walls of A and B are covered with a thick enough layer of *microwave absorber* of the largest possible *emissivity* $\varepsilon \geq 0.9999$, so that radiation within each cavity is completely thermalized. As discussed in chapter 4, in order to avoid ground state decoupling effects, A and B must further be shielded from stray electromagnetic radiation. We will be working with temperatures of at least 8 K. The ground state energy density at this temperature is equivalent to the electric field density of an electric field of magnitude $|\vec{E}| = 2.216 \text{ mV/cm}$ (see Eqs. (4.15) and (4.16)). We therefore require the cavity to be shielded from stray electromagnetic radiation down to $|\vec{E}| = 10^{-3} \text{ mV/cm}$, to be certain that no decoupling effects occur at all.

Cavity B is further equipped with two capacitor plates positioned at opposite sides within the cavity, connected to an adjustable voltage source V_c , so that a constant electric field of energy density ρ_c can be generated inside B.

A Dicke Radiometer is also brought inside the cryogenic chamber. The radiometer parameters are discussed in the next sections. Dicke switching occurs between the terminals of two identical *horn antennas*, labelled A and B. Each antenna is placed inside their corresponding cavity, as shown in the figure.

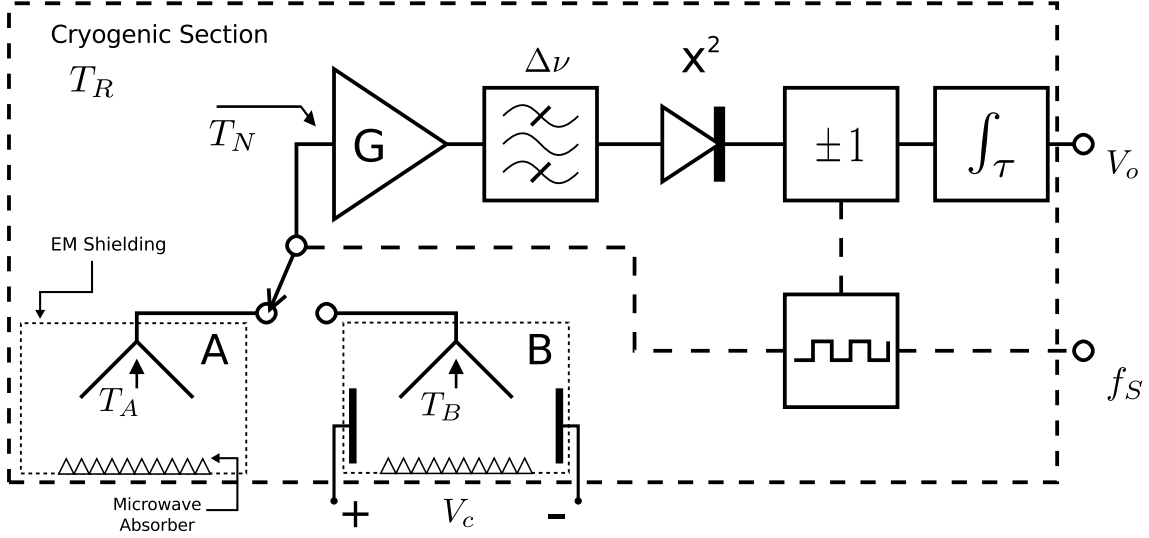


Figure 5.9: Basic Radiometer Setup for the detection of thermal SU(2) effects. Inside a cryogenic chamber at temperature T_R we place two identical cavities A and B, of side dimensions $L \sim 1\text{m}$. The interior cavity walls of both cavities are fully coated with a thick enough layer of microwave absorber with $\varepsilon \geq 0.99$ emissivity. (This is shown in the diagram only for one wall). Cavity B is further equipped with capacitor plates opposite to each other. They connect to a voltage source V_c to generate a static electric field of adjustable energy density inside the cavity. Each cavity is also shielded from stray electromagnetic fields. Identical horn antennas are placed inside each cavity, both of which connect to the radiometer through a Dicke switch. The radiometer is also placed inside the cryogenic chamber, so that the whole system: cavities, antennas, couplers and radiometer is at the same thermodynamic temperature T_R .

In order to specify the necessary experimental parameters, we must first choose the spectral region and working temperature the radiometer is going to probe. This is done in the next section.

5.4.3 Working frequency and temperatures

Here we determine the optimal frequency bandwidth for the receiver, and the corresponding radiation temperature range.

In order to test for screening effects, we need to measure the propagation of thermal radiation inside and outside the photon screening region (see section 3.5.4). This region is determined by a frequency $\nu^* = \nu^*(T)$, above and below of which photon propagation is allowed and forbidden, respectively.

We first define the *middle frequency* ν_m and *bandwidth* $\Delta\nu$ which will be investigated in this experiment. Following [61], we choose the 10 GHz Low channel which is used there with $\nu_m = 9.72\text{ GHz}$ and $\Delta\nu = 860\text{ MHz}$. Now use the results of section 3.5.4 to plot ν^* as a function of T and select an adequate temperature region.

Since we would like to avoid boundary effects such as having the frequency ν^* lie within the bandwidth region of the above 10 GHz channel, we avoid temperatures for which the

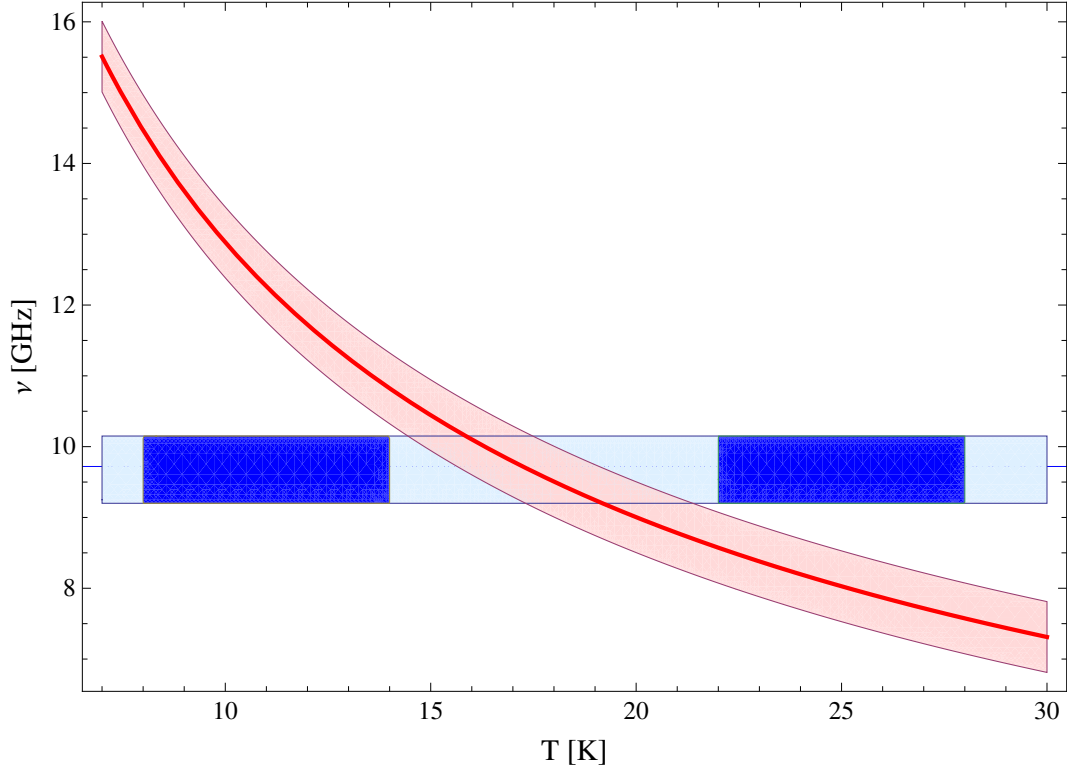


Figure 5.10: The red line plots the cutoff frequency ν^* , calculated as in section 3.5.4. The region 500 MHz above and below ν^* is plotted in light red. The 860 MHz bandwidth available to the radiometer is shown as light blue, centred around the frequency $\nu_m = 9.72$ GHz. The region lying within available bandwidth and working temperature is shown in blue. The temperature regions were so chosen that the measured bandwidth lie at least 500 MHz above or below the temperature-dependent cutoff frequency ν^*

bandwidth boundary would lie within 500 MHz from the cutoff. The temperature ranges $8 \text{ K} \leq T_R \leq 14 \text{ K}$ and $22 \text{ K} \leq T_R \leq 28 \text{ K}$ match this condition. In figure 5.10 we have plotted the cutoff frequency ν^* and the region 500 MHz above and below it. The working bandwidth of 860 MHz around the middle frequency $\nu_m = 9.72$ GHz is visible, along with the chosen temperature ranges. We therefore need a cryogenic chamber capable of working between temperatures $T_{min} = 8 \text{ K}$ and $T_{max} = 28 \text{ K}$.

Note also that with our choice of frequencies and temperatures, we still lie within the Rayleigh-Jeans region, since for the lowest temperature, $(h\nu_m)/(k_B T_{min}) = 0.0583 \ll 1$.

The rest of the experimental parameters are taken to be of the order of magnitude as those in the radiometer configuration used in [61]. This is discussed in the next section.

5.4.4 Radiometer parameters

In this section, we will simulate the results of radiometer measurements predicted from the $SU(2)_{\text{CMB}}$ hypothesis described in section 3.4. The most important radiometric consequence of this hypothesis is the existence of a frequency cutoff ν^* below which photon propagation is impossible. Using the formulas for radiometer temperature and standard

Radiometer Parameters		I	II	IIIa	IIIb
Antenna efficiency	η	0.99	0.99	0.99	0.99
Middle frequency	ν_m	9.72 GHz	9.72 GHz	9.72 GHz	9.72 GHz
Bandwidth	$\Delta\nu$	0.86 GHz	0.86 GHz	0.86 GHz	0.86 GHz
Radiometer noise	T_{rec}	$0.1T+10\text{K}$	$0.2T + 15\text{K}$	$T + 15\text{K}$	$T + 15\text{K}$
Radiometer offset	T_{off}	200 mK	500mK	1K	1K
Gain variation	$(\Delta G/G)$	-30 dB= 10^{-3}	-20 dB= 10^{-2}	-10 dB= 10^{-1}	-20 dB= 10^{-2}
Loss factor	L	0.5 dB = $10^{0.05}$	1 dB= $10^{0.1}$	5 dB= $10^{0.5}$	5 dB= $10^{0.5}$
Integration time	τ	0.1s	1s	10s	10s
Switching frequency	f_S	75 Hz	75 Hz	75 Hz	75 Hz

Table 5.1: Radiometer parameters, see text. Note that $N_{dB} \equiv 10 \log(N)$.

deviation, (5.57), (5.60), (5.58), and (5.61), we can generate expected measurement plots, so as to have an intuitive idea of the order of magnitude of both the expected signal average and stochastic variation. But before using the radiometer formulas given above, we must specify certain *characteristic parameters* of the radiometer.

The parameters used to generate simulation plots are given in table 5.1. These are taken to be of the same order of magnitude as those described in the literature [2, 33, 34, 56, 61, 62, 64, 69] for radiometers used in experimental situations closely matching our own. That is, low temperatures and frequencies in the microwave region. We have divided them in three sets. Set I is the parameter set which corresponds to an ideal radiometer with above-average sensitive. The parameter set II corresponds to a radiometer with average performance. Set III results in a very noisy radiometer. This parameter set is further divided in IIIa and IIIb, the only difference being the gain variation. The choice of parameters is explained in detail below.

Corrugated horn antennas are a popular choice for microwave applications because of high beam symmetry, low side-lobes, low crosspolarization and low reflection over a wide broadband. Horn antennas may be designed to satisfy requirements such as working frequency, antenna gain and directivity [45]. This in turn specifies the expected antenna radiation efficiency, which we take to be 0.99. This sole parameter characterises the antenna response in our simplified example. Of course, a full characterisation including radiation beam pattern is needed to precisely describe an actual experiment, see for example [62]. Antenna efficiency is taken to be the same in all cases.

Middle frequency and bandwidth of the radiometer were chosen following [61]. Radiometric equipment in this frequency region is commercially readily available, further, the temperature region it imposes is such that radiometer and amplifier noise remains low enough for our purposes. Higher frequencies show too narrow temperature ranges to test for screening effects, compare with figure 5.10, and we would like to measure screening effects over a relatively wide range of temperatures. On the other hand, a lower frequency would imply increasingly large temperatures ranges to test for non-screening (note the

decreasing slope of $\nu^*(T)$ in figure 5.10). Noise and random measurement error increase with temperature, so we would like to avoid relatively large temperatures. We find that $\nu_m = 9.72$ GHz is a nice compromise. The temperature ranges for testing above and below ν^* are then given by $8 \text{ K} \leq T_R \leq 14 \text{ K}$ and $22 \text{ K} \leq T_R \leq 28 \text{ K}$.

Receiver noise is determined by the thermodynamical temperature of the physical radiometer system. The HEMT amplifier noise is also dependent on the working frequency band [69]. Since we plan to access the $SU(2)$ ground state by probing different temperatures T_i , receiver noise will in general change for each temperature. In the actual experiment this will become a source of systematic error, since for each run T_{rec} will vary, however slightly, as a function of the working temperature. This variation should be calibrated for each T_i , so that for every measurement run we may extract the *output power temperature* T_o , whatever the radiometer working temperature. Further, the receiver noise temperature T_{rec} crucially limits the experimental precision of the radiometer. Here, we assume the simple linear model given in (5.56)

$$T_{\text{rec}}(T_{p,\text{rec}}) = a_{\text{rec}} T_{p,\text{rec}} + c_{\text{rec}}, \quad (5.62)$$

where $T_{p,\text{rec}}$ is the physical receiver temperature. The coefficients a_{rec} and c_{rec} are chosen such that in the temperature range we work with, $T_{\text{min}} = 8 \text{ K}$ and $T_{\text{max}} = 28 \text{ K}$, they are of the same order of magnitude as the receiver noise found in the literature, e.g. [2, 34, 56, 61, 64, 69], which we have estimated into best, average and worst performance (sets I, II and III).

Radiometer offset is the baseline noise in Dicke switching measurements [33]. We have taken it to be of the order of 10^{-1} K [61].

The *power gain variation* $\Delta G/G$ is the most important determinant of radiometer precision, as can be seen from the equations (5.58) and (5.61). (And as we will later confirm in the simulations). Commercially available HEMT amplifiers come with gain variation of the order of 10^{-3} [5]. We take this value for the best case scenario I. We assume a poorer mean fluctuation of the order of 10^{-2} for the average case II and "better" worst case IIIb. For the worst case scenario IIIa we take fluctuations of the order 10^{-1} .

Loss factor gives the signal power loss between antenna and receiver. Here we have taken to be of the order of $1 \text{ dB} = 10^{0.1}$ for the average scenario, based on the [61] setup. The values for the I and III cases were taken to be some orders of magnitude above and below 1 dB .

The *integration time* can be calculated so as to minimise radiometer uncertainty [70]. Here we take it to be $\tau = 1 \text{ s}$ in the average case and vary the value accordingly for best and worst case. Finally, the *switching frequency* f_S when working in Dicke mode should be chosen such as to be greater than the characteristic fluctuation frequency of the amplifier, $f_S > f_{\text{knee}}$. Otherwise the Dicke switching formulas (5.60) and (5.61) do not apply. Here we use the value given in [61], $f_S = 75 \text{ Hz}$.

5.4.5 Experimental signature

Having defined the most important experimental parameters in table 5.1, we may now use those values to estimate the radiometer output in the experiment. As already described, two experimental procedures are possible, total power mode and Dicke switching mode.

We simulate an experimental run of 600 measurements. The integration time of the radiometer is given in table 5.1 for each set of parameters, so each measurement run has

a duration of 1 minute, 10 minutes and 100 minutes for each case I, II and III. Output temperatures for each single measurement were simulated by using a Gauss-distributed random generator with mean T_o and standard deviation ΔT_o , both of which were calculated using the appropriate formulae (5.57), (5.58) for a total power run and (5.60), (5.61) for a Dicke switch run. The radiometer noise temperature T_N given in (5.55) was used in both cases to calculate the noise contribution to the output signal.

The temperature of the cryogenic chamber *defines* the radiation temperature T_R , since the black-body cavities then have thermodynamical temperature T_R . The physical temperature of the receiver and of the antenna and transmission-line coupling, were also taken to be T_R , since the radiometer is placed inside the cryogenic chamber. That is, T_p and $T_{p,\text{rec}}$ are taken equal to the radiation temperature $T_p = T_{p,\text{rec}} = T_R$.

Recall that the antenna temperature T_A is by definition the temperature of the collected radiation. Inside the black-body cavity, radiation is at thermal equilibrium with the cavity walls and $T_A = T_R$. This means that the antenna efficiency η *cancels* in the expression (5.57), since in our case, $T_A = T_p$.

The results of the simulations are discussed below.

Total power mode

In total power mode, we set the cryogenic chamber to a temperature T_R then let the radiometer observe the output A. For each T_R we run 600 measurements. The results are plotted below. We first describe the experimental procedure, then comment on each case.

Start the first measurement run at $T_R = 28\text{K}$, then decrease the temperature to $T_R = 26\text{K}$ and measure again, and so on until $T_R = 22\text{K}$. If the radiometer parameters are such that the relative signal error is small enough for a distinct linear relationship between T_o and T_R to be identified, we may fit the four pairs (T_R, T_o) to a line

$$T_o = A_{ac}T_R + C_{ac}. \quad (5.63)$$

The subscript *ac* stands for "above cutoff". We call this measurement series the *above-cutoff* series.

Decrease now the temperature further, to $T_R = 14\text{K}$, and start the measurement series again going down to $T_R = 8\text{K}$. As above, if the measurement errors are small enough, we can fit the four measured data points to a line

$$T_o = A_{bc}T_R + C_{bc}, \quad (5.64)$$

where *bc* stands for "below cutoff". Similarly, we call this measurement series the *below-cutoff* series.

As an example, take the average radiometer (II) first. It has integration period $\tau = 1\text{ s}$, so each measurement run takes 10 minutes. The results are plotted in figure 5.11a for all temperatures T_R . The red lines represent simulated experimental runs assuming the SU(2) hypothesis, the grey lines would be the result of U(1) dynamics.

The standard error ΔT_o is also visible in figure 5.11a as the width of the measurement. For parameter set II, it is of the order of 10^{-2} , the dominant contribution coming from the average gain fluctuation. This is small enough to fit Eqs. (5.63), (5.64).

Now consider the *above-cutoff* series. In this temperature range, the cutoff temperature lies below the radiometer frequency bandwidth, compare with figure 5.10. We should

therefore measure a radiometer output temperature T_o consistent with a finite T_R temperature and equation (5.57), independently of whether the photon obeys SU(2) or pure U(1) dynamics. Figure 5.11a shows how both predictions overlap in this temperature region.

Take now the *below-cutoff* series. Assume SU(2) dynamics. Then, in this temperature range, the radiometer is now directly looking at the *screening* region, compare with figure 5.10. There can be no propagation inside the cavity within the frequency bandwidth of the radiometer. The effective radiation temperature T_R the radiometer sees is therefore zero. The expected output temperature inside this region is then given by (5.57) with T_R set to zero, $T_R = 0\text{K}$. From this same formula, we see that the only output measured is radiometer noise. This is now the key experimental fact. If we compare the fitted parameters in (5.64), (5.63), for the SU(2) case, they should *differ*. The parameters *above-cutoff* characterize a finite antenna signal plus noise, while those *below-cutoff* pick up only the noise signal. For small standard variation in T_o both sets of parameters should differ beyond curve fitting errors.

In the case of U(1) dynamics, on the contrary, both linear fits should be similar enough so as to have each fitted parameter lie within each others error bars.

All of this is visible in figure 5.11a. The red lines show a slope in the non-screening region of about $A_{ac} = 1.6$, compared to the slope in the screening domain of $A_{bc} = 0.3$. The gray lines, on the other hand, both show the same slope $A_{bc} = A_{ac} = 1.6$ above and below the screening region.

This is therefore the *experimental signature* of SU(2) Yang-Mills thermal ground state when probed by a total power radiometer.

We now discuss the other sets of radiometer parameters. The results of the *worst case* radiometer IIIa measuring in total power mode are given in figure 5.12a. We see that in this case, the signal error is so great that no definitive linear relationship may be attributed between measured radiometer temperature T_o and the cavity radiation temperature T_R . It is still of note that an *absolute difference* is visible in the screening region between the U(1) case (grey) and SU(2) case (red), they do not overlap. But this depends on the calculation of predicted U(1) signals, which in turns depends on the full characterization of the radiometer noise temperature function. This would induce enough error dependencies that such a signal would lose any experimental significance.

Amusingly, this worst case radiometer may be immediately made useful by just replacing the 10^{-1} gain variation amplifier with a quieter one of gain variation 10^{-2} . Since gain fluctuations ΔG are the dominant error source in the receiver, this change is enough to make the IIIa radiometer a good enough IIIb. This is seen in figure 5.13a. The high receiver noise still influences the absolute value of the output temperature (compare the $T_o \sim 225\text{K}$ at $T_R = 28\text{K}$ with $T_o \sim 61\text{K}$ at the same radiation temperature for the II radiometer), but the different slopes are clearly visible: $A_{ac} \approx 4.75$ outside the screening region and $A_{bc} \approx 2.35$ inside it. This shows that the most important radiometer parameter in our case is the average gain fluctuation ΔG .

Figure 5.14a shows the results from simulating a *best case* radiometer measurement in total power mode. The SU(2) signal is clearly visible, with $A_{ac} \approx 0.93$ *above-cutoff* and $A_{bc} \approx 0.08$ below it. It is remarkable that such a strong signal may be recovered from a very simple radiometric technique. This of course assumes the availability of a *best case* radiometer as listed in table 5.1.

Dicke switching mode

We now discuss the radiometer working in Dicke switching mode. As explained before, in this mode the radiometer switches with frequency f_S between measuring the antenna temperature T_A and a reference temperature T_{ref} . In this experiment we will use a $U(1)$ cavity as reference. Such a cavity is prepared as described in section 4.2.

A voltage is applied to the condensator plates inside the shielded cavity B, so that the ground state is destroyed, and the thermal radiation behaves identically as in a $U(1)$ gas. The field should be of the order of $|\vec{E}| \sim 1 \text{ V/cm}$ or greater, compare equations (4.15) and (4.16). This ensures a $U(1)$ radiating cavity.

The antenna B may now be used as a reference emitter for the Dicke switching experiment. Each experimental run of 600 individual measurements is done, as before, for temperatures between 8K and 14K (the *below-cutoff* series) and temperatures between 22K and 28K (the *above-cutoff* series).

Since both cavities find themselves inside the cryogenic chamber, both radiate at the same temperature T_R , outside the screening region.

That is, for the *above-cutoff* series, we expect from formula (5.60) that the output temperature of the radiometer be just T_{off} , which is of the order of 0.5 K. This should be the case whether the $SU(2)_{\text{CMB}}$ hypothesis is true or not, since above the cutoff frequency both $U(1)$ and $SU(2)$ cavities have the same power output. Since both signal and reference temperature are the same, we further expect the influence of gain fluctuation errors ΔG on radiometer sensitivity to vanish in this temperature region.

It is inside the screening region, that is for the *below-cutoff* measurement series, where we expect large differences between the $U(1)$ and $SU(2)$ behaviour. In this temperature range the cavity B still emits $U(1)$ radiation at a temperature $T_{\text{ref}} = T_R$. If the $SU(2)_{\text{CMB}}$ hypothesis is correct, however, no photon propagation can occur in cavity A. The effective antenna temperature *vanishes*, $T_A = 0$, and formula (5.60) now results in $T_o = T_{\text{off}} - T_R$ (in our plots we have redefined T_o to be positive, for convenience). The influence of gain fluctuation errors ΔG cannot vanish anymore, on the contrary, it should return to be the dominant fluctuation source. If the $SU(2)_{\text{CMB}}$ hypothesis is false, no change from the *above-cutoff* series should be noticeable, since both cavities would still have non vanishing output power.

As an example, take radiometer II with average parameters. The output of a Dicke switching measurement run is given in figure 5.11b. Outside the screening region, the generated values for T_o hover above the radiometer offset noise of $T_{\text{off}} = 0.5\text{K}$, as expected. Inside the screening region, however, there is a big jump in the signal in the case of $SU(2)$ dynamics. This is the *experimental signature* for the Dicke switching experiment. If photon dynamics are indeed described by an effective thermal theory with nontrivial ground state, then the signature event would be a nontrivial signal, of the order of 10K *below-cutoff*.

For the average radiometer II such a signal is easily detectable. Figure 5.12b shows the generated temperature output for the radiometer with parameter set III. And here is where the Dicke switching technique really shines. As long as the switching frequency has been chosen correctly (that is, smaller than the characteristic gain fluctuation frequency of the amplifier) the $SU(2)$ signal is also clearly visible! The measured signal shows a large error inside the screening region but that is not a problem, since we can automatically detect the presence of $SU(2)$ dynamics just by having a non trivial signal at all! Compare the difference in orders of magnitude from $T_o \sim 40\text{K}$ below the cutoff, to 1K above it.

Such a huge disparity in the Dicke signal output would immediately signal the presence of the SU(2) ground state. Since this signal is visible even for the worst of parameters, it is the ideal configuration for a radiometric experiment probing for the existence in nature of SU(2) physics. On the other hand, if the radiometer output below 14K stayed close to zero, the SU(2)_{CMB} hypothesis would be automatically falsified.

For comparison, diagrams 5.13b and 5.14b show the simulated outputs for a radiometer with parameters from the set IIIb and I respectively.

5.5 Bolometry of SU(2) photons

Aside from the radiometric experiment described in section 5.4, a type of bolometric experiment can be conceived. Unlike radiometric experiments where a narrow measurement frequency band is used, bolometric experiments are by design generally *broadband* experiments, probing a wide region in the frequency spectrum.

Here we review a type of bolometric experiment first discussed in [13] that detects the presence of SU(2) ground state dynamics by *thermal cooling*. The down side of this experimental setup is the need for special filters, which should ideally absorb all radiation above (or below) the cutoff frequency ν^* . The experimental setup is as follows.

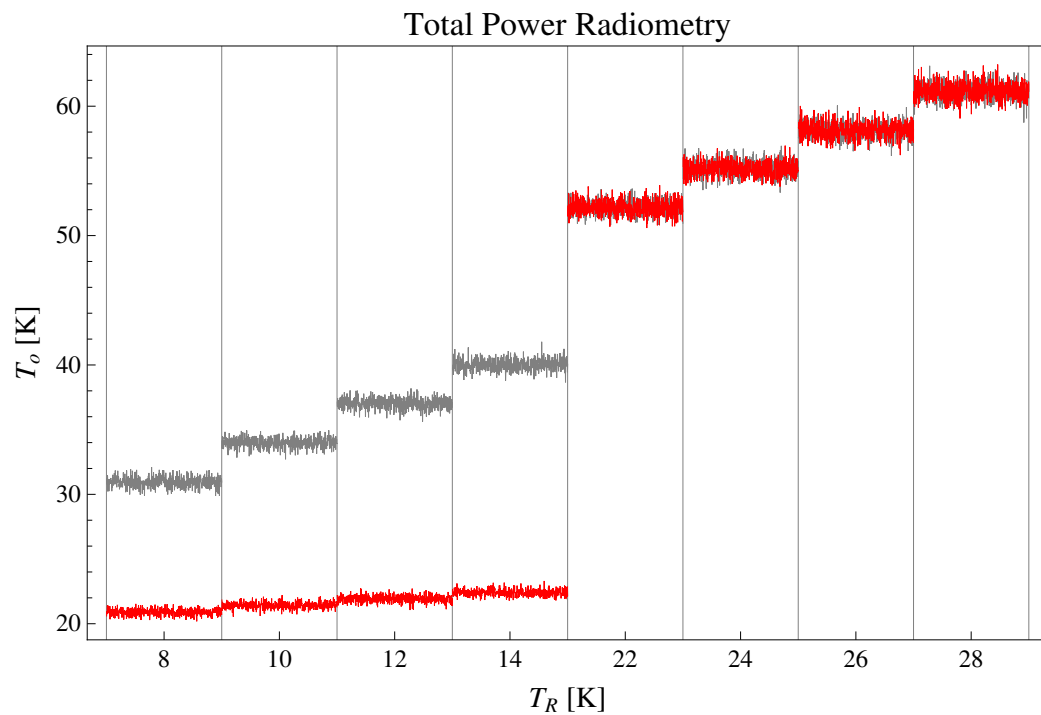
Let the apertures of an isolated low-temperature U(1) black-body at temperature T_1 and that of an SU(2) black-body of identical characteristics at temperature T_2 face each other, and exchange radiant energy. The U(1) black-body is prepared as before, by means of a static electric field. At low temperatures, of the order of 5K-10K, the magnitude of the electric field should be of the order of $|\vec{E}| \sim 1$ V/cm to guarantee a decoupling from the SU(2) ground state (compare with section 4.2). Couple the SU(2) black-body to a large heat reservoir, so as to keep its thermodynamical wall temperature T_2 constant, and insert a *low-pass filter* within the common aperture so that photons above the cutoff frequency of the SU(2) cavity $\nu^*(T_2)$ are completely absorbed. The filter works bi-directionally, that is, no matter from which direction the photons come from, they are absorbed if they propagate above $\nu^*(T_2)$.

Our bolometric experiment is then so configured that, if the SU(2)_{CMB} hypothesis is correct, power is transmitted *unidirectionally* from the U(1) cavity to the SU(2) cavity. Because of the spectral gap below ν^* , the SU(2) cavity cannot radiate in this region of the spectrum. Energy is transferred continuously from the U(1) cavity to the SU(2) cavity only, and thermal equilibrium can never be reached. This effect can then be detected as the *lowering* of the U(1) cavity temperature T_1 .

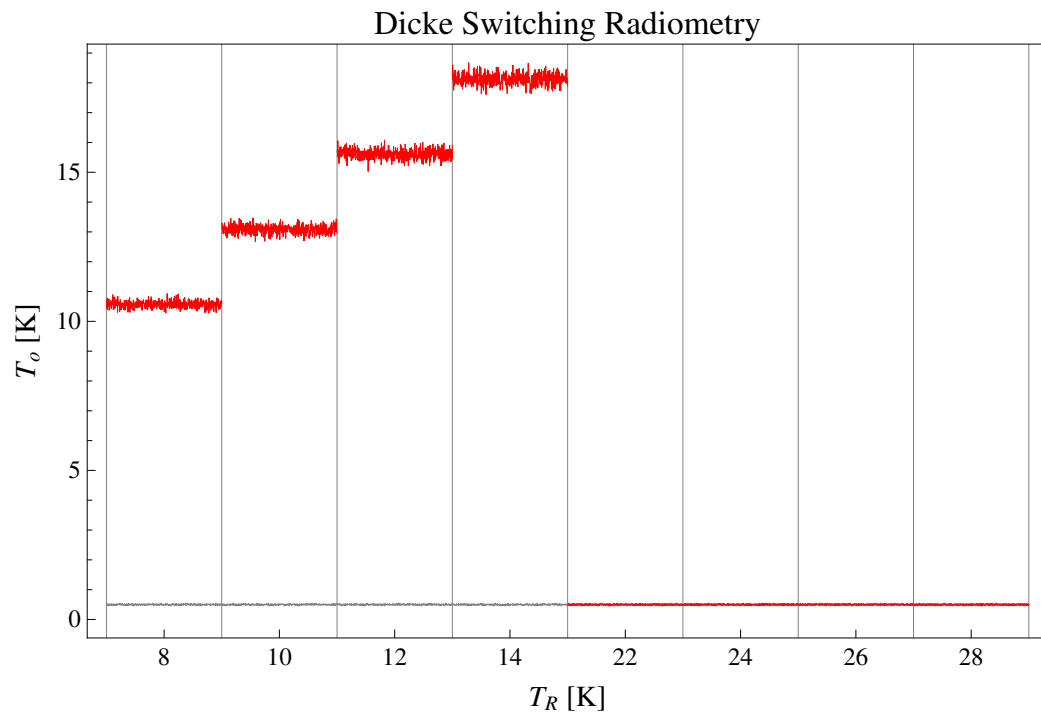
Consider now the case $T_1 = T_2 \equiv T$. Replace the low-pass filter from before with a *high-pass filter* which absorbs all radiation below the cutoff frequency $\nu^*(T)$. Let a monochromatic radiant beam of frequency $\nu > \nu^*(T)$ propagate from the SU(2) cavity into the U(1) region through the aperture, along an axis \hat{n} with solid angle $d\Omega_{U(1)}$ defined on a sphere centered at a point within the common aperture (recall Fig. 5.1). Similarly, have another radiant beam of same frequency ν propagate from the U(1) cavity into the SU(2) region, along an axis $-\hat{n}$ with solid angle $d\Omega_{SU(2)}$.

First note that by Snell's law [39], we can relate both solid angles as

$$\frac{d\Omega_{SU(2)}}{d\Omega_{U(1)}} = \frac{v_{ph}^2}{c^2}, \quad (5.65)$$

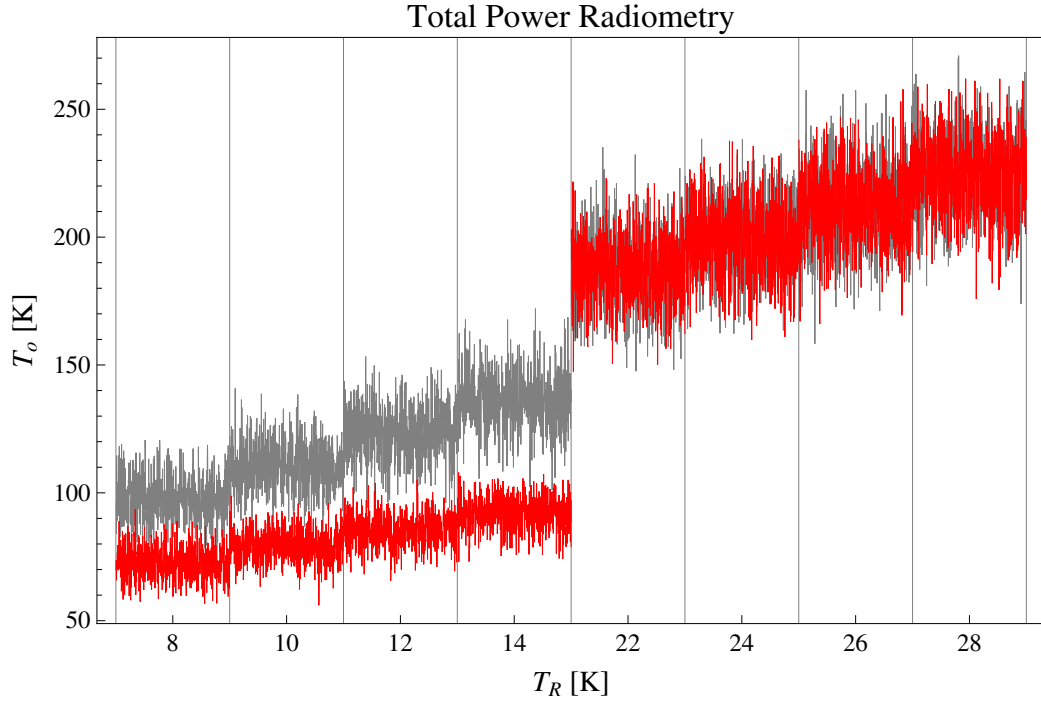


(a) Output temperature T_o measured by a total power radiometer. The graphic was generated by using a Gauss-distributed random generator of mean T_o and standard deviation ΔT_o , which were calculated using the corresponding formulas (5.57) and (5.58)

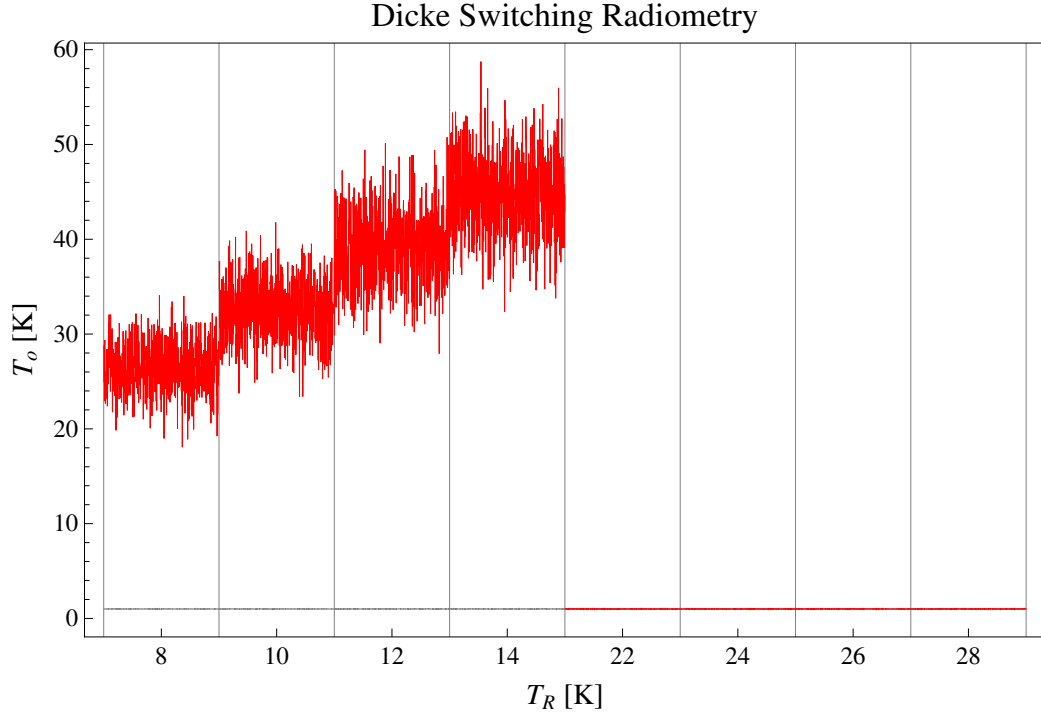


(b) Output temperature T_o measured by a Dicke switching radiometer. The graphic was generated by using a Gauss-distributed random generator of mean T_o and standard deviation ΔT_o , which were calculated using the corresponding formulas (5.60) and (5.61)

Figure 5.11: Simulated results for the set of radiometer parameters II given in table 5.1

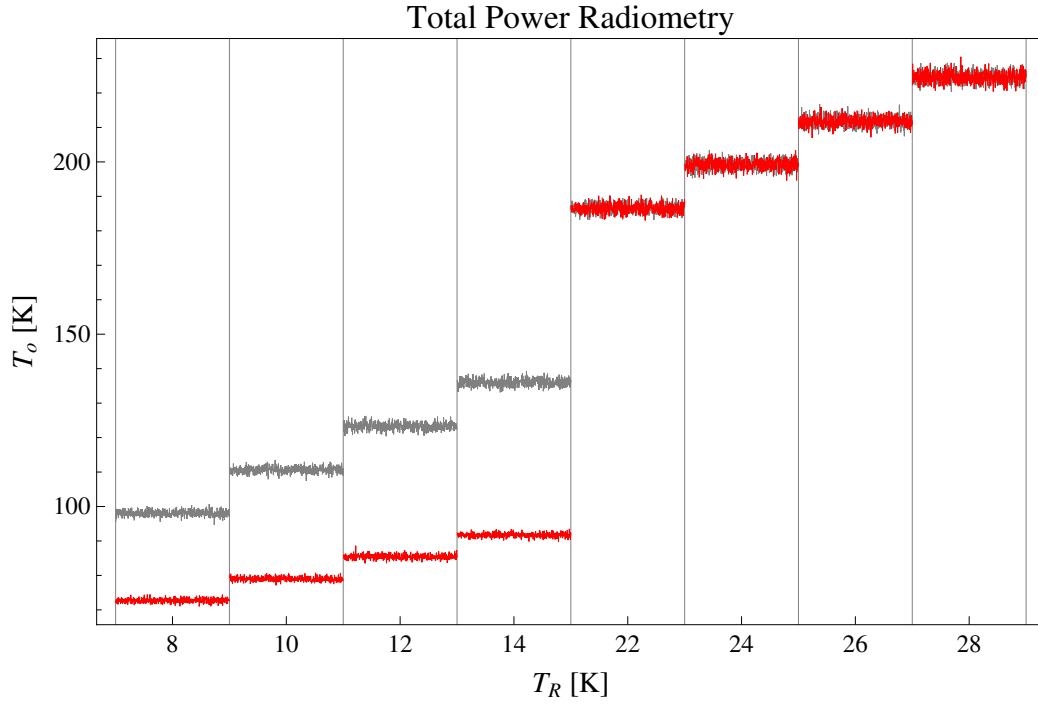


(a) Output temperature T_o measured by a total power radiometer. The graphic was generated by using a Gauss-distributed random generator of mean T_o and standard deviation ΔT_o , which were calculated using the corresponding formulas (5.57) and (5.58)

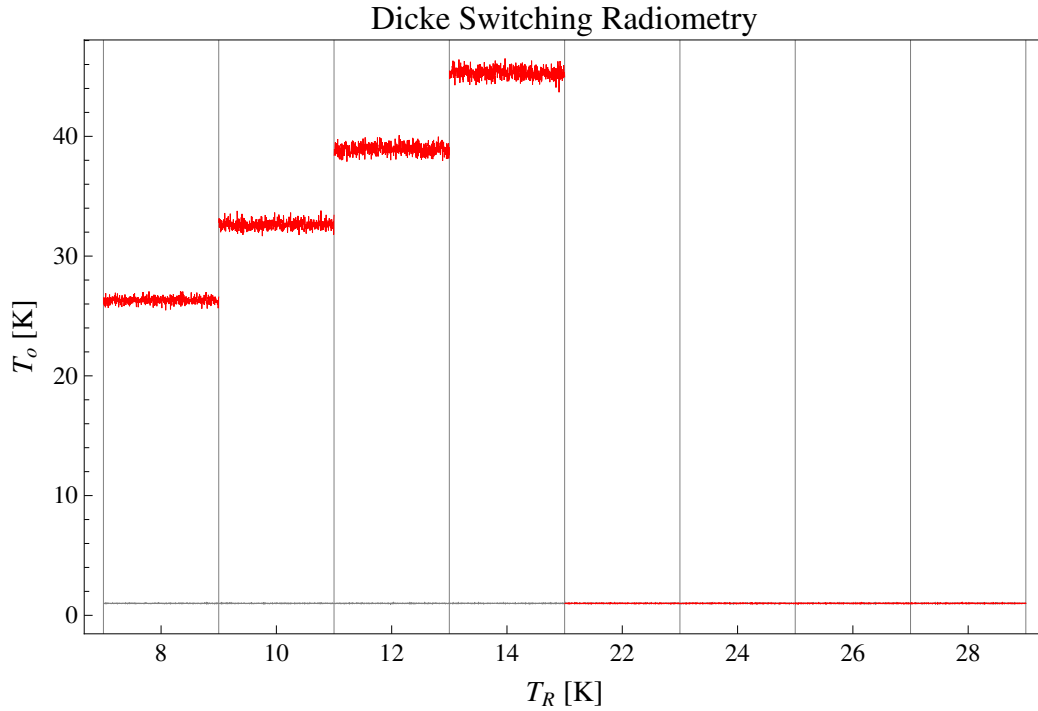


(b) Output temperature T_o measured by a Dicke switching radiometer. The graphic was generated by using a Gauss-distributed random generator of mean T_o and standard deviation ΔT_o , which were calculated using the corresponding formulas (5.60) and (5.61)

Figure 5.12: Simulated results for the set of radiometer parameters IIIa given in table 5.1

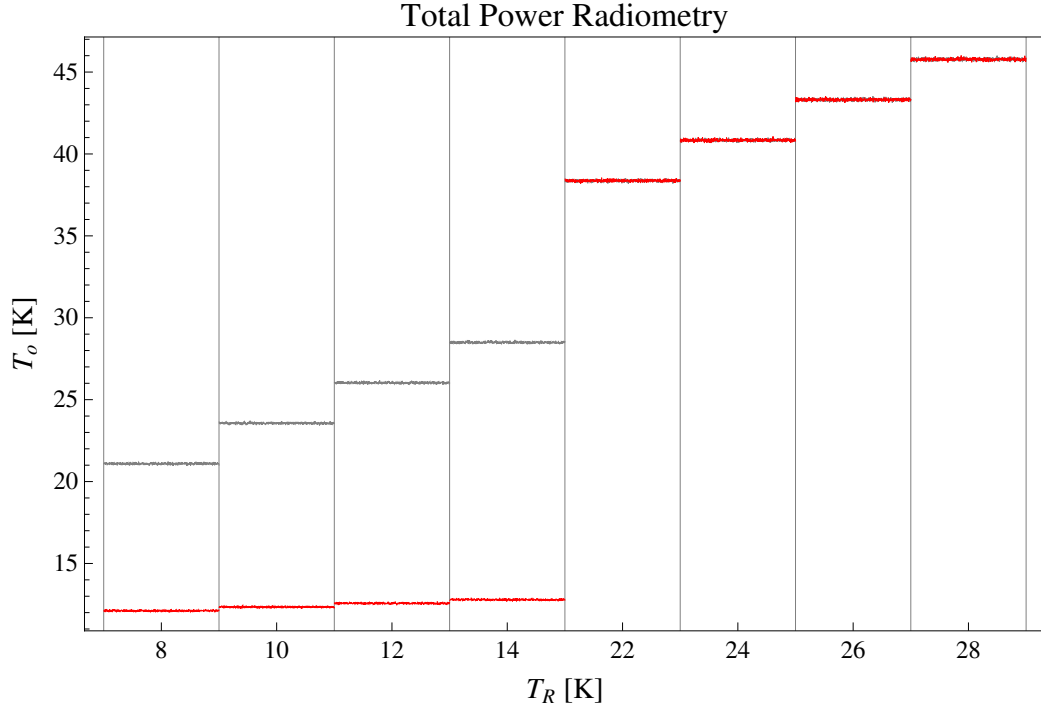


(a) Output temperature T_o measured by a total power radiometer. The graphic was generated by using a Gauss-distributed random generator of mean T_o and standard deviation ΔT_o , which were calculated using the corresponding formulas (5.57) and (5.58)

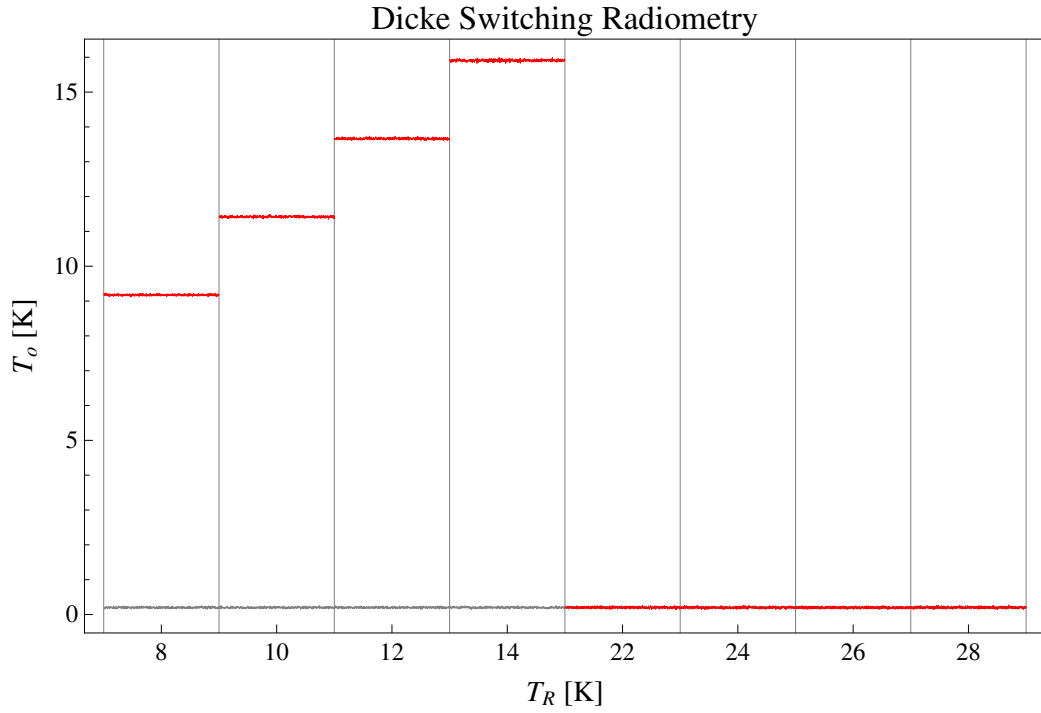


(b) Output temperature T_o measured by a Dicke switching radiometer. The graphic was generated by using a Gauss-distributed random generator of mean T_o and standard deviation ΔT_o , which were calculated using the corresponding formulas (5.60) and (5.61)

Figure 5.13: Simulated results for the set of radiometer parameters IIIb given in table 5.1



(a) Output temperature T_o measured by a total power radiometer. The graphic was generated by using a Gauss-distributed random generator of mean T_o and standard deviation ΔT_o , which were calculated using the corresponding formulas (5.57) and (5.58)



(b) Output temperature T_o measured by a Dicke switching radiometer. The graphic was generated by using a Gauss-distributed random generator of mean T_o and standard deviation ΔT_o , which were calculated using the corresponding formulas (5.60) and (5.61)

Figure 5.14: Simulated results for the set of radiometer parameters I given in table 5.1

where the phase velocity v_{ph} of energy propagation inside the SU(2) black-body is given by $v_{ph} \equiv \frac{\omega}{k} = c \left(\sqrt{1 - \frac{c^2 G}{(h\nu)^2}} \right)^{-1}$. But this results in the identity

$$L_{\nu \, bb}^{SU(2)}(\nu, T) d\Omega_{SU(2)} = L_{\nu \, bb}^{U(1)}(\nu, T) d\Omega_{U(1)} . \quad (5.66)$$

From Eqs. (5.5) and (5.6) we recognize the left and right hand side of expression (5.66) as the total power emitted respectively by the SU(2) and U(1) cavities. That is, for temperature T and frequency $\nu > \nu^*(T)$, the total power transfer from the U(1) cavity into the SU(2) cavity is equal to the total power transfer from the SU(2) cavity into the U(1) cavity. Above the cutoff frequency $\nu^*(T)$, the system is in equilibrium, and no temperature change takes place.

Chapter 6

Summary and Outlook

The main subject of this thesis was the investigation of possible experimental methods to detect the presence of a nontrivial effective thermal ground state, under the hypothesis that the abelian $U(1)$ gauge group responsible for photon dynamics in the Standard Model is not fundamental, but emerges from a pure $SU(2)$ Yang-Mills theory as the unbroken gauge symmetry at finite temperature in the effective theory of the deconfining phase after coarse-graining. In this thesis, we refer to this identification as the $SU(2)_{\text{CMB}}$ hypothesis, following the literature. The CMB in the subscript refers to the fact that the single parameter of the nonperturbative approach to $SU(2)$ thermodynamics can be fixed by the observation that the temperature of the CMB radiation gas filling the universe should be very close to the critical temperature for the deconfining/preconfining transition of the thermal $SU(2)$ gas in its deconfining phase.

Under the $SU(2)_{\text{CMB}}$ hypothesis, thermalized photons are understood as free propagating thermal quasiparticles whose dispersion law in the effective theory is determined by interactions with massive vector modes.

In this thesis, we have calculated these dispersion laws and discussed the results, in the context of possible experimental detection. It was found that the *transverse polarization modes* propagate via a modified dispersion relation. The modified dispersion relation reflects the fact that a temperature- and momentum-dependent dynamical photon mass $\sqrt{G(\mathbf{p}, T)}$ emerges in the effective theory. Further, this dispersion law shows a temperature dependent minimal propagation frequency, which we call the *cutoff frequency* $\nu^*(T)$. It is shown that below this frequency, no propagation of transverse polarized photons is possible. This defines a spectral *screening region* for frequencies below $\nu^*(T)$. We have calculated numerically a functional relationship for $\nu^*(T)$ by fitting to a power law. A novel result of this thesis is the calculation of the dispersion law for the *longitudinal mode*. The dispersion relation shows that longitudinal mode propagation is possible only for very short momentum (or long wavelength) and therefore cannot be probed by neither radiometric nor bolometric means.

The prediction of a temperature-dependent screening region has important experimental consequences, which were investigated in this thesis. It was shown that an antenna immersed in an $SU(2)$ photon gas of temperature T collecting radiation within a bandwidth $\Delta\nu \equiv \nu_2 - \nu_1 > 0$ about a middle frequency $\nu_m \equiv \nu_1 + \frac{\Delta\nu}{2}$ would measure a power output P_o identical to that of the $U(1)$ gas, as long as the entire bandwidth $\Delta\nu$ lies above the cutoff, $\nu_1 > \nu^*(T)$. By decreasing the temperature to $T' < T$, however, an experimental situation can be achieved in which the entire bandwidth $\Delta\nu$ lies *below* the cutoff,

$\nu_2 < \nu^*(T')$. In this case, photon propagation is forbidden and the antenna would deliver zero power output. This fundamental difference between U(1) and SU(2) behaviour becomes the *experimental signature* for the existence of SU(2) photon dynamics. Namely, since this region can be probed by radiometrical or bolometrical methods, the $SU(2)_{\text{CMB}}$ hypothesis becomes experimentally testable, and thus falsifiable. This is the main result of our thesis.

Two experimental techniques proposed in this thesis for probing the power output of a thermal photon gas at low temperatures and frequencies are total power and Dicke switching radiometry. It is shown that both can be made sensitive enough to detect SU(2) ground-state effects on photon propagation. Dicke switching, however, is preferable because by design it suppresses gain variations of the amplifier.

A bolometric technique is also discussed in which the observable effect is cooling by power emission. This technique depends on the availability of a low-pass filter which should bidirectionally absorb radiation above the cutoff frequency $\nu^*(T)$.

Beside our main experimental result, we offer a novel theoretical investigation on the possibility of studying thermally inhomogeneous ground-state dynamics. This subject is by itself interesting (thermomagnetic effect), but also necessary to elucidate questions of experimental parameter tolerance. We have found a solution to the pure SU(2) Yang-Mills equations of motion in Minkowski signature with an adjoint scalar field, which in the context of nonperturbative Yang-Mills thermodynamics and under the adiabatic approximation allows for the generalization of the thermal ground state to space-dependent temperature profiles. It was shown that such temperature gradients are capable of generating magnetic fields. This is the SU(2) thermomagnetic effect.

Finally, an investigation on the consistency of 1-loop resummation of the energy density and pressure of the SU(2) gas was made. We found that thermodynamical consistency cannot be guaranteed if radiative corrections to the vector modes in the effective theory are ignored.

It is remarkable that the experimental detection of SU(2) effects and thus confirmation of the $SU(2)_{\text{CMB}}$ hypothesis is achievable by a simple tabletop experiment consisting of a cryogenic chamber, black-body cavities and a well calibrated radiometer. The experimental realization of the black-body experiment described in this thesis is a worthwhile endeavour because of its considerable implications were the $SU(2)_{\text{CMB}}$ hypothesis be confirmed.

We introduced this work by referring to the low-frequency power-like deviation of the CMB spectrum from perfect black-body physics, which can be explained by assuming the $SU(2)_{\text{CMB}}$ hypothesis. Another important consequence of SU(2) dynamics can be read in [58]. There it is shown that the realization in nature of the $SU(2)_{\text{CMB}}$ hypothesis would invalidate the Higgs mechanism for electroweak symmetry breaking in the Standard Model. $SU(2)_{\text{CMB}}$ yields six additional degrees of freedom to the total number of cosmologically active relativistic degrees of freedom g_* at Big-Bang nucleosynthesis. This in turn would imply a value for the Fermi coupling at zero temperature G_F of about 12% larger than predicted by electroweak SM physics.

It is our hope that this thesis aids further experimental investigations regarding the $SU(2)_{\text{CMB}}$ hypothesis.

Appendices

Appendix A

SU(2) Equations of Motion with Scalar Field

A.1 Introduction

Here we derive a special solution to the SU(2) Yang-Mills Equations of Motion with a scalar field Φ taken as perturbation. The derivation is subject to some simplifying assumptions. Our only purpose here is to present the mathematical details, the physical interpretation of the result is discussed in chapter 4.

We work with Minkowski metric, defined here as $g^{\mu\nu} = \text{diag}(-1, 1, 1, 1)$ to streamline calculations

A.2 A particular solution

We now embark in our search for particular solutions of the SU(2) Yang-Mills equations of motion (3.9) with scalar field. These are given by

$$D_\mu G^{\mu\nu} = ie [\Phi, D^\nu \Phi] . \quad (\text{A.1})$$

We write the scalar field in capital greek Φ so as to differentiate it from the inert scalar ϕ described in chapter 3, since we will allow the scalar field to variate in space. Here we work in the physical unitary gauge (3.14), $\Phi^a = 2 \delta^{a3} |\Phi|$

Recall now that both Φ and the trivial topology gauge field $a_\mu = a_\mu^a t^a$ live in the adjoint representation, so the covariant derivative acts on them as $D_\mu = \partial_\mu \cdot -ie[a_\mu, \cdot]$. With this in mind we expand (A.1)

$$\begin{aligned} & \partial_\mu (\partial_\mu a_\nu - \partial_\nu a_\mu) \\ & -2ie\partial_\mu [a_\mu, a_\nu] + ie [\partial_\mu a_\mu, a_\nu] - ie [\partial_\nu a_\mu, a_\mu] - e^2 [a_\mu, [a_\mu, a_\nu]] \\ & -ie [\Phi, \partial_\nu \Phi] + e^2 [\Phi, [\Phi, a_\nu]] = 0 . \end{aligned} \quad (\text{A.2})$$

A.2.1 The Yang-Mills equations for static fields in Minkowski space-time

We are going to look for *stationary solutions*, that is, $\partial_0 \equiv 0$. The time-like $\nu = 0$ and space-like $\nu = k$ components of (A.2) then become

$$\begin{aligned} \partial_j^2 a_0 - 2ie\partial_j [a_j, a_0] + ie [\partial_j a_j, a_0] \\ - e^2 [a_\mu, [a_\mu, a_0]] + e^2 [\Phi, [\Phi, a_0]] = 0, \end{aligned} \quad (\text{A.3})$$

$$\begin{aligned} \partial_j^2 a_k - \partial_k \partial_j a_j - 2ie\partial_j [a_j, a_k] + ie [\partial_j a_j, a_k] \\ - ie [\partial_k a_\mu, a_\mu] - e^2 [a_\mu, [a_\mu, a_k]] + e^2 [\Phi, [\Phi, a_k]] = 0. \end{aligned} \quad (\text{A.4})$$

To simplify our notation, we define the complex fields

$$a_j^\pm \equiv \frac{1}{\sqrt{2}} (a_j^1 \pm ia_j^2). \quad (\text{A.5})$$

Now write equations (A.3) and (A.4) explicitly in color indices

$$\begin{aligned} [\partial^2 + 2iea_j^3 \partial_j + ie\partial_j a_j^3 - e^2 a_\mu^3 a_\mu^3 + 4e^2 |\Phi|^2] a_0^+ = ie [a_0^3 \partial_j + 2\partial_j a_0^3] a_j^+ \\ + e^2 [a_0^+ a_\mu^- - a_0^- a_\mu^+ - a_0^3 a_\mu^3] a_\mu^+, \end{aligned} \quad (\text{A.6})$$

$$\begin{aligned} [\partial^2 - 2e^2 a_\mu^+ a_\mu^-] a_0^3 + e^2 [a_0^+ a_\mu^- + a_0^- a_\mu^+] a_\mu^3 = -ie [a_0^- \partial_j + 2\partial_j a_0^-] a_j^+ \\ + c.c., \end{aligned} \quad (\text{A.7})$$

$$\begin{aligned} [\partial^2 + 2iea_j^3 \partial_j + ie\partial_j a_j^3 - e^2 a_\mu^3 a_\mu^3 + 4e^2 |\Phi|^2] a_k^+ \\ - ie [a_k^3 \partial_j + 2\partial_j a_k^3] a_j^+ + ie [a_\mu^3 \partial_k - \partial_k a_\mu^3] a_\mu^+ - \partial_k \partial_j a_j^+ = e^2 [a_k^+ a_\mu^- - a_k^- a_\mu^+ - a_k^3 a_\mu^3] a_\mu^+, \end{aligned} \quad (\text{A.8})$$

$$\begin{aligned} [\partial^2 - 2e^2 a_\mu^+ a_\mu^-] a_k^3 + e^2 [a_k^+ a_\mu^- + a_k^- a_\mu^+] a_\mu^3 - \partial_k \partial_j a_j^3 = -ie [a_k^- \partial_j + 2\partial_j a_k^-] a_j^+ - ie a_\mu^- \partial_k a_\mu^+ \\ + c.c.. \end{aligned} \quad (\text{A.9})$$

The symbol *c.c.* denotes the complex conjugate of the expression on the right hand side of equations A.7 and (A.9).

A.2.2 Simple configurations with U(1) magnetic field

In order to solve the above equation system, we make further simplifying assumptions. Namely, that the time-like-component of the tree-level massless gauge field (photon), as well as the space-like components of the complex tree-level heavy fields (A.5), both vanish.

$$a_0^3 = a_k^\pm = 0. \quad (\text{A.10})$$

Since we have already assumed stationarity, this restriction limits the set of possible solutions to pure magnetic field configurations. Under our assumptions, the electric field is

always zero $\mathbf{E} = -\nabla A^0 - \partial_t \mathbf{A} = 0$, and only magnetic configurations $\mathbf{B} = \nabla \times \mathbf{A}$ are possible. From (A.10) it follows that the expression $a_\mu^\pm a_\mu^3 = 0$ vanishes, equations (A.7) and (A.8) are thus trivially satisfied. Inserting (A.10) in equation (A.6) we obtain (recall our metric convention)

$$[\partial^2 + 2iea_j^3 \partial_j + ie \partial_j a_j^3 - e^2 a_j^3 a_j^3 + 4e^2 |\Phi|^2] a_0^+ = 0. \quad (\text{A.11})$$

Recall the identity $f \partial^2 f = \frac{1}{2} \partial^2 f^2 - (\partial f)^2$, which we use to write the above expression as

$$\left[\frac{1}{2} \partial^2 + e^2 (4|\Phi|^2 - a_j^3 a_j^3) \right] (a_0^+)^2 = (\partial_j a_0^+)^2 - ie \partial_j \left[(a_0^+)^2 a_j^3 \right]. \quad (\text{A.12})$$

Reordering terms, (A.12) becomes

$$e^2 (4|\Phi|^2 - a_j^3 a_j^3) - \left(\frac{\partial_j a_0^+}{a_0^+} \right)^2 + \frac{1}{2} \partial^2 a_0^{+2} / a_0^{+2} + ie \partial_j \left[a_0^{+2} a_j^3 \right] / a_0^{+2} = 0. \quad (\text{A.13})$$

Expanding a_0^+ in a positive real magnitude $a_0(x)$ and a real phase $\varphi(x)$

$$a_0^+ \equiv a_0 e^{i\varphi}, \quad (\text{A.14})$$

we can simplify the gradient, Laplacian and divergence terms in (A.13)

$$\begin{aligned} \partial_j \left[a_0^{+2} a_j^3 \right] / a_0^{+2} &= \partial_j a_j^3 + 2a_j^3 \frac{\partial_j a_0^+}{a_0^+}, \\ \frac{\partial_j a_0^+}{a_0^+} &= \frac{\partial_j a_0}{a_0} + i \partial_j \varphi, \\ \partial^2 a_0^{+2} / a_0^{+2} &= 2 \left(\frac{\partial_j a_0}{a_0} \right)^2 + 2 \frac{\partial^2 a_0}{a_0} - 4 (\partial_j \varphi)^2 + 2i \left(\partial^2 \varphi + 4 \partial_j \varphi \frac{\partial_j a_0}{a_0} \right). \end{aligned}$$

Separate (A.13) into real and imaginary components

$$\begin{aligned} e^2 (4|\Phi|^2 - a_j^3 a_j^3) - (\partial_j \varphi)^2 - 2ea_j^3 \partial_j \varphi + \frac{\partial^2 a_0}{a_0} \\ + i \left[\partial^2 \varphi + 2 \partial_j \varphi \frac{\partial_j a_0}{a_0} + e \partial_j a_j^3 + 2ea_j^3 \frac{\partial_j a_0}{a_0} \right] = 0. \end{aligned} \quad (\text{A.15})$$

Taking $\text{Re}[(\text{A.15})]=0$ and $\text{Im}[(\text{A.15})]=0$ we obtain two real equations

$$e^2 |\vec{a}^3|^2 - \frac{\partial^2 a_0}{a_0} + \partial_j \varphi [\partial_j \varphi + 2ea_j^3] = 4e^2 |\Phi|^2, \quad (\text{A.16})$$

$$e \partial_j a_j^3 + 2ea_j^3 \frac{\partial_j a_0}{a_0} + \partial^2 \varphi + 2 \partial_j \varphi \frac{\partial_j a_0}{a_0} = 0. \quad (\text{A.17})$$

Inserting (A.10) in (A.9) gives us

$$[\partial^2 + 2e^2 a_0^+ a_0^-] a_k^3 - \partial_k \partial_j a_j^3 = ie [a_0^- \partial_k a_0^+ - a_0^+ \partial_k a_0^-]. \quad (\text{A.18})$$

Writing a_0^+ in components as in (A.14), we finally get

$$[\partial^2 + 2e^2 (a_0)^2] a_k^3 - \partial_k \partial_j a_j^3 = -2e (a_0)^2 \partial_k \varphi. \quad (\text{A.19})$$

Reordering (A.19)

$$2e(a_0)^2 [ea_k^3 + \partial_k \varphi] = \partial_k \partial_j a_j^3 - \partial^2 a_k^3. \quad (\text{A.20})$$

Now, from (A.17) one may easily see that

$$\partial_j [(a_0)^2 (ea_j^3 + \partial_j \varphi)] = 0.$$

That is, there is some vector field $\vec{V}(x)$ such that

$$(a_0)^2 (ea_k^3 + \partial_k \varphi) = \mathbf{rot}_k \vec{V}, \quad (\text{A.17}')$$

where we have defined $\mathbf{rot}_k \vec{V} \equiv (\nabla \times \vec{V})_k$.

Moreover, from (A.20) we infer

$$2e \mathbf{rot}_k \vec{V} = \partial_k \partial_j a_j^3 - \partial^2 a_k^3. \quad (\text{A.20}')$$

So $\vec{V}(x)$ must be of the form

$$2e \vec{V}_k = \mathbf{rot}_k \vec{a}^3 \stackrel{!}{=} \mathbf{B}_k. \quad (\text{A.21})$$

Equation (A.21) can be used to rewrite (A.16) as

$$4e^2 |\Phi|^2 = e^2 |\vec{a}^3|^2 - \frac{\partial^2 a_0}{a_0} + \partial_j \varphi \frac{\mathbf{rot}_j \mathbf{B}}{e(a_0)^2} - (\partial_j \varphi)^2. \quad (\text{A.16}')$$

A.2.3 One-dimensional temperature distribution

We now specialize to the case of spatial dependency in just one dimension, and assume that the scalar source Φ and all Φ -coupled physical fields to be functions of coordinate $z \equiv x_3$ only, so that $|\Phi(\vec{x})| = |\Phi(z)|$, and so on. Our double primed equations will hold for this special case only (together with stationarity and unitary gauge fixing (3.14), remember).

Under this assumptions, we can write equation (A.21) in the form

$$\begin{aligned} a_k^3 &= a_k^3(z), \\ \implies 2e \mathbf{rot}_k \vec{V} &= \mathbf{rot}_k \mathbf{B} = (\delta_{k3} - 1) \partial_z^2 a_k^3. \end{aligned} \quad (\text{A.22})$$

The magnetic field \mathbf{B} is perpendicular to the z -axis. Further, together with equation (A.17'), equation (A.22) directly implies

$$ea_3^3(x) = -\partial_z \varphi(x). \quad (\text{A.23})$$

It follows that $\varphi(x)$ functions as a U(1) gauge parameter, and can be set to zero (together with a_3^3). The identity (A.23) allows us to use equation (A.17') to solve for a_0

$$(a_0)^2 = -\frac{\partial_z^2 a_1^3}{2e^2 a_1^3} \stackrel{!}{=} -\frac{\partial_z^2 a_2^3}{2e^2 a_2^3}, \quad (\text{A.17}'')$$

since under our assumptions $\partial_1 \varphi = \partial_2 \varphi = 0$. Equation (A.17'') implies the identity $a_2^3 \partial_z^2 a_1^3 = a_1^3 \partial_z^2 a_2^3$, and can be used to determine a_0 from the fields $a_{1,2}^3$. These fields also define the magnetic field \mathbf{B} , $B_1 = -\partial_z a_2^3$, $B_2 = \partial_z a_1^3$.

The expression (A.16') for $|\Phi|^2$ also simplifies in this special case. From (A.22) we read $\mathbf{rot}_3 \mathbf{B} \equiv 0$, which together with $\partial_1 \varphi = \partial_2 \varphi = 0$ and equation (A.23), reduces (A.16') to

$$|\Phi|^2 = \frac{1}{4} \sum_{i=1,2} a_i^3 a_i^3 - \frac{\partial_z^2 a_0}{4e^2 a_0}. \quad (\text{A.24})$$

The temperature profile can be calculated from (3.2). Inserting (A.24) we obtain ($T \equiv \beta^{-1}$)

$$T(z) = \frac{\Lambda^3}{2\pi |\Phi|^2} = \frac{\Lambda^3}{2\pi} \left(\frac{1}{4} \sum_{i=1,2} a_i^3 a_i^3 - \frac{\partial_z^2 a_0}{4e^2 a_0} \right)^{-1}. \quad (\text{A.25})$$

This means that if we find a reasonable Ansatz for $a^3(z)$, we automatically obtain the fields a_0 , \mathbf{B} , $|\Phi|$ and the profile for the temperature $T(z)$. Such solutions and their physical interpretations are discussed in chapter (4).

Appendix B

Review of Classical Gauge Fields

The basic result of the nonperturbative approach to SU(2) Yang-Mills thermodynamics in the deconfining phase reviewed in chapter 3 is the emergence of an inert scalar field ϕ , which together with a pure gauge configuration a_μ^{gs} (see equation (3.10)) defines an effective thermal ground state acting as a background for the dynamics of weakly interacting thermal quasiparticles. The scalar field ϕ is also responsible for breaking the original SU(2) gauge symmetry down to its abelian subgroup U(1). Two of the original off-Cartan gauge modes acquire a temperature dependent mass, while a third one is left massless at tree-level. Under the SU(2)_{CMB} hypothesis, this tree-level massless (TLM) gauge mode is identified with the SM photon. (see section 3.4). Radiative corrections, however, induce an effective *screening mass* $m = \sqrt{G}$ for the transverse polarizations of the TLM mode, which modifies their dispersion law (see section 3.5.3). Further, a possible longitudinal polarization is rendered nonpropagating (see section 3.5.5).

Massive particles of spin 1 are described by the *Proca equations*. But the standard radiometric results used in this work were derived for massless spin 1 fields, described by the *Maxwell equations*. We must therefore explicitly check how these results are altered for spin 1 (vector boson) particles of nonzero dynamical mass.

In this Appendix, we review the theory of classical spin-1 (vector boson) fields, following the presentation in [20]. First we introduce the Lagrangians for the massless and the massive case, i.e., the Maxwell and Proca fields. The respective equations of motion are derived, along with expressions for the energy and momentum density for each field. In section B.2, polarization vectors for the massless and the massive case are introduced, we then expand the energy and momentum density in Fourier modes. Section B.3 recalls the continuity equation. Finally, since propagating excitations of the SU(2) TLM mode may only be transverse, transversality must therefore be imposed on these Proca solutions. This is done in section B.4.

The results of this appendix are mostly needed to rederive Planck's black-body formula (see section 5.1.4) and the Fresnel-Kirchhoff diffraction integral used in calculating the effective antenna area (see appendix C and section 5.2.2). It will be seen that the standard results remain unchanged, save for the modified dispersion relation

$$(\hbar\omega_{\mathbf{p}})^2 = (c\mathbf{p})^2 + G(\omega, \mathbf{p}; T, \Lambda) . \quad (\text{B.1})$$

B.1 Lagrangian formulation

B.1.1 The Maxwell field

As we saw in chapter 2, the dynamics of the massless spin-1 field A^μ subject to an external current density $j^\mu = (\rho, \mathbf{j})$ are described by the Lagrangian density

$$\mathcal{L}_M \equiv -\frac{1}{4}F^{\mu\nu}F_{\mu\nu} - ej^\mu A_\mu. \quad (\text{B.2})$$

with the *gauge field* $A_\mu = (A_0, \mathbf{A})$, the *field strength* $F_{\mu\nu} = \partial_\mu A_\nu - \partial_\nu A_\mu$ and the *coupling* e is the charge of the external field inducing the current density j^μ . The physical electric and magnetic fields are defined as in (2.4) and (2.5).

By the principle of least action

$$\delta S = \delta \int d^4x \mathcal{L} \stackrel{!}{=} 0 \quad \Longrightarrow \quad \frac{\delta \mathcal{L}}{\delta A_\nu} - \partial_\mu \frac{\delta \mathcal{L}}{\delta \partial_\mu A_\nu} = 0,$$

we obtain the Maxwell field equations of motion

$$\partial_\mu F^{\mu\nu} = j^\nu, \quad (\text{B.3})$$

which for the massless gauge field A^μ read

$$\square A^\nu + \partial^\nu \partial_\mu A^\mu = j^\nu. \quad (\text{B.4})$$

Taking the divergence of (B.3) leads to the *continuity equation*

$$\partial_\nu j^\nu = 0, \quad (\text{B.5})$$

since $F^{\mu\nu}$ is antisymmetric. Thus, in the massless spin-1 field theory, current conservation is *automatically guaranteed*. This is a direct consequence of the conservation of U(1) gauge symmetry.

Writing (B.4) in terms of the electromagnetic fields (2.4) and (2.5), we recover the familiar *inhomogeneous* Maxwell equations, which we write here in SI units

$$\nabla \cdot \mathbf{E} = \frac{\rho}{\varepsilon_0}, \quad (\text{B.6a})$$

$$\nabla \times \mathbf{B} - \varepsilon_0 \mu_0 \partial_t \mathbf{E} = \mu_0 \mathbf{j}. \quad (\text{B.6b})$$

Recall also from chapter 2 that the *Bianchi identity* satisfied by the field strength tensor [3, 15, 57]

$$\partial_\mu \tilde{F}^{\mu\nu} = 0, \quad (\text{B.7})$$

results in the *homogeneous* Maxwell equations, here given in SI units

$$\nabla \cdot \mathbf{B} = 0, \quad (\text{B.8a})$$

$$\nabla \times \mathbf{E} + \partial_t \mathbf{B} = 0. \quad (\text{B.8b})$$

In the following, we will be mostly interested in *vacuum* configurations, that is, $j^\mu \equiv 0$.

Note first that the covariant formulation in (B.2) introduces redundant degrees of freedom that allow for *local gauge transformations* without affecting the Lagrangian density

$$A_\mu \rightarrow A'_\mu = A_\mu + \partial_\mu \Lambda(x), \quad (\text{B.9})$$

$$\mathcal{L} \rightarrow \mathcal{L}' = \mathcal{L}, \quad (\text{B.10})$$

for a Lorentz scalar function $\Lambda(x)$. In order to interpret the gauge field A^μ physically, we must *fix the degrees of freedom* so as to eliminate spurious polarization modes. This is called *gauge fixing*, and can be done in various ways. A manifestly covariant gauge fixing is given by the *Lorentz gauge*

$$\partial_\mu A^\mu = 0, \quad (\text{B.11})$$

In this gauge, the field equations for the Maxwell Field (B.4) become

$$\square A^\mu = j^\mu. \quad (\text{B.12})$$

The Lorentz condition (B.11) however still does not fix the gauge completely. Gauge equivalent field configurations may still be found that are related to each other by gauge transformation functions $\Lambda(x)$ which solve the Laplace equation, $\square \Lambda(x) = 0$. The Lorentz constraint $\partial_\mu A^\mu = 0$ cannot fix A^μ uniquely, as the Maxwell field possesses just two independent degrees of freedom, not four.

Energy and momentum density

The familiar expression for the *energy-momentum tensor*

$$\theta^{\mu\nu} = \frac{\delta \mathcal{L}}{\delta \partial_\mu A_\sigma} \delta^\nu A_\sigma - g^{\mu\nu} \mathcal{L}, \quad (\text{B.13})$$

turns out to be not symmetric (also not gauge invariant) when the Lagrangian B.2 is inserted directly in (B.13). To construct a physical energy-momentum tensor $T^{\mu\nu}$ we add a surface term to (B.13)

$$\begin{aligned} T^{\mu\nu} &= \theta^{\mu\nu} + \partial_\sigma (F^{\mu\sigma} A^\nu) \\ &= \frac{1}{4} g^{\mu\nu} F^{\alpha\beta} F_{\alpha\beta} + F^\mu{}_\sigma F^{\sigma\nu} + g^{\mu\nu} j_\sigma A^\sigma - j^\mu A^\nu. \end{aligned} \quad (\text{B.14})$$

Writing (B.14) in terms of the physical fields (2.4) and (2.5), and taking $j^\mu = 0$, we recover the familiar expression for the electromagnetic *energy density* in vacuum

$$\begin{aligned} \rho \equiv T^{00} &= \frac{1}{4} (2F^{0i} F_{0i} + F^{ij} F_{ij}) + F^0{}_\sigma F^{\sigma 0} \\ &= \frac{1}{2} \mathbf{E}^2 + \frac{1}{4} (\delta_m^j \delta_n^k - \delta_m^k \delta_n^j) F_{jk} F^{mn} \\ &= \frac{1}{2} \mathbf{E}^2 + \left(-\frac{1}{2} \varepsilon^{ijk} F_{jk} \right) \left(-\frac{1}{2} \varepsilon_{imn} F^{mn} \right) \\ &= \frac{1}{2} (\mathbf{E}^2 + \mathbf{B}^2), \end{aligned} \quad (\text{B.15})$$

with $\varepsilon^{ijk}\varepsilon_{imn} = \delta_m^j\delta_n^k - \delta_m^k\delta_n^j$. The *Poynting vector* of the Maxwell field in vacuum, that is, the vacuum *momentum density*, can also be easily calculated

$$\begin{aligned} S^k &\equiv T^{0k} = F^{0\sigma}F_\sigma{}^k = E^i F_i{}^k = E^i \frac{1}{2} \left(\delta_i^m \delta_n^k - \delta_i^k \delta_n^m \right) F_m{}^n \\ &= \varepsilon_{ijk} E^i \left(-\frac{1}{2} \varepsilon^{jmn} F_{mn} \right), \\ \mathbf{S} &= \mathbf{E} \times \mathbf{B}. \end{aligned} \tag{B.16}$$

In SI units the fields are rescaled as $\mathbf{E} \rightarrow \frac{\mathbf{E}}{c}$, $\mathbf{S} \rightarrow \frac{\mathbf{S}}{c}$, $T^{\mu\nu} \rightarrow \frac{1}{\mu_0} T^{\mu\nu}$ and

$$\rho = \frac{1}{2} \left(\varepsilon_0 \mathbf{E}^2 + \frac{1}{\mu_0} \mathbf{B}^2 \right), \tag{B.17}$$

$$\mathbf{S} = \frac{1}{\mu_0} \mathbf{E} \times \mathbf{B}. \tag{B.18}$$

This basic results can now be compared with the same expressions for the Proca field, which we review next.

B.1.2 The Proca field

The massive spin-1 field, or *Proca* field, is described by the Lagrangian density (B.2) plus a mass term quadratic in the gauge field

$$\mathcal{L} = -\frac{1}{4} F_{\mu\nu} F^{\mu\nu} - j_\mu A^\mu + \frac{1}{2} m^2 A_\mu A^\mu. \tag{B.19}$$

The electric and magnetic fields are again defined as in (2.4) and (2.5).

By the principle of least action we obtain the Proca field equations of motion

$$\partial_\mu F^{\mu\nu} + m^2 A^\nu = j^\nu. \tag{B.20}$$

In terms of the field A^μ this reads

$$(\square + m^2) A^\nu = \partial^\nu \partial_\mu A^\mu + j^\nu. \tag{B.21}$$

The *inhomogeneous* Proca equations result from writing (B.20) in terms of the electric and magnetic fields, as in the Maxwell case. In SI units, they are given by

$$\nabla \cdot \mathbf{E} = \frac{\rho}{\varepsilon_0} - \left(\frac{mc}{\hbar} \right)^2 A^0, \tag{B.22a}$$

$$\nabla \times \mathbf{B} - \varepsilon_0 \mu_0 \partial_t \mathbf{E} = \mu_0 \mathbf{j} - \left(\frac{mc}{\hbar} \right)^2 \mathbf{A}. \tag{B.22b}$$

These are the inhomogeneous Maxwell equations (B.3) modified by a mass term $\left(\frac{mc}{\hbar} \right)^2$. Note the appearance of \hbar along with c . As in the massless case, the Bianchi identity (B.7) results in the *homogeneous* Proca equations

$$\nabla \cdot \mathbf{B} = 0, \tag{B.23a}$$

$$\nabla \times \mathbf{E} + \partial_t \mathbf{B} = 0. \tag{B.23b}$$

which remain unchanged from the massless case

The addition of a mass term to the spin-1 field Lagrangian (B.2) breaks the U(1) gauge invariance. As consequence of this, the current j^ν is no longer inevitably conserved. Taking the four-divergence from (B.20), we get

$$m^2 \partial_\nu A^\nu = \partial_\nu j^\nu. \quad (\text{B.24})$$

This expression does not automatically vanish, in contrast to the massless case, and one needs to explicitly postulate $\partial_\nu j^\nu \stackrel{!}{=} 0$ if current conservation is to be maintained. By demanding current conservation, the massive spin-1 field automatically satisfies the *Lorentz condition*

$$\partial_\nu A^\nu = 0. \quad (\text{B.25})$$

There is no gauge freedom left as in the Maxwell case, and the Proca field equations become

$$(\square + m^2) A^\mu = j^\mu. \quad (\text{B.26})$$

Energy and momentum density

The energy momentum tensor is given by (B.14) with an added mass term

$$\begin{aligned} T^{\mu\nu} = & \frac{1}{4} g^{\mu\nu} F^{\alpha\beta} F_{\alpha\beta} + F^\mu{}_\sigma F^{\sigma\nu} + g^{\mu\nu} j_\sigma A^\sigma - j^\mu A^\nu \\ & + m^2 \left(A^\mu A^\nu - \frac{1}{2} g^{\mu\nu} A_\sigma A^\sigma \right). \end{aligned} \quad (\text{B.27})$$

Setting $j^\mu = 0$ we obtain the energy density in vacuum

$$\rho \equiv T^{00} = \frac{1}{2} (\mathbf{E}^2 + \mathbf{B}^2) + \frac{1}{2} m^2 (A_0^2 + \mathbf{A}^2). \quad (\text{B.28})$$

Similarly, the *Poynting vector* of the Proca field in vacuum can be calculated to be

$$\begin{aligned} S^i & \equiv T^{0i}, \\ \mathbf{S} & = \mathbf{E} \times \mathbf{B} + m^2 A_0 \mathbf{A}. \end{aligned} \quad (\text{B.29})$$

By converting to SI units, the fields are rescaled as $\mathbf{S} \rightarrow \frac{\mathbf{S}}{c}$, $\mathbf{E} \rightarrow \frac{\mathbf{E}}{c}$, $A^0 \rightarrow \frac{A^0}{c}$, $T^{\mu\nu} \rightarrow \frac{1}{\mu_0} T^{\mu\nu}$. The energy and momentum density of the Proca field are given in SI units by

$$\rho = \frac{1}{2} \left(\varepsilon_0 \mathbf{E}^2 + \frac{1}{\mu_0} \mathbf{B}^2 \right) + \frac{1}{2} \left(\frac{mc}{\hbar} \right)^2 \left(\varepsilon_0 A_0^2 + \frac{1}{\mu_0} \mathbf{A}^2 \right), \quad (\text{B.30})$$

$$\mathbf{S} = \frac{1}{\mu_0} \left(\mathbf{E} \times \mathbf{B} + \left(\frac{mc}{\hbar} \right)^2 A_0 \mathbf{A} \right). \quad (\text{B.31})$$

B.2 Plane wave expansion and dispersion relations

B.2.1 Polarization vectors

To ease calculations, we will expand the vector field A^μ in its Fourier modes,

$$A_{k,\lambda}{}^\mu(x) = N_k \epsilon_{k,\lambda}{}^\mu e^{-ikx}, \quad (\text{B.32})$$

with $\epsilon_{k,\lambda}^\mu$ a set of four 4-dimensional *polarization vectors* labeled by λ . Demand that the polarization vectors $\epsilon_{k,\lambda}^\mu$ build a 4-dimensional orthonormal system

$$\epsilon_{k,\lambda}^\mu \epsilon_{k,\lambda'\mu} = g_{\lambda\lambda'}. \quad (\text{B.33})$$

Following [20], we may define a set of polarization vectors obeying (B.33) for the Maxwell and Proca fields.

Polarization vectors for the massless field

In the Lorentz frame where the plane wave has 3-momentum \mathbf{k} , we may pick two space-like *transverse polarization vectors*

$$\epsilon_{k,1} = (0, \vec{\epsilon}_{k,1}), \quad (\text{B.34a})$$

$$\epsilon_{k,2} = (0, \vec{\epsilon}_{k,2}), \quad (\text{B.34b})$$

such that for $i, j \in \{1, 2\}$ it holds

$$\mathbf{k} \cdot \vec{\epsilon}_{k,i} = 0, \quad (\text{B.35a})$$

$$\vec{\epsilon}_{k,i} \cdot \vec{\epsilon}_{k,j} = \delta_{ij}. \quad (\text{B.35b})$$

For the *longitudinal polarization* $\epsilon_{k,3}$ a covariant expression can be written by first defining the time-like unit vector n with $n^2 = 1$ and $n = (1, \vec{0})$ in the local frame. Then

$$\epsilon_{k,3} = \frac{k - n(k \cdot n)}{\sqrt{(k \cdot n)^2 - k^2}}. \quad (\text{B.36})$$

In the local frame therefore $\epsilon_{k,3} = (0, \frac{\mathbf{k}}{|\mathbf{k}|})$. The remaining *time-like polarization* degree can be taken to be n ,

$$\epsilon_{k,0} = n. \quad (\text{B.37})$$

One can easily check that this set of four polarization vectors satisfy the normalization condition (B.33).

Polarization vectors for the massive field

Again, working in the Lorentz frame where the plane wave has 3-momentum \mathbf{k} , we define *transverse polarization* vectors as in the massless case (B.34), (B.35). The third vector may be chosen so that its spatial components are parallel to \mathbf{k} . Its zero-component can be further specified by the condition that $\epsilon_{k,3}$ is orthogonal to the momentum four-vector $k_\mu \epsilon_{k,3}^\mu = 0$. This completely defines the *longitudinal polarization vector*

$$\epsilon_{k,3} = \left(\frac{|\mathbf{k}|}{m}, \frac{\mathbf{k}}{|\mathbf{k}|} \frac{k^0}{m} \right). \quad (\text{B.38})$$

Note that this definition was impossible in the massless case, where 4-dimensional transversality would have implied infinite norm.

The fourth *time-like polarization vector* can be defined as

$$\epsilon_{k,0} = \frac{1}{m} k. \quad (\text{B.39})$$

This set of polarization vectors also satisfy condition (B.33).

B.2.2 Plane wave expansion of the Maxwell field

In the *Lorentz gauge* $\partial_\mu A^\mu = 0$ the equations of motion (B.4) for the Maxwell field A^μ become (B.12) and the general solution may be given as a sum over polarizations λ , which labels the set of four polarization vectors ϵ_λ^μ for the massless case given in (B.34), (B.35), (B.37), (B.36).

$$A^\mu(x) \sim \sum_\lambda \sum_k \epsilon_{k,\lambda}^\mu e^{-ikx} \Big|_{k^0=\omega_{\mathbf{k}}}, \quad (\text{B.40})$$

The familiar dispersion relation for the Maxwell field in vacuum can easily be recovered in the Lorentz gauge $\partial_\mu A^\mu = 0$ by inserting (B.40) into (B.12) and taking $j^\mu = 0$,

$$\omega_{\mathbf{k}} = |\mathbf{k}|. \quad (\text{B.41})$$

Consider now the *Coulomb gauge* $\nabla \cdot \mathbf{A} = 0$. Then (B.4) becomes

$$\square \mathbf{A} + \partial_t \nabla A^0 = 0, \quad (\text{B.42a})$$

$$\nabla^2 A^0 = 0. \quad (\text{B.42b})$$

We can take $A^0 = 0$ and expand \mathbf{A} in its Fourier modes. Taking the limit

$$\lim_{V \rightarrow \infty} \frac{1}{V} \sum_{\mathbf{k}} \rightarrow \int \frac{d^3 \mathbf{k}}{(2\pi)^3}, \quad (\text{B.43})$$

we can write the sum over all modes \mathbf{k} as

$$\mathbf{A}(x) = \sum_\lambda \int \frac{d^3 \mathbf{k}}{(2\pi)^3} N_k \left(\vec{\epsilon}_{k,\lambda} e^{-ikx} + \vec{\epsilon}_{k,\lambda}^* e^{ikx} \right) \Big|_{k^0=\omega_{\mathbf{k}}}. \quad (\text{B.44})$$

Since $\nabla \cdot \mathbf{A} = 0$ we sum only over the transverse (physical) modes $\lambda = 1, 2$. Choose linear polarization so we can take $\epsilon_{k,\lambda}$ real. The fields are then given by

$$\mathbf{A}(x) = \sum_{\lambda=1}^2 \int \frac{d^3 \mathbf{k}}{(2\pi)^3} N_k \vec{\epsilon}_{k,\lambda} \left(e^{-ikx} + e^{ikx} \right) \Big|_{k^0=\omega_{\mathbf{k}}}, \quad (\text{B.45a})$$

$$\mathbf{E}(x) = \sum_{\lambda=1}^2 \int \frac{d^3 \mathbf{k}}{(2\pi)^3} N_k i\omega_{\mathbf{k}} \vec{\epsilon}_{k,\lambda} \left(e^{-ikx} - e^{ikx} \right) \Big|_{k^0=\omega_{\mathbf{k}}}, \quad (\text{B.45b})$$

$$\mathbf{B}(x) = \sum_{\lambda=1}^2 \int \frac{d^3 \mathbf{k}}{(2\pi)^3} N_k i\mathbf{k} \times \vec{\epsilon}_{k,\lambda} \left(e^{-ikx} - e^{ikx} \right) \Big|_{k^0=\omega_{\mathbf{k}}}. \quad (\text{B.45c})$$

We may now express the total energy Q of the Maxwell field as the integral of (B.15) over some finite volume V

$$\begin{aligned} Q &= \int_V d^3 \mathbf{x} \rho \\ &= \int_V d^3 \mathbf{x} \frac{1}{2} (\mathbf{E}^2 + \mathbf{B}^2). \end{aligned} \quad (\text{B.46})$$

Inserting the Fourier expansion of the fields and taking $V \rightarrow \infty$ we get

$$Q = \frac{1}{2} \sum_{\lambda=1}^2 \sum_{\lambda'=1}^2 \int_V d^3\mathbf{x} \int \frac{d^3\mathbf{k}}{(2\pi)^3} \int \frac{d^3\mathbf{q}}{(2\pi)^3} N_k N_q (\omega_{\mathbf{k}} \omega_{\mathbf{q}} \vec{\epsilon}_{k,\lambda} \cdot \vec{\epsilon}_{q,\lambda'} + (\mathbf{k} \times \vec{\epsilon}_{k,\lambda}) \cdot (\mathbf{q} \times \vec{\epsilon}_{q,\lambda'})) \left(e^{ix(k-q)} + e^{-ix(k-q)} - e^{-ix(k+q)} - e^{ix(k+q)} \right) \Big|_{\substack{k^0=\omega_{\mathbf{k}} \\ q^0=\omega_{\mathbf{q}}}}.$$

The resulting delta functions are integrated over $d^3\mathbf{q}$. Recalling the vector identity $(\mathbf{a} \times \mathbf{b}) \cdot (\mathbf{c} \times \mathbf{d}) = (\mathbf{a} \cdot \mathbf{c})(\mathbf{b} \cdot \mathbf{d}) - (\mathbf{a} \cdot \mathbf{d})(\mathbf{b} \cdot \mathbf{c})$, the expression simplifies further to

$$Q = \frac{1}{2} \sum_{\lambda=1}^2 \sum_{\lambda'=1}^2 \int \frac{d^3\mathbf{k}}{(2\pi)^3} \left\{ 2N_k^2 (\omega_{\mathbf{k}}^2 \vec{\epsilon}_{k,\lambda} \cdot \vec{\epsilon}_{k,\lambda'} + \mathbf{k}^2 \epsilon_{k,\lambda} \cdot \vec{\epsilon}_{k,\lambda'} - (\mathbf{k} \cdot \vec{\epsilon}_{k,\lambda}) \cdot (\mathbf{k} \cdot \vec{\epsilon}_{k,\lambda'})) \right. \\ \left. - (e^{-2it\omega_{\mathbf{k}}} + e^{2it\omega_{\mathbf{k}}}) (\omega_{\mathbf{k}}^2 \vec{\epsilon}_{k,\lambda} \cdot \vec{\epsilon}_{k,\lambda'} - \mathbf{k}^2 \epsilon_{k,\lambda} \cdot \vec{\epsilon}_{k,\lambda'} + (\mathbf{k} \cdot \vec{\epsilon}_{k,\lambda}) \cdot (\mathbf{k} \cdot \vec{\epsilon}_{k,\lambda'})) \right\}.$$

Remembering the dispersion relation (B.41) and the polarization tensor definition (B.35)

$$Q = \sum_{\lambda=1}^2 \sum_{\lambda'=1}^2 \int \frac{d^3\mathbf{k}}{(2\pi)^3} 2N_k^2 \omega_{\mathbf{k}}^2 \vec{\epsilon}_{k,\lambda} \cdot \vec{\epsilon}_{k,\lambda'} = \sum_{\lambda=1}^2 \sum_{\lambda'=1}^2 \int \frac{d^3\mathbf{k}}{(2\pi)^3} 2N_k^2 \omega_{\mathbf{k}}^2 \delta_{\lambda\lambda'} \\ = \sum_{\lambda=1}^2 \int \frac{d^3\mathbf{k}}{(2\pi)^3} (2N_k^2 \omega_{\mathbf{k}}) \omega_{\mathbf{k}}. \quad (\text{B.47})$$

A similar calculation for the total momentum vector results in

$$\mathbf{P} = \sum_{\lambda=1}^2 \int \frac{d^3\mathbf{k}}{(2\pi)^3} (2N_k^2 \omega_{\mathbf{k}}) \mathbf{k}. \quad (\text{B.48})$$

B.2.3 Plane wave expansion of the Proca field

The vacuum solutions of the equations of motion for the Proca field (B.26) may also be written as plane waves

$$A^\mu(x) = \sum_{\lambda} \int \frac{d^3\mathbf{k}}{(2\pi)^3} N_k \left(\epsilon_{k,\lambda}^\mu e^{-ikx} + \epsilon_{k,\lambda}^{*\mu} e^{ikx} \right) \Big|_{k^0=\omega_{\mathbf{k}}}. \quad (\text{B.49})$$

The dispersion relation for the Proca field of mass m in vacuum results from replacing (B.49) into (B.26) and taking $j^\mu = 0$,

$$\omega_{\mathbf{k}} = \sqrt{\mathbf{k}^2 + m^2}. \quad (\text{B.50})$$

Recalling the consistency condition $\partial_\mu A^\mu = 0$ and again choosing $\epsilon_{k,\lambda}^\mu$ real this can be written as

$$A^0(x) = \sum_{\lambda=1}^3 \int \frac{d^3\mathbf{k}}{(2\pi)^3} N_k \frac{1}{\omega_{\mathbf{k}}} \mathbf{k} \cdot \vec{\epsilon}_{k,\lambda} \left(e^{-ikx} + e^{ikx} \right) \Big|_{k^0=\omega_{\mathbf{k}}}, \quad (\text{B.51})$$

$$\mathbf{A}(x) = \sum_{\lambda=1}^3 \int \frac{d^3\mathbf{k}}{(2\pi)^3} N_k \vec{\epsilon}_{k,\lambda} \left(e^{-ikx} + e^{ikx} \right) \Big|_{k^0=\omega_{\mathbf{k}}}. \quad (\text{B.52})$$

The electric and magnetic fields expand as

$$\mathbf{E}(x) = \sum_{\lambda=1}^3 \int \frac{d^3\mathbf{k}}{(2\pi)^3} N_k i \omega_{\mathbf{k}} \left(\vec{\epsilon}_{k,\lambda} - \frac{\mathbf{k} \cdot \vec{\epsilon}_{k,\lambda}}{\omega_{\mathbf{k}}^2} \mathbf{k} \right) \left(e^{-ikx} - e^{ikx} \right) \Big|_{k^0=\omega_{\mathbf{k}}}, \quad (\text{B.53})$$

$$\mathbf{B}(x) = \sum_{\lambda=1}^3 \int \frac{d^3\mathbf{k}}{(2\pi)^3} N_k i \mathbf{k} \times \vec{\epsilon}_{k,\lambda} \left(e^{-ikx} - e^{ikx} \right) \Big|_{k^0=\omega_{\mathbf{k}}}. \quad (\text{B.54})$$

Then the total energy may be calculated as before from (B.28) to give

$$Q = \sum_{\lambda=1}^3 \int \frac{d^3\mathbf{k}}{(2\pi)^3} (2N_k^2 \omega_{\mathbf{k}}) \omega_{\mathbf{k}}. \quad (\text{B.55})$$

This is the same expression as (B.47) but with an added (longitudinal) polarization.

The total momentum also follows from (B.29) after a little calculation, given by

$$\mathbf{P} = \sum_{\lambda=1}^3 \int \frac{d^3\mathbf{k}}{(2\pi)^3} (2N_k^2 \omega_{\mathbf{k}}) \mathbf{k}, \quad (\text{B.56})$$

summing over all 3 modes λ . Note that the total momentum it is always longitudinal, even though the gauge field and the electromagnetic fields are not always transverse.

B.3 Energy density and Flux

Recall that the *energy-momentum tensor* derived from the invariance of the Lagrangian under space-time translations obeys the conservation equation

$$\partial_\mu T^{\mu\nu} = 0, \quad (\text{B.57})$$

which integrated over a volume V in 3-space becomes

$$\begin{aligned} 0 &= \int_V d^3\mathbf{x} \partial_\mu T^{\mu\nu} \\ &= \int_V d^3\mathbf{x} (\partial_0 T^{00} + \partial_i T^{0i}) \\ &= \partial_t \int_V d^3\mathbf{x} \rho + \int_V d^3\mathbf{x} \nabla \cdot \mathbf{S}. \end{aligned}$$

Applying the known Gauss theorem we recover the familiar *equation of continuity*

$$\partial_t \int_V d^3\mathbf{x} \rho + \oint_{\partial V} d\sigma \cdot \mathbf{S} = 0, \quad (\text{B.58})$$

which is valid for both Maxwell and Proca fields.

B.4 Transversal solutions for the Proca field

It will become necessary for us to ignore the longitudinal modes of the Proca Equation since those modes are unexcitable in the thermal Yang Mills theory in the deconfining phase we reviewed in chapter 3. From (B.26) it is clear that we can choose transverse-only solutions for the sourceless case so long as we respect the condition $\partial_\mu A^\mu = 0$. Choosing $A^0 = 0$ immediately imposes the Coulomb "gauge" $\nabla \cdot \mathbf{A} = 0$, making the gauge field transverse. The electric field also recovers transversality since $\nabla \cdot \mathbf{E} = -m^2 A^0 = 0$. The degrees of freedom are now restricted to just two, and we recover all the same results from the Maxwell theory in Coulomb gauge but with a modified dispersion relation $\omega_{\mathbf{k}} = \sqrt{\mathbf{k}^2 + m^2}$

$$Q = \sum_{\lambda=1}^2 \int \frac{d^3\mathbf{k}}{(2\pi)^3} (2N_k^2 \omega_{\mathbf{k}}) \omega_{\mathbf{k}}, \quad (\text{B.59})$$

$$\mathbf{P} = \sum_{\lambda=1}^2 \int \frac{d^3\mathbf{k}}{(2\pi)^3} (2N_k^2 \omega_{\mathbf{k}}) \mathbf{k}. \quad (\text{B.60})$$

Consider now a single mode $\mathbf{A} = \mathbf{A}_{\mathbf{k}} e^{-ikx}|_{k^0=\omega_{\mathbf{k}}}$. The electric and magnetic fields are given by

$$\mathbf{E}_{\mathbf{k}} = i\omega_{\mathbf{k}} \mathbf{A}_{\mathbf{k}}, \quad (\text{B.61})$$

$$\mathbf{B}_{\mathbf{k}} = i\mathbf{k} \times \mathbf{A}_{\mathbf{k}}. \quad (\text{B.62})$$

The *time averaged Poynting vector* of this mode is given by

$$\begin{aligned} \mathbf{S}_{\mathbf{k}} &= \frac{1}{2} \text{Re} (\mathbf{E}_{\mathbf{k}} \times \mathbf{B}_{\mathbf{k}}^*) = \frac{1}{2} \omega_{\mathbf{k}} (\mathbf{A}_{\mathbf{k}}^2 \mathbf{k} - \mathbf{A}_{\mathbf{k}} \cdot \mathbf{k} \mathbf{A}_{\mathbf{k}}) \\ &= \frac{1}{2} \omega_{\mathbf{k}} |\mathbf{A}_{\mathbf{k}}|^2 \mathbf{k}, \end{aligned} \quad (\text{B.63})$$

$$|\mathbf{S}_{\mathbf{k}}| = \frac{1}{2} \frac{|\mathbf{k}|}{\omega_{\mathbf{k}}} |\mathbf{E}_{\mathbf{k}}|^2. \quad (\text{B.64})$$

We will use these expressions in our discussions of antennas in chapter 5.

Appendix C

The Fresnel-Kirchhoff Diffraction Integral from the Proca Equations

Here, we sketch a derivation of the *Fresnel-Kirchhoff Diffraction Integral* for the case of massive spin-1 particles. This integral formula is needed to calculate the effective antenna area, see section 5.2.2. We follow the presentation given in [60, 67], but accounting for nonzero mass.

C.1 Helmholtz equations

Take the curl of (B.23b) and eliminate \mathbf{B} with (B.22b) to get an expression containing only \mathbf{E} . Do likewise for \mathbf{B} with (B.22b), we arrive at

$$\nabla \times \nabla \times \mathbf{E} + (\partial_t^2 + m^2) \mathbf{E} = -\partial_t \mathbf{j} + \nabla (\nabla \cdot \mathbf{E}) , \quad (\text{C.1a})$$

$$\nabla \times \nabla \times \mathbf{B} + (\partial_t^2 + m^2) \mathbf{B} = \nabla \times \mathbf{j} . \quad (\text{C.1b})$$

Using the identity $\nabla \times \nabla \times \mathbf{V} = \nabla (\nabla \cdot \mathbf{V}) - \nabla^2 \mathbf{V}$ and recalling $\nabla \cdot \mathbf{B} = 0$ we get finally

$$(\nabla^2 - \partial_t^2 - m^2) \mathbf{E} = \partial_t \mathbf{j} , \quad (\text{C.2a})$$

$$(\nabla^2 - \partial_t^2 - m^2) \mathbf{B} = -\nabla \times \mathbf{j} . \quad (\text{C.2b})$$

Consider now the Fourier expansion of the components E_i, B_i . It is clear that, in the absence of charges, each such Fourier mode $E_{\mathbf{k}}, B_{\mathbf{k}}$ obeys the *homogeneous Helmholtz Equations*

$$(\nabla^2 + \mathbf{k}^2) E_{\mathbf{k}} = 0 , \quad (\text{C.3a})$$

$$(\nabla^2 + \mathbf{k}^2) B_{\mathbf{k}} = 0 , \quad (\text{C.3b})$$

with *dispersion relation*

$$\omega_{\mathbf{k}} = \sqrt{\mathbf{k}^2 + m^2} . \quad (\text{B.50})$$

We have omitted the component indices for clarity.

Finally, recall that the *Green's function* $G_{\mathbf{k}}(x, x_0)$ to the Helmholtz Equation

$$(\nabla^2 + \mathbf{k}^2) G_{\mathbf{k}}(x, x_0) = -4\pi \delta(x_0) , \quad (\text{C.4})$$

is given by the spherical wave $G_{\mathbf{k}}$ expanding about a point \mathbf{x}_0

$$G_{\mathbf{k}}(x, x_0) \equiv \frac{e^{-i|\mathbf{k}||x-x_0|}}{|x-x_0|}. \quad (\text{C.5})$$

C.2 Integral theorem of Helmholtz and Kirchhoff

We now investigate the problem of determining the field Vectors \mathbf{E} , \mathbf{B} at a point x_0 , given the values of the electric and magnetic field vectors over an equiphase surface S .

Recall *Green's theorem*: Let two scalar functions F , G be defined over some volume V , further let them have continuous first and second derivatives in V . Then F , G satisfy the following identity

$$\int_V dV (F \nabla^2 G - G \nabla^2 F) + \oint_{\partial V} d\vec{A} (F \nabla G - G \nabla F) = 0. \quad (\text{C.6})$$

Let \mathbf{E} , \mathbf{B} be defined over a volume V which contains x_0 , and have $u_{\mathbf{k}}(x)$ stand for any Fourier mode $E_{\mathbf{k}}$, $B_{\mathbf{k}}$. Inserting $u_{\mathbf{k}}$ and $G_{\mathbf{k}}$ as scalar potentials in (C.6), we get¹

$$\begin{aligned} \int_V dV (G_{\mathbf{k}}(x, x_0) \nabla^2 u_{\mathbf{k}}(x) - u_{\mathbf{k}}(x) \nabla^2 G_{\mathbf{k}}(x, x_0)) \\ = - \oint_{\partial V} d\vec{A} (G_{\mathbf{k}}(x, x_0) \nabla u_{\mathbf{k}}(x) - u_{\mathbf{k}}(x) \nabla G_{\mathbf{k}}(x, x_0)). \end{aligned} \quad (\text{C.7})$$

Using the identities (C.3), (C.4)

$$u_{\mathbf{k}}(x_0) = -\frac{1}{4\pi} \oint_{\partial V} d\vec{A} (G_{\mathbf{k}}(x, x_0) \nabla u_{\mathbf{k}}(x) - u_{\mathbf{k}}(x) \nabla G_{\mathbf{k}}(x, x_0)). \quad (\text{C.8})$$

The fields at point x_0 have thus been expressed as an integral over a boundary surface ∂V which must contain x_0 .

In application to antenna radiation problems, the surface ∂V (called antenna *aperture*) for which we know the field distribution (called *illumination*) is not closed. To calculate anything useful, formula (C.8) needs to be generalized to open surfaces. We expect linear integrals over the open surface boundary to appear as extra terms. However, it turns out that under still reasonable conditions we may ignore the extra terms and integrate directly with (C.8) over the open surface [60]. Namely, in the *Frauenhofer (far-field) approximation* the *diffraction field* $u_{\mathbf{k}}$ over the antenna aperture A is given by

$$u_{\mathbf{k}}(x_0) = -\frac{1}{4\pi} \int_A d\vec{A} (G_{\mathbf{k}}(x, x_0) \nabla u_{\mathbf{k}}(x) - u_{\mathbf{k}}(x) \nabla G_{\mathbf{k}}(x, x_0)). \quad (\text{C.9})$$

The Frauenhofer approximation is valid provided the point x_0 is far enough from the aperture,

$$R \geq \frac{1}{\pi} d^2 |\mathbf{k}|, \quad (\text{C.10})$$

¹The function $G_{\mathbf{k}}(x, x_0)$ is not continuous at x_0 . In this particular case, use of Green's theorem may be made rigorous by a simple limiting process [65]

where R is the distance from x_0 to the aperture surface A , d the maximum linear dimension of the aperture, and \mathbf{k} the wave vector of the monochromatic wave illuminating the aperture [67]. Expression (C.10) defines the *Frauenhofer region*. Integral expression (C.9) allows the calculation of $u_{\mathbf{k}}$ in the Frauenhofer region, *given the values of $u_{\mathbf{k}}$ at the aperture*. Thus, we may use (C.9) to solve antenna aperture problems by replacing $u_{\mathbf{k}}$ with the corresponding electromagnetic field component $E_{\mathbf{k}}$, $B_{\mathbf{k}}$.

Let us now approximate the field illuminating the aperture by using simple monochromatic wave

$$u_{\mathbf{k}}(x) = A(x) e^{ikL(x)}, \quad (\text{C.11})$$

with amplitude $A(x)$ and phase $L(x)$. Then

$$\begin{aligned} \frac{\partial u_{\mathbf{k}}}{\partial n} &\equiv \hat{\mathbf{n}} \cdot \nabla u_{\mathbf{k}} = ik u_{\mathbf{k}} \hat{\mathbf{n}} \cdot \nabla L + u_{\mathbf{k}} \frac{1}{A} \frac{\partial A}{\partial n} \\ &\approx ik u_{\mathbf{k}} \hat{\mathbf{n}} \cdot \nabla L, \end{aligned} \quad (\text{C.12})$$

where $\hat{\mathbf{n}}$ is defined as the normal to the surface element in (C.9), $d\vec{A} \equiv dA \hat{\mathbf{n}}$. It can further be shown that $\mathbf{s} \equiv \nabla L$ is the normal unit vector to the propagation wavefront [60]. It defines the direction of propagation of the wave illuminating the aperture A .

The second expression we need is

$$\frac{\partial G_{\mathbf{k}}}{\partial n} = \mathbf{n} \cdot \nabla G_{\mathbf{k}} = \left(\frac{1}{r} - ik \right) \mathbf{n} \cdot \hat{\mathbf{r}} \frac{e^{ikr}}{r}, \quad (\text{C.13})$$

where $\mathbf{r} \equiv \mathbf{x} - \mathbf{x}_0$. Finally, we define $\cos \theta_r = \mathbf{n} \cdot \hat{\mathbf{r}}$, $\cos \theta_s = \mathbf{n} \cdot \mathbf{s}$. After joining terms we get

$$u_{\mathbf{k}}(x, y, z) = \frac{1}{4\pi} \int_A dx_a dy_a \left[\left(\frac{1}{r} - ik \right) \cos \theta_r - ik \cos \theta_s \right] \frac{e^{ikr}}{r} u_{\mathbf{k}}(x_a, y_a). \quad (\text{C.14})$$

C.3 Fresnel-Kirchhoff diffraction integral

Since our derivation of (C.9) depended only on the field $u_{\mathbf{k}}$ obeying the Helmholtz equation, we may replace it with any solution of (C.3), including the vector components of the electric and magnetic fields. We can then write the *Fresnel-Kirchhoff Diffraction Integral*

$$E_{\mathbf{k}}(x, y, z) = \frac{1}{4\pi} \int_A dx_a dy_a \left[\left(\frac{1}{r} - ik \right) \cos \theta_r - ik \cos \theta_s \right] \frac{e^{ikr}}{r} E_{a,\mathbf{k}}(x_a, y_a). \quad (\text{C.15})$$

Here $E_{a,\mathbf{k}}(x_a, y_a)$ is the electric field at the aperture. In the Frauenhofer region, this expression can be further simplified to give

$$E_{\mathbf{k}}(r, \theta, \phi) = \frac{1}{2\pi i} \frac{e^{ikr}}{r} |\mathbf{k}| h_{\mathbf{k}}(\theta, \phi), \quad (\text{C.16})$$

with r, θ, ϕ polar coordinates defined with the aperture at the origin and normal to the z-axis [67]. The polar function $h_{\mathbf{k}}(\theta, \phi)$ is defined as surface integral over the illumination at the aperture A

$$h_{\mathbf{k}}(\theta, \phi) = \int_A dx_a dy_a e^{-ik \sin \theta (x_a \cos \phi + y_a \sin \phi)} E_{a,\mathbf{k}}(x_a, y_a). \quad (\text{C.17})$$

In this region, the propagating modes are simply spherical waves, with the Poynting vector \mathbf{S} parallel to \mathbf{k} and $\hat{\mathbf{r}}, \mathbf{S} \parallel \mathbf{k} \parallel \hat{\mathbf{r}}$. The radial component is then read from (B.64) as

$$S_{\mathbf{k}}(\theta, \phi) = \frac{1}{8\pi^2} \frac{|\mathbf{k}|^2}{r^2} \frac{|\mathbf{k}|}{\omega_{\mathbf{k}}} |h_{\mathbf{k}}(\theta, \phi)|^2. \quad (\text{C.18})$$

Appendix D

Fundamental Radiometric Quantities

Quantity	Symbol / Definition	Units
Radiant Energy	Q	J (Joules)
Radiant Energy Density	$w = dQ/dV$	J m ⁻³
Radiant Power (Flux)	$\Phi = dQ/dt$	W (Watt)
Radiant Exitance	$M = d\Phi/dA$	W m ⁻²
Irradiance	$E = d\Phi/dA$	W m ⁻²
Radiant Intensity	$I = d\Phi/d\Omega$	W sr ⁻¹
Radiance	$L = d^2\Phi/(d\Omega dA \cos \theta)$	W m ⁻² sr ⁻¹
Emmisivity	$\varepsilon = M/M_{bb}$	-

Taken from [22]

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